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Corunna Downs H2 Hydrogeological Study

CONTENTS

| 1. | Introduction | 1 |
|-----|--|----|
| 1.1 | Background | 1 |
| 1.1 | Scope of Work | 1 |
| 1.3 | Previous work | 4 |
| 2. | Physical setting | 4 |
| 1.2 | Topography | 4 |
| 2.1 | Climate | 4 |
| 2.2 | Catchments and Drainage | 6 |
| 3. | Regional Geology | 8 |
| 4. | Regional Hydrogeology | 9 |
| 5. | Drilling investigations | 11 |
| 5.1 | Pilot Bores | 11 |
| 5.2 | Production Bores | 11 |
| 6. | Hydraulic Testing | 14 |
| 6.1 | Data Analysis | 14 |
| 6.2 | Discussion of Test Results | 14 |
| 7. | Groundwater and Surface Water Chemistry | 16 |
| 8. | Conceptual Hydrogeology | 21 |
| 8.1 | Local recharge and discharge areas | 22 |
| 8.2 | Local groundwater occurrence | 23 |
| 8.3 | Corunna Downs mining area surface water features | 25 |
| 9. | Assessment of Potential Impacts | 26 |
| 9.1 | Numerical Modelling of Mining Area | 26 |
| 9.2 | Drawdown and Radius of Influence | 28 |
| 9.3 | Groundwater Dependant Ecosystems | 29 |
| 9.4 | Other Groundwater Users | 32 |
| 9.5 | Groundwater Quality | 32 |
| 10. | Operating Strategy | 32 |
| 11. | Summary/Recommendations | 32 |
| 12. | References | 34 |

LIST OF TABLES

| Table 3-1: Alignment stratigraphy | 8 |
|---|------------|
| Table 5-1: Details of regulatory approvals | 11 |
| Table 5-2: Summary of Pilot Bores | 12 |
| Table 5-3: Summary of Production Bores | 13 |
| Table 6-1: Summary of Pumping Test Details | 15 |
| Table 6-2: Summary of Pumping Test Results | 16 |
| Table 9-1: Mine Site Operational Abstraction Rates | 26 |
| Table 9-2: Summary of Modelled Operational Drawdown for Road Construction | 28 |
| Table 9-3: Summary of surface water feature details | 29 |
| Table 9-4: Drawdown estimates for key environmental locations, at specified time steps | 30 |
| LIST OF FIGURES | |
| Figure 1-1: Location of proposed haul road alignment | 2 |
| Figure 1-2: Corunna Downs hydrogeological investigation – drilling target locations | 3 |
| Figure 2-1: Marble Bar mean monthly rainfall and temperature | 5 |
| Figure 2-2: Marble Bar annual rainfall | 5 |
| Figure 2-3: Marble Bar mean monthly rainfall and evaporation | 6 |
| Figure 2-4: Regional surface water catchments | 7 |
| Figure 3-1: Cross section of regional geology (see Figure 4-1 for section location). | 8 |
| Figure 4-1: Simplified geological map of the Corunna Downs area | 10 |
| Figure 7-1: Schoeller diagram illustrating the range of major ion concentration in groundwater and the ionic concentration of surface water samples collected from the Corunna Downs mining area on 24/07/2017. | |
| Figure 7-2: Piper diagram of surface water (blue) and groundwater (red) samples from Corunna Down area. The green symbol represents rainfall. | S |
| Figure 7-3: Major ion chemistry – groundwater samples | 19 |
| Figure 7-4: Major ion chemistry – surface water (pools) | 20 |
| Figure 8-1: Approximately south to north, hydrogeological long section along the project alignment (B looking west) and west to east section (C to C', looking north) | to B 21 |
| Figure 8-2: Groundwater hydrograph showing overall groundwater level recession, with occasional recharge events. | 23 |
| Figure 8-3: Conceptual hydrogeology of Corunna Downs area showing surface water pond locations | s. 24 |
| Figure 8-4: Conceptual mode of occurrence of surface features located around the Corunna Downs mining area | 25 |
| Figure 9-1: Drawdown estimate at end of the life of mine (LOM) | 27 |
| Figure 9-2: Location of Possible Groundwater Dependant Ecosystems | 31 |

APPENDICES

Appendix A Groundwater Licences

Appendix B Type lithology examples

Appendix C Drillhole Graphic Logs
Appendix D Step Rate Test Results

Appendix E Constant Rate Pumping Test Results

Appendix F Water Chemistry Database and Laboratory Analysis Reports

Appendix G Numerical Model Summary

Appendix H Operating Strategy

1. Introduction

This H2 Hydrogeological Assessment report has been prepared by MWH (now part of Stantec) to document field work and findings from hydrogeological investigations carried out on behalf of Atlas Iron Limited (Atlas), for the purpose of identifying groundwater resources for use in road construction and mining operations. The field work was carried out in two field campaigns between April and August 2017, and in November 2017.

The report is to be submitted to the Department of Water and Environmental Regulation (DWER) in support of an application for a 5C Licence to Take Water under the Rights in Water and Irrigation Act 1914 (RIWI Act), for the purpose of abstracting groundwater for road construction and mining operations.

The groundwater investigations included the drilling of, construction and hydraulic testing of 12 pilot drill holes and 8 production bores.

1.1 Background

The Corunna Downs mining project (Corunna) is located approximately 237 km by road, southeast of Port Hedland and 33 km south southwest from Marble Bar (Figure 1-1). The project has the potential to deliver 4 Mtpa of lump and fines direct shipping iron ore (DSO) over an initial mine life of five to six years. In order to achieve this target a 22 km public road upgrade and 13 km mine access road construction is required.

Groundwater abstraction is currently authorised under two 5C licences to take water, GWL184565(1) for 100,000 kL/annum for road construction purposes, and GWL176960(4) for 100,000 kL/annum construction, campsite and potable water supply purposes (Appendix 1). In March 2017, Atlas applied to amend GWL176960, seeking 1,100,000 kL/annum for all mining purposes on the Corunna mining leases. DWER specified that additional information was required before they could assess the application:

- H2 basic hydrogeological assessment including drilling and test pumping
- Groundwater Operating Strategy

This H2 report constitutes the reporting component of DWERs request for additional information. (Figure 1-2).

1.1 Scope of Work

The overarching objective of the groundwater investigation was to identify groundwater resources and construct production bores that can provide a sustainable groundwater resource for the six year life of the Atlas Iron Corunna Downs project.

The specific tasks completed to meet the objectives include:

- Management and supervision of hydrogeological drilling and aquifer testing, including:
 - Drilling of twelve (12) water exploration pilot holes located along the proposed Corunna Downs haul road and pit areas;
 - Drilling, construction and testing of eight (8) production bores along the proposed haul road and within the ROM areas; and
- Hydrogeological reporting in support for an application for a 5C licence to abstract groundwater.

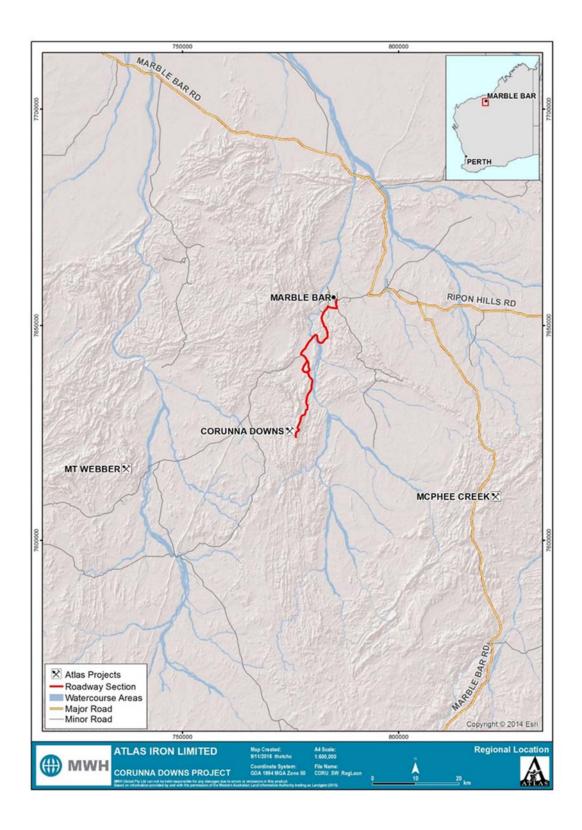


Figure 1-1: Location of proposed haul road alignment

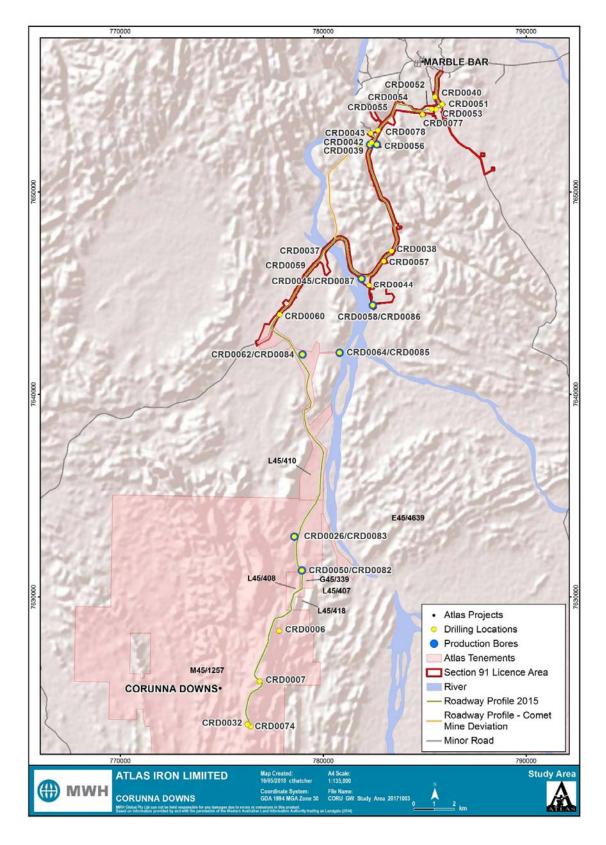


Figure 1-2: Corunna Downs hydrogeological investigation – drilling target locations

1.3 Previous work

Stantec completed a review of the water supply targets for the Section 91 area of the proposed haul road (MWH, 2017). This comprised a desktop study to review each proposed exploration drilling location and provide a location ranking based on geological lithology, geological structure, likely groundwater recharge characteristics, and drill pad access.

The study supported the proposed hydrogeological drilling targets provided by Atlas and characterised them as logical and well-founded based on the available knowledge base. Fractured rock aquifers (basalt, chert and dolerite dykes) were identified to be the primary targets for groundwater exploration.

2. Physical setting

1.2 Topography

The prevalent landforms around the project area are steep-sided ridges and hills (Figure 2-1). They are associated with outcrops of greenstone, chert and, in some locations, sandstone and dolomite.

Steep slopes are associated with ridges formed by hard rock outcrops comprising predominantly banded iron lithologies. Well-developed drainage lines incised into the ridge areas form gorges and gullies. Away from the ridge areas, ground surface changes to gentle to undulating slope surfaces in valley areas and river floodplains, typically underlain by basalt.



Figure 2-1: Example of the landscape in the Corunna Downs area

2.1 Climate

The climate of the Pilbara region is classified as semi-arid to arid and is characterised by hot summers and warm winters. The area experiences a climate of extremes, where severe droughts and major floods can occur at close intervals. Tropical cyclones can occur between January and April, bringing sporadic, high-intensity, rainfall events.

The closest Bureau of Meteorology (BOM) weather station to the project is located at Marble Bar (station number 004106, previously station number 004020), located 25 km to the northeast (BOM 2016a). During the summer months of November to February, the mean maximum temperature for Marble Bar is 40.7 °C and the mean minimum temperature is 25.3 °C (Figure 2-1). Marble Bar averages 104 days above 40°C per year (BOM 2016a). During the winter months of June to August, the mean maximum temperature for Marble Bar is 27.8 °C and the mean minimum temperature is 12.7 °C (BOM 2016a)

Annual rainfall at Marble Bar is shown as the red bar in Figure 2-2. Rainfall within the Project area can be highly localised and unpredictable with substantial fluctuations occurring from year to year. Mean annual rainfall is around 362 mm, with minimum and maximum annual rainfall of 71 mm (1924) and 798 mm (1980), respectively. Approximately 70% of the rainfall in the area occurs from December to March, and is generally associated with the passage of tropical cyclones. Most of the rainfall events occur as scattered thunderstorms, producing heavy localised falls over short periods. Tropical lows, usually originating off the Pilbara coast, can also bring widespread rain to the region.

Average annual pan evaporation (based on Marble Bar evaporation data) is around 3,300 mm/year, which is an order of magnitude higher than the average annual rainfall (Figure 2-3).

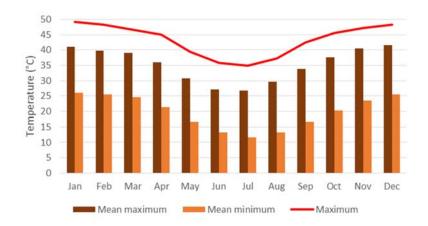


Figure 2-1: Marble Bar mean monthly rainfall and temperature

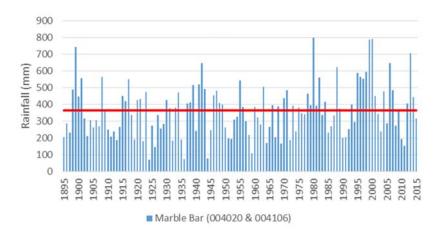


Figure 2-2: Marble Bar annual rainfall

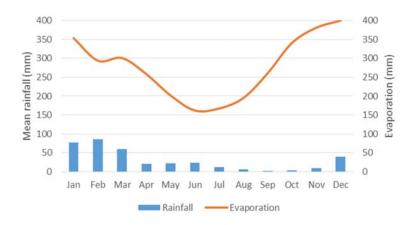


Figure 2-3: Marble Bar mean monthly rainfall and evaporation

2.2 Catchments and Drainage

The Project area lies within the middle reaches of the Coongan River catchment which sits within the De Grey River Basin (Figure 2-4). The De Grey River Basin covers an area of 56,890 km² (Ruprecht et al. 2000) with its major tributaries being the Strelley, Shaw, Coongan, Oakover and Nullagine Rivers. The Coongan River system has a total catchment area of around 7,090 km² and lies between the Chichester Ranges in the south and minor ranges on the west and east. The Coongan River has a number of tributaries, including: Budjen Creek, Triberlar Creek, Boobina Creek, Emu Creek and Camel Creek. The Coongan River joins the De Grey River at Mulyie Pool, about 41 km upstream of the confluence with the Shaw River.

Rivers in the Pilbara region are typically ephemeral in nature; however, surface water is present throughout the year in pools along the main rivers and creeks. These pools are most likely surface expressions groundwater within the alluvium.

The local catchments generally drain from west to east across the Project area towards the Coongan River. Gradients along the elevated areas are steep, reducing to flatter gradients along the valley floor. Incised drainage paths along the ridge and hill areas within the Project area are indicative of high flows occurring within well-defined channels. The flat areas spreading out from the ridges provide evidence of sheet flow with lower gradient drainage paths. In these areas finer material settles out as flow energy decreases after a rainfall event.

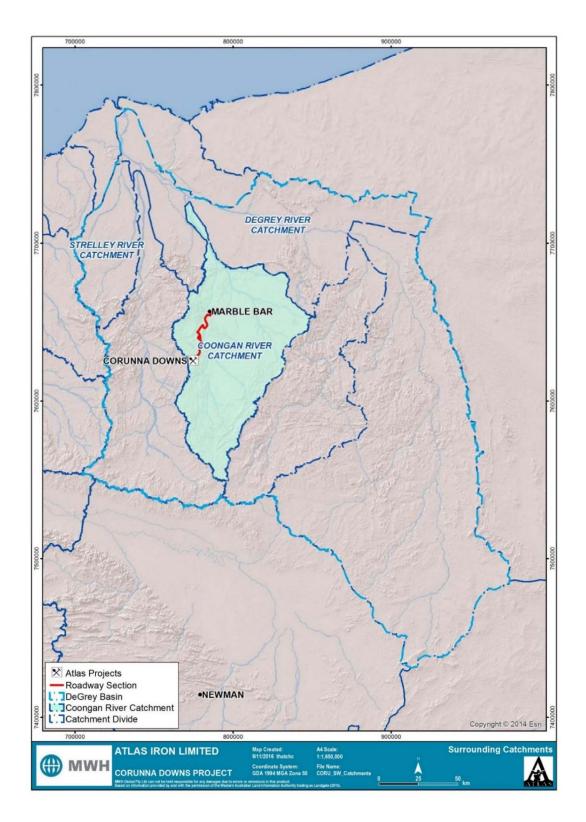


Figure 2-4: Regional surface water catchments

3. Regional Geology

The Corunna Downs Project and proposed haul road lie predominantly within Archaean greenstone belt rocks of the Coongan Syncline, located between the Shaw Batholith and Corunna Downs Batholith; all major structural units on the Pilbara Craton (Hickman 2010, and Hickman and Lipple, 1978).

The key formations underlying the haul road alignment belong to the Pilbara, De Grey and Mount Bruce Supergroups as presented in Table 3-1.

Table 3-1: Alignment stratigraphy

| Supergroup | Group | Formation | Lithologies | | | | |
|-------------|-------------|------------------|--|--|--|--|--|
| Mount Bruce | Fortescue | Hardey | Sedimentary and felsic volcanics, local intrusives | | | | |
| | | Mount Roe Basalt | Basaltic volcanic rock, local voclaniclastic and siliciclastic rocks | | | | |
| De Gray | Gorge Creek | Cleaverville | Metamorphosed banded iron formation (BIF), sandstone, siltstone and shale, chert and felsic volcaniclastic rocks | | | | |
| Pilbara | Warrawoona | Duffer | Metamorphosed felsic volcanic rock, local basalt, chert and felsic schist | | | | |

The rocks of the Pilbara and De Grey Supergroups have experienced four deformation periods resulting in a strongly and complexly folded terrain. The Mount Bruce Supergroup has experienced a single period of open folding. Faulting is extremely common.

The rocks of the Pilbara and De Grey Supergroups are affected by pervasive greenstone facies metamorphism, but rocks from lower structural levels have attained amphibolite facies.

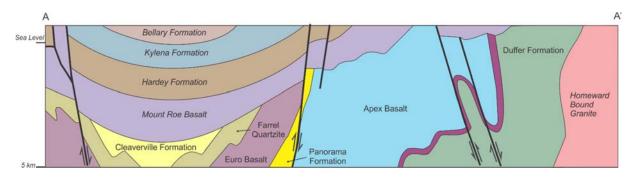


Figure 3-1: Cross section of regional geology (see Figure 4-1 for section location).

4. Regional Hydrogeology

The hydrogeology of the northern Pilbara is typified by faulted granitoid rocks and folded Archaean greenstone belt rocks, predominantly providing a fractured rock setting in which groundwater storage and transmission is structurally controlled. Aquifers types range from unconfined to confined, with the fractured rock setting typically unconfined to semi confined. Groundwater is predominantly recharged on the regional scale by episodic intense tropical low and cyclonic rainfall events, plus intense thunderstorm events on the local scale.

Groundwater may also occur in the upper weathered zones of all rocktypes, and where storage and transmission may be enhanced in secondary porosity associated with extensive weathering along zones, geological contacts and quartz veining.

The regional groundwater likely flows to the north consistent with the drainage direction of the major surface drainage features (rivers), while local groundwater flow directions will be driven by the interaction of topography, the elevation of the water table, and the interconnectivity of the structural elements of the rock mass.

Groundwater quality is likely to be fresh to brackish, but is directly coupled with recharge processes and the history of the water along individual flowlines, such that the presence of saline water cannot be discounted.

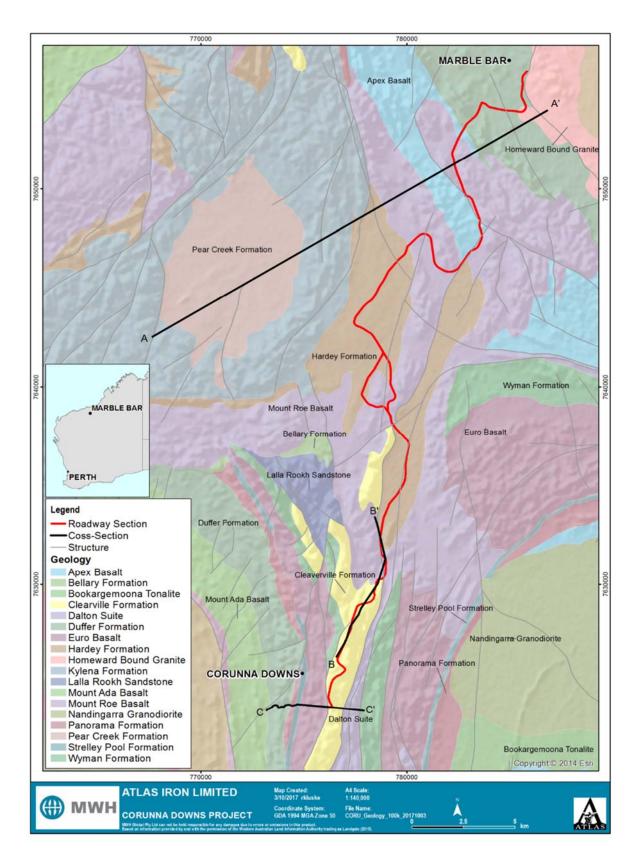


Figure 4-1: Simplified geological map of the Corunna Downs area

5. Drilling investigations

Groundwater exploration and production bore drilling was undertaken in the Corunna Downs study area between April and May 2017, and again in November 2017. Drillhole locations were selected by Atlas Pty Ltd and were reviewed by MWH (now part of Stantec). Drilling locations targeted, fractures (shear or fault zones), geological contact zones, areas of alluvial or calcrete cover, in relatively close proximity to drainage lines to provide recharge potential. Pilot holes were initially drilled before the final locations of the production bores were chosen.

Drilling was undertaken by drilling contractor Foraco using a KWL 700 drilling rig. The drilling was carried out under Licences to Construct or Alter Wells (Table 5-1), approved by the Department of Water in accordance with the Rights in Water and Irrigation Act 1914.

Table 5-1: Details of regulatory approvals

| Licence | Approval Date | Expiry Date |
|--------------|-------------------|-------------------|
| CAW183385(1) | 22 September 2016 | 19 September 2018 |
| CAW184294(1) | 21 April 2017 | 31 January 2019 |

The intersected geology was entirely consistent with the anticipated lithologies (Table 3-1). Photos of type examples are illustrated in the Appendix A.

5.1 Pilot Bores

All pilot bores were pre-collared to 6 m, drilling with a 190 mm tri-cone drill bit, and installing a 6 m length of ND150 mm ID uPVC surface casing, secured in place with AB foam. Each hole was then drilled open hole with conventional rotary air, down-the-hole hammer techniques, utilising a 6" (152.4 mm) bit on a 5" (127 mm) hammer. After drilling, the bore was airlifted for approximately 2 hours to determine water quality and discharge yield. **Table 5-2** provides a summary of pilot bore drilling, while summary drill hole logs are presented in Appendix C.

5.2 Production Bores

All production bores were initially drilled to 6 mbgl with a 305 mm (12") tri-cone bit, then reamed out with a 380mm (15") bit before installing a 300mm (12") steel surface collar, and cement grouting the annulus. The holes were then drilled with conventional rotary air, down-the-hole hammer techniques to depth utilising a 254mm (10") bit. The holes were completed with blank and slotted 8" Class 18 PVC casing and gravel packed to within a metre of the surface, where a bentonite seal was installed. **Table 5-3** provides a summary of production bore details, while summary drill hole logs are presented in Appendix C.

Table 5-2: Summary of Pilot Bores

| Hole ID | Date started | Date completed | Easting | Northing | Total depth (mbgl) | Water Strike Depths (mbgl) | Lithology/Formation | Max airlift yield whilst drilling (L/s) | На | EC (µS/cm) |
|---------|--------------|-------------------|---------|----------|--------------------------|-------------------------------|--------------------------------------|--|------|---------------|
| CRD0038 | 9/04/2017 | 10/04/2017 | 783368 | 7647094 | 60 | From 19 | Weathered granite and basalt | 0.5 | 8.1 | 310.0 |
| CRD0057 | 10/04/2017 | 10/04/2017 | 782993 | 7646586 | 72 | N/A | | 0.0 | dry | dry |
| CRD0044 | 11/04/2017 | 11/04/2017 | 782273 | 7645380 | 66 | 5 16 | Alluvials Weathered Basalt | 2.6 | 7.65 | 2,670 |
| CRD0058 | 11/04/2017 | 12/04/2017 | 782443 | 7644390 | 66 | 10 | Weathered Basalt | 1.0 - 1.5 | 7.37 | 2,965 |
| CRD0045 | 12/04/2017 | 13/04/2017 | 781895 | 7645717 | 72 | 16 46 | Weathered Basalt Weathered Basalt | 4.5 | 8.01 | 1,003 |
| CRD0078 | 9/05/2017 | 9/05/2017 | 782700 | 7653040 | 84 | 34 | Duffer Formation | 0.8 | NS | NS |
| CRD0043 | 4/11/2017 | 4/11/2017 | 782275 | 7652340 | 84 | 4 | Weathered Basalt | 2.2 | NS | 1,136 |
| CRD0039 | 5/11/2017 | 6/11/2017 | 782368 | 7652870 | 102 | 10 | Weathered Basalt | 4.8 | NS | 1,118 |
| CRD0056 | 6/11/2017 | 7/11/2017 | 782732 | 7652279 | 102 | 30 | Weathered Basalt | 2.5 | NS | 1,209 |
| CRD0040 | 9/11/2017 | 10/11/2017 | 785602 | 7654390 | 102 | 13 | Fractured and Weathered Basalt | 1.6 | NS | 1,894 |
| CRD0051 | 10/11/2017 | 11/11/2017 | 785884 | 7654307 | 102 | 24 | Fractured and Weathered Basalt | 1.8 | NS | 1,961 |
| CRD0081 | 11/11/2017 | 12/11/2017 | 785348 | 7654094 | 102 | 24 | Weathered Basalt | 0.3 | NS | 1,216 |

Notes: mbgl = metres below ground level, NS = Not Sampled

Table 5-3: Summary of Production Bores

| Hole ID | Date started | Date finish | Easting | Northing | Depth (m) | Screened Interval (mbgl) | Water Strike Depths (mbgl) | Lithology/Formation | Max airlift yield whilst drilling (L/s) | рН | EC (µS/cm) |
|---------|-----------------|-------------|---------|----------|--------------|--------------------------------|----------------------------------|---|---|------|---------------|
| CRD0082 | 13/04/2017 | 17/04/2017 | 778953 | 7631289 | 88 | 10 to 88 | 6 33 approx46 74 to 82 | Hardey Formation Weathered Basalt Weathered Basalt Weathered Basalt | 50-70 (Dev. 35) | 7.2 | 850 |
| CRD0083 | 17/04/2017 | 23/04/2017 | 778579 | 7632984 | 82 | 6 to 78 | 20 approx. 40 | Weathered Basalt, quartz vein Weathered Basalt | 18.8 – 20 | 7.79 | 763.1 |
| CRD0084 | 24/04/2017 | 27/04/2017 | 778981 | 7641952 | 64 | 6 to 60 | 24 26 | Weathered Basalt Fractured Zone | 2.9 – 5.5 | 7.94 | 1,330 |
| CRD0085 | 27/04/2017 | 30/04/2017 | 780809 | 7642040 | 64 | 6 to 64 | 14 40 | Weathered Basalt Weathered Basalt | 4.9 | 7.88 | 1,454 |
| CRD0086 | 1/05/2017 | 4/05/2017 | 782443 | 7644390 | 70 | 4 to 70 | 11 60 | Weathered Basalt Weathered Basalt | 3 | 8.16 | 2,800 |
| CRD0087 | 5/05/2017 | 7/05/2017 | 781895 | 7645717 | 64 | 4 to 64 | 8 38 | Weathered Basalt Weathered Basalt | 15 (Dev. 6.8) | 8.01 | 947 |
| CRD0088 | 14/11/2017 | 17/11/2017 | 782285 | 7652335 | 102 | 9 to 99 | 24 to 98 | Weathered and Fractured Basalt | 10.3 | 7.85 | 880 |
| CRD0089 | 18/11/2017 | 21/11/2017 | 782719 | 7652280 | 100 | 12.3 to 96.3 | 26 to 94 | Weathered and Fractured Basalt | 10.3 | 7.79 | 925 |

Notes: mbgl = metres below ground level,

6. Hydraulic Testing

Hydraulic testing (test pumping) was carried out to assess the availability of water for the proposed development, to determine hydraulic properties of the geological materials intersected by drilling, and assess the potential long-term impacts from the proposed abstraction on the source aquifers, the environment, and other groundwater users. The test pumping was undertaken in accordance with Australian Standards (AS 2368–1990 Test pumping of water wells).

The testing was carried out by Airwell Group Pty Ltd on all new production bores. Testing comprised a calibration test, a step rate test (four 100 minute steps at increasing rates), a 72 hour constant rate test (CRT), and a recovery test. Test details are summarised in Table 6-1.

The pump used was a Shakti QF100 (156 mm diameter). The flow rate was measured with two Danfoss EM-Flowmeters and controlled by a VSD (variable speed drive) system. Water level measurements were collected both manually, and with Druck 1930 vented pressure transducer loggers which were installed in the pumping bore and adjacent monitoring bore. The groundwater level data was recorded manually and also via a SCADA software system which enabled real time viewing of flow rate, water level, electrical conductivity and temperature data.

Step rate test data was analysed with the Beirschenk & Wilson method utilising in-house spreadsheets, while CRT and Recovery Test results were analysed both manually (spreadsheet based), and using proprietary hydraulic test analysis software AQTESOLV Pro Version 4.5.002.

6.1 Data Analysis

Analysis of CRT data was often confounded by the non-standard drawdown response in the fractured rock settings, where the basic assumptions of classical hydraulic test data analysis methods, including efficient hydraulic connection between pumping bore and monitoring bore, do not apply. When this occurs, derived hydraulic properties such a transmissivity and specific yield must be treated with appropriate caution, depending upon the specific purpose for which they are used. Nevertheless, the analysis methods of Theis, Cooper Jacob and Moench were applied assuming unconfined conditions. Analysis using various fractured aquifer analysis techniques was unsuccessful due to the failure of the solutions to converge.

Individual step rate test results are presented in Appendix C. CRT test results and interpretations are provided in Appendix D, while a summary of the pumping test results is present in Table 6-2.

6.2 Discussion of Test Results

Referring to the individual pumping test drawdown curves presented in Appendix D and Table 6-2, the key findings from the hydraulic test work are as follows:

- The production bores are all hydraulically inefficient and none will be able to maintain the pumping rates selected for the CRTs. This is common when hydraulically testing bores in fractured rock settings, so operational abstraction rates will typically be lower than the CRT rates.
- Sustainability at any selected pumping rate for individual bores will be a function or balance between recharge (rainfall), available storage, and the rate of pumping. Accordingly the time of the year when the six month water supply is required will affect the operational sustainability of supply.

Table 6-1: Summary of Pumping Test Details

| Pumping Bore | Test Dates | Static water level (mbtoc) | Pump setting depth (mbtoc) | Step Test Rates (L/s) | Constant Rate (L/s) | Total Drawdown in pumping bore (m) | Monitoring Bore | Monitoring Bore Static water level (mbtoc) | Drawdown observed (m) | Distance from pumping bore (m) | Time for 95% Recovery (mins) |
|-----------------|--------------------------|-------------------------------------|-------------------------------------|-----------------------------|---------------------------|--|--|---|-----------------------------|--------------------------------|------------------------------------|
| CRD0082 | 27/06/2017 03/07/2017 | 4.65 | 52.05 | 10, 15, 20, 25 | 25 | 6.1 | CRD0050 No_ID CRD0048 | 4.1 2.67 2.09 | 3.6 NR NR | 10 700 1000 | 2800 |
| CRD0083 | 05/07/2017 09/07/2017 | 3 | 42.05 | 10, 15, 20, 25 | 20 | 13.3 | CRD0026 CRD0071 CRD0027 CRD0050 | 2.94 2.81 4.3 3.9 | 10.3 1.64 0.06 0.0 | 8.35 432 1162 1729 | 390 mins to 89% |
| CRD0084 | 10/07/2017 16/07/2017 | 4.31 | 41.735 | 3, 4, 5, 6 | 6 | 14.9 | CRD0062 CRD0064 | 4.25 7.83 | 14.1 0.0 | 10 1750 | 20 |
| CRD0085 | 16/07/2017 21/07/2017 | NR | 47.05 | 3, 5, 7, 9 | 5 | 16.6 | CRD0064 | 9.74 | 2.03 | 10 | 66 |
| CRD0086 | 23/07/2017 27/07/2017 | 3.5 | 61.83 | 2, 3, 4, 5 | 4 | 8.14 | CRD0058 | 3 | 0.87 | 8 | 107 |
| CRD0087 | 28/07/2017 | 4.86 | 51.82 | 10, 15, 20, 25 | 15 | 31.61 | CRD0044 | 2.91 | 25.53 | 700 | 94 % 15 mins 95% 110 mins |
| CRD0088 | 19/11/2017 23/11/2017 | 6.79 | 49.8 | 4, 8, 12, 16 | 12 | 16.2 | CRD0039 | 5.73 | 1.5 | 11 | 2 |
| CRD0089 | 24/11/2017 27/11/2017 | 11.47 | 59.8 | 5, 10, 15, 20 | 12 | 21.5 | CRD0056 | 10.8 | 15.5 | 13 | NA, 85% in 360 mins |

Notes: mbtoc = metres below top of casing. Mins = minutes.

- Analytically estimating the drawdowns for individual production wells utilising their derived well equations, will be inaccurate due to the inability of honouring the aquifer assumptions required for classical hydraulic test analysis, in fractured rock aquifers.
- All bores will require close operational monitoring to identify declines in bore performance. If drawdown in a particular bore becomes critical (approaches pump intake level), then abstraction duty should be given to another production bore. Alternation of production bores will be necessary during the duration of the haul road construction.

Table 6-2: Summary of Pumping Test Results

| Pumped Bore | Well Efficiency* (%) | CRT Pumping Rate (L/s) | Transmissivity (m²/day) | Drawdown response in terms of classical drawdown curve analysis | | | | |
|----------------|----------------------------|------------------------------|----------------------------|---|--|--|--|--|
| CRD0082 | 53 (25 L/s) | 25 | 190 to 210 | Poor fit, strong strip aquifer (strip) response | | | | |
| CRD0083 | 22 (25 L/s) | 20 | 200 to 220 | Poor fit, delayed yield then strip response | | | | |
| CRD0084 | 9 (6L/s) | 6 | 47 to 237 | Poor fit, delayed yield then strip response | | | | |
| CRD0085 | 20 (7 L/s) | 5 | 100 to 165 | Poor fit, delayed yield then strip response | | | | |
| CRD0086 | 9 (5 L/s) | 4 | 395 | Very noisy data, poor fit, possible compaction | | | | |
| CRD0087 | 28 (25 L/s) | 15 | 593 | Poor fit, strong strip aquifer (strip) response | | | | |
| CRD0088 | 15 (16 L/s) | 12 | 300 to 440 | Reasonable fit | | | | |
| CRD0089 | 26 (20 L/s) | 12 | 22 to 54 | Poor fit, delayed yield then strip response | | | | |

Notes: * Well efficiency for highest interpretable step test pumping rate (flow rate in brackets).

7. Groundwater and Surface Water Chemistry

Groundwater samples were collected during development of each drill hole and also during test pumping. The samples were then submitted to MPL Laboratories for major ions and trace metals analysis. The results and laboratory analytical reports are presented in Appendix F.

Groundwater in the study area is fresh to brackish, with total dissolved solids (TDS) ranging from 410 to 1,800 mg/L. The key major ions include sodium (43 to 630 mg/L), chloride (19 to 500 mg/L), and bicarbonate (300 to 700 mg/L). Potassium concentrations are relatively low (0.5 to 2.5 mg/L).

With the exception of fluoride, arsenic, manganese and nickel, all groundwater sample concentrations for analytes listed in the Australian Drinking Water Guidelines (NHMRC, NRMMC, 2011) are below guideline concentrations.

Fluoride was detected at or above the guideline concentration of 1.5 mg/L in CRD0086 on 3 samples collected to date (maximum concentration 2.0 mg/L), and in CRD0058 once at 1.8 mg/L.

Arsenic was detected in CRD0086 on 3 occasions (maximum concentration 0.014 mg/L), twice in CRD0040 (0.01 mg/L), and once in CRD0038 (0.013 mg/L), CRD0058 ((0.012 mg/L) and CRD0073 (0.010 mg/L).

Groundwater and Surface Water Chemistry

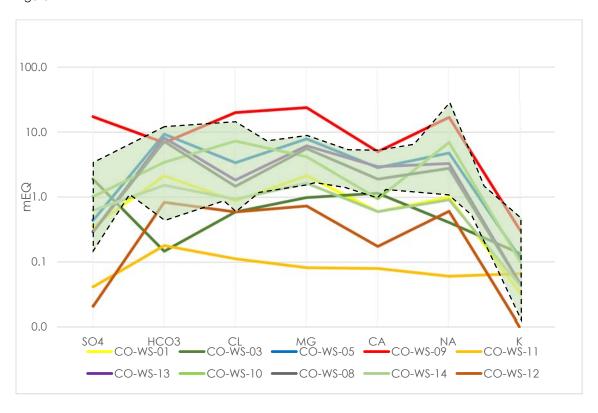
May 16, 2018

Manganese was detected twice in CRD0003 (maximum 0.87 mg/L), and once in CDRC0334 (4.2 mg/L), CRD0027 (1.4 mg/L), CRD0031 (3.2 mg/L), and CRD0033 (0.96 mg/L).

Nickel was detected in in CRD0062 (0.410 mg/L) and CRD0071 (0.022 mg/L).

CRD0086 is the only production bore in which criteria were exceeded and given the groundwater will be used for road construction, the exceedances are not considered to be a risk to livestock or the environment.

Surface water TDS ranges from 33 to 2,800 mg/L, and is generally characterised by the same major ions, although in differing relative concentrations. A Schoeller diagram illustrating the relative major ion concentrations of surface water compared to the range observed in groundwater is shown in Figure 7-1



Range of groundwater ionic concentrations from 39 samples

Figure 7-1: Schoeller diagram illustrating the range of major ion concentration in groundwater and the ionic concentration of surface water samples collected from the Corunna Downs mining area on 24/07/2017.

Figure 7-2 presents a Piper plot of all available groundwater chemistry data currently available from the project site. Reference to the figure shows a broad distribution of groundwater types (hydrochemical facies) with the dominant anionic species being bicarbonate (bicarbonate type water) but with no overwhelmingly dominant cation. The broad distribution indicates a broad range of histories for the individual groundwater samples, with mixing of groundwaters with differing

Groundwater and Surface Water Chemistry

May 16, 2018

histories of aquifer residence time or exposure to recent recharge, and interaction with differing rock types.

The groundwater samples indicate marginal sodium enrichment in northerly direction accompanied also by slight chloride enrichment suggesting groundwater chemistry evolution from south to north as evidenced in spatial distribution of hydrochemical signatures presented in Figure 7-3 and Figure 7-4 for groundwater and surface water respectively. The total dissolved solid concentrations also have a tendency to increase in northerly direction.

Several samples (e.g. CRD0003, CRD0031, and CRD0041) indicate sulphate enrichment (Figure 7-3) at the expense of bicarbonate and chloride possibly suggesting the presence of sulphide oxidation in parts of the aquifer system.

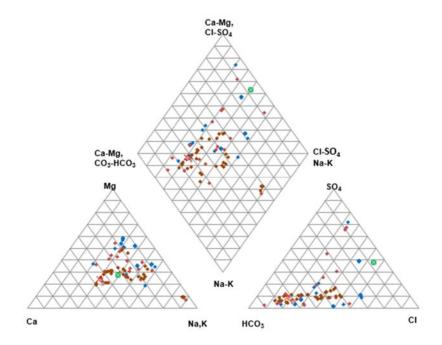


Figure 7-2: Piper diagram of surface water (blue) and groundwater (red) samples from Corunna Downs area. The green symbol represents rainfall.

Hydrochemical signatures of surface water samples are inconsistent with the groundwater samples (Figure 7-2 and Figure 7-4), suggesting that in surface water bodies, the water is affected by evapoconcentration and biological processes.

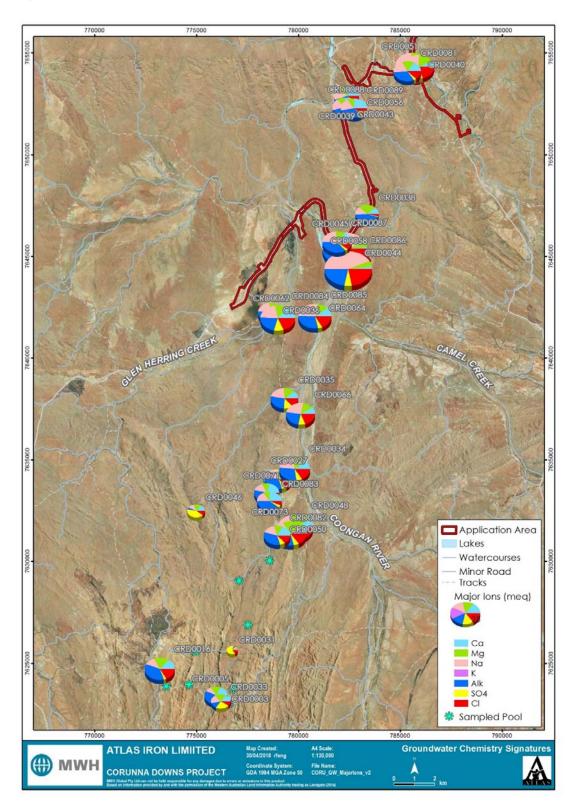


Figure 7-3: Major ion chemistry – groundwater samples

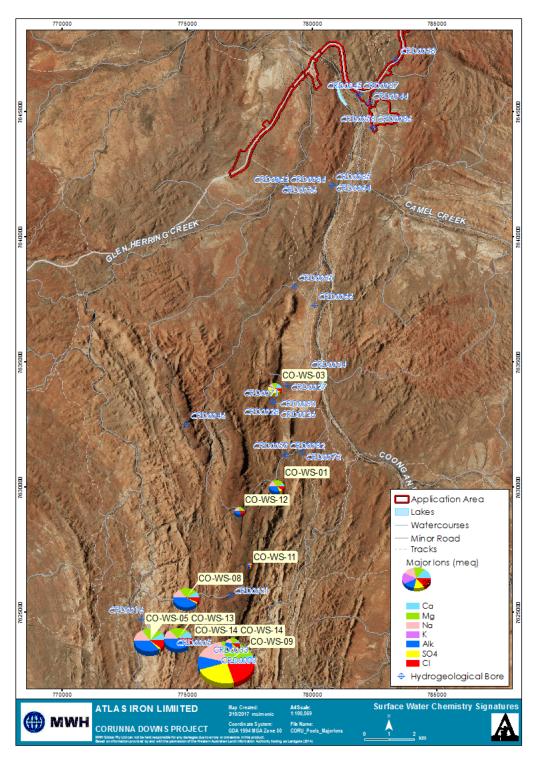


Figure 7-4: Major ion chemistry – surface water (pools)

8. Conceptual Hydrogeology

Conceptually, the hydrogeological setting for the region comprises predominantly fractured rock within a package of crystalline and sedimentary rocks that have been exposed to significant structural deformation and metamorphism. With the exception of weathered and mineralised zones, groundwater storage and transmission principally occurs in joints, fractures and other defects in the rock mass. Colluvial and alluvial deposits may have developed in the vicinity of high relief or major drainage features, although the amount of groundwater stored in such settings is thought to be minor. The highly faulted nature of the fractured rock setting may hydraulically compartmentalise individual blocks of rock mass such that the phreatic surface (water table) may not form a continuum across geological boundaries.

Figure 8-1 presents two geological cross sections that provide hydrogeological context for project. The locations of the cross sections are provided on Figure 4-1, a regional geological base-map showing the extent of the project within a geological context.

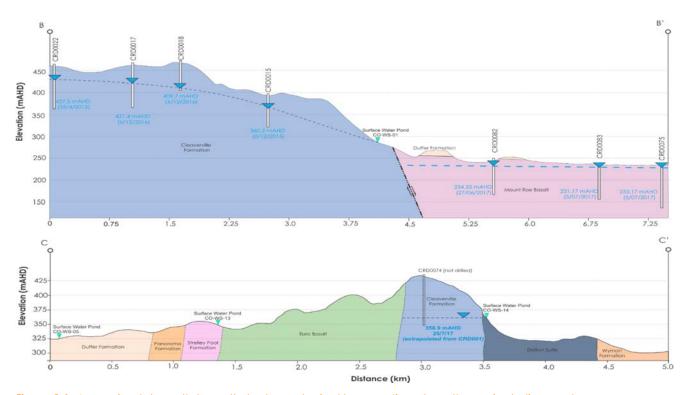


Figure 8-1: Approximately south to north, hydrogeological long section along the project alignment (B to B', looking west) and west to east section (C to C', looking north)

Reference to Figure 8-1 shows a number of hydrogeological concepts thought to active in the study area:

• A northerly water table gradient within the Cleaverville Formation (banded iron formation) groundwater flow direction (Section B to B")

May 16, 2018

- Compartmentalisation at the fault separating the Cleaverville Formation (Cleaverville) from the Mount Roe Basalt, such that saturated conditions exist within Cleaverville causing groundwater to discharge where the water table daylights against the fault, conceptually overflowing into the different hydrogeological domain within the Mt Roe Basalt.
- Groundwater levels within the Mt Roe Basalt being uncoupled with levels in the Cleaverville, and constrained by discharge processes elsewhere. Accordingly transient groundwater levels are a balance between recharge and discharge processes, with a primary constraint being the topographic level of the ground surface.

Groundwater has been classified into two key zones for the purpose of this study. The zones are separated based on groundwater elevation and hydraulic connection, as follows:

- Corunna Mining area (CORU): Groundwater exists on the elevated Corunna Down mining area plateau within the Cleaverville Formation and adjacent igneous intrusions. Groundwater level ranges between 430 to 360 mAHD (Figure 8-1 and Figure 8-3) and TDS ranges from 280 to 710 mg/L.
- Coongan River Valley (CRV): Groundwater is hosted within alluvial sediments and fractured Mount Roe Basalt. Groundwater levels range from 230 to 190 mAHD with a hydraulic gradient of 0.0037 which follows the Coongan River valley topography in a northerly direction. TDS ranges from 290 to 1,800 mg/L, the higher values are a result increased evapotranspiration of shallow groundwater and/or mixing with older groundwater.

8.1 Local recharge and discharge areas.

Groundwater recharge across the study area will occur primarily during and after intense rainfall events, which are generally associated with tropical lows and cyclonic weather systems. Regional groundwater levels typically rise significantly during and after these major recharge events, then commence recession until the next major recharge event, which may be some years later. Figure 8-2 shows the longest continual groundwater hydrograph available for the Corunna area, from CRD0003 at the southern extent of the project. The hydrograph shows a four year overall groundwater level recession, interspersed with occasional recharge events correlating with the wet season.

After rainfall, recharge will be enhanced along alluvial filled drainage lines and where surface water collects allowing infiltration to occur directly into outcropping or subcropping fractured rock.

During the wet season the Coongan River is likely to act as a losing system, contributing recharge to groundwater environment.

Groundwater discharge also occurs from a number of springs that are located around the Corunna Downs mining area plateau (Figure 8-3).

May 16, 2018

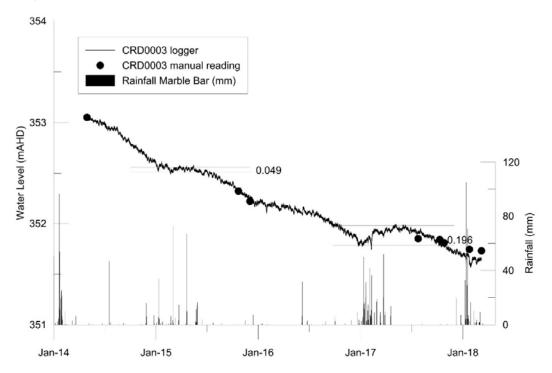


Figure 8-2: Groundwater hydrograph showing overall groundwater level recession, with occasional recharge events.

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8.2 Local groundwater occurrence

Drilling in the Coongan River valley was undertaken after the wet season when water levels were relatively high. The first groundwater strike was often encountered within the unconfined alluvial sediments. This aquifer is thought to support the vegetation that line the drainage lines, and is likely to exhibit a large seasonable variation.

Holes drilled further away from the drainage lines didn't strike groundwater until drilling proceeded into the underlying Mount Roe Basalt, the upper few metres were generally hard and dry with low apparent permeability. As drilling continued into the basalt, water strikes were noted at multiple depth horizons, and the groundwater level often rose 5-10 m after the initial water strike. Groundwater strikes in the Mount Roe basalt was generally associated with increases in quartz (silica) concentration, which may indicate the local lithology is actually more rhyodacitic (i.e. technically not the basalt), and the lithology is more conducive to secondary porosity than the surrounding basalt. Note silica-rich pillow lavas have been identified in Archaean basalts to the west of the Shaw Batholith (Lipple, date unknown).

Drilling and testing of the Mount Roe Basalt illustrated that hydraulic performance varied significantly within the rocktype with airlift yields ranging from 0 (dry) to 4.5 L/s being obtained from holes in the same formation. This highlights the importance of intersecting structural or secondary porosity features in fractured rock settings.

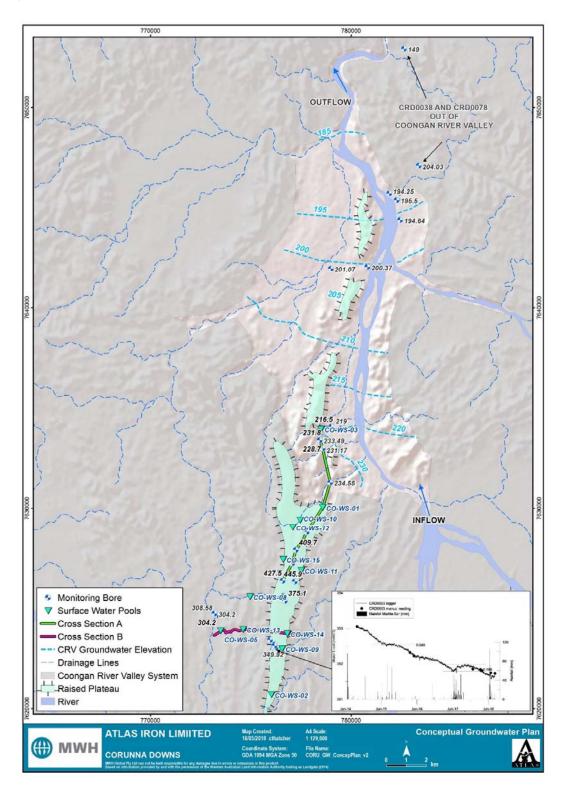


Figure 8-3: Conceptual hydrogeology of Corunna Downs area showing surface water pond locations

8.3 Corunna Downs mining area surface water features

A number of pools, seeps and springs are situated around the Corunna Downs mining area, the mode of occurrence of these features are likely from one of three mechanisms (Figure 8-4):

- 1. Where the local groundwater level intersects topography, mostly occurring in incised gullies where groundwater is shallow. This may also support groundwater dependant vegetation. The hydrochemical signature of these pools are dependent on the amount of evaporation that has occurred.
- 2. Infiltrated groundwater may discharge before reaching the saturated zone due to geological structures or perched aquifers. The short aquifer residence time minimises the effect of rock-water interaction on the hydrochemical signature of these surface water features.
- 3. Pools may exist where the morphology allows rainwater to collect in locations where evaporation is minimal. The hydrochemical signature of these surface water features will be similar to that of the regional groundwater, but may be modified by subsequent evaporation after discharge.

Analysis of hydrochemical signatures, elevation and aerial photography has been used to delineate the mode of occurrence of each pool, this is detailed below and in Table 9-3.

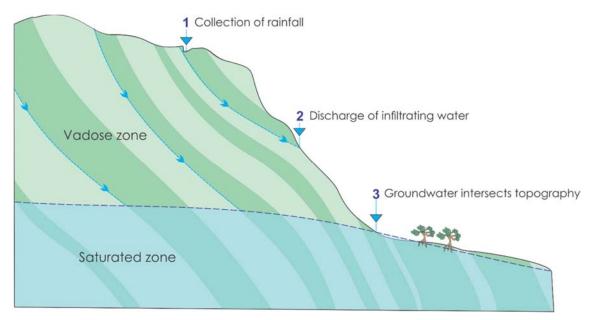


Figure 8-4: Conceptual mode of occurrence of surface features located around the Corunna Downs mining area

Assessment of Potential Impacts

9.1 Numerical Modelling of Mining Area

A simple numerical model was constructed to allow assessment of drawdown impacts due to pumping groundwater for site water requirements. The model was constructed in the numerical groundwater modelling code MODFLOW-2005 using the Upstream Weighting Package. The Groundwater Vistas graphical user interface (Version 6.96) was used to develop the model input files and process the model output. Technical details of the model are summarised in Appendix G.

The Class 1 model (Australian groundwater modelling guidelines, 2012) was constructed to incorporate structural elements such as major faults and key geological formations, in recognition of the fractured rock nature of the groundwater environment in the project area. Compartmentalisation is common in structurally complex terrains so the model gave some flexibility in exploring the implications of structure on groundwater movement and drawdown. The model domain has dimensions of 39 km (north to south) by 25.4 km (east to west), and has 3 layers with the top layer incorporating a digital terrain model of actual topography (Figure 9-1).

Key features of interest were incorporated into the model, such as abstraction bores and environmental features such as known rock pools and seepage locations (soaks). This was to allow assessment of the drawdown impacts that abstraction would have on these key features.

Model zone hydraulic properties in the key areas of interest were based upon actual parameters determined from hydraulic testing carried out at production bores installed during groundwater exploration programs. The model was calibrated to the available groundwater level data set, by adjusting until a reasonable calibration was achieved Appendix G.

The best calibrated model was used to evaluate various pumping schedules for the available production bores and two proposed production bore locations, with the objective of minimising the amount of drawdown at the end of the life of the mine (LoM), equivalent to 2190 days of mining, whilst meeting the mine's operational need for water over the LoM. The operational mine requires 30.5 L/s over its 6 year life. This is equivalent to an annual abstraction rate of 962,000 kL/annum.

The abstraction schedule that provided the least drawdown at sensitive locations is presented in Table 9-1

Table 9-1: Mine Site Operational Abstraction Rates

| Bore ID | Proposed Pumping Rate (L/s) |
|---------|-----------------------------------|
| CRD0071 | 8.0 |
| CRD0074 | 5.0 |
| CRD0082 | 5.0 |
| CRD0083 | 6.5 |
| CRD0084 | 3.0 |
| CRD0085 | 3.0 |

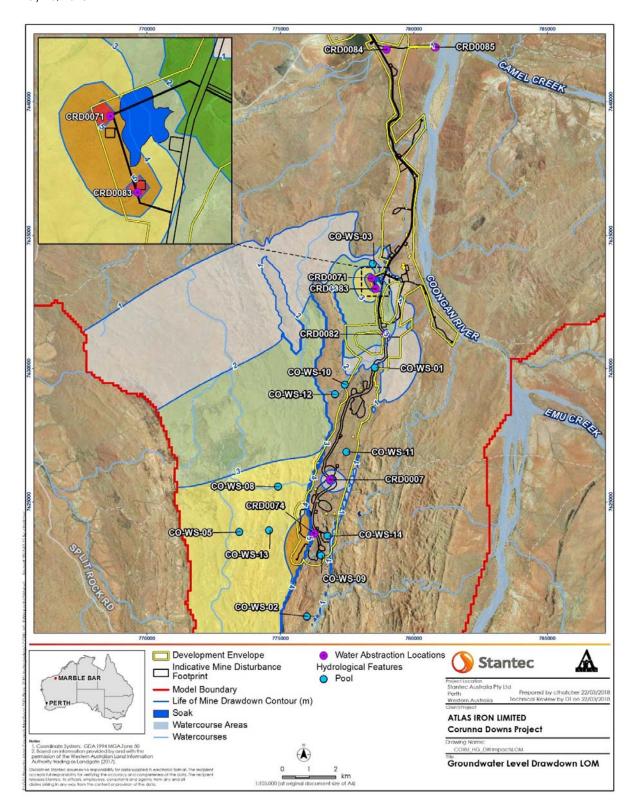


Figure 9-1: Drawdown estimate at end of the life of mine (LOM)

9.2 Drawdown and Radius of Influence

9.2.1 Mine Site Operational Water Supply

The maximum predicted drawdown at the end of LOM is presented on Figure 9-1, for the production schedule outlined in Table 9-1. This is the operational abstraction schedule, numerically modelled to minimise likely drawdown impacts at sensitive environmental locations (refer Section 9.3).

While drawdown contours in the southern cluster (associated with water abstraction at CRD0074 and CRD0007) may be considered to be tentative given no test pumping has been conducted in this area, available information from testing in other areas and from exploration bores (including the nature of water level distribution) suggests that aquifer permeability may be low and/or the aquifer geometry may be affected by compartmentalisation.

Future drilling and test pumping on the range will provide useful information to better understand the hydrogeological environment/connectivity in this area and can be used to revise the numerical model and associated drawdown estimations at the key environmental features.

9.2.2 Road Construction Water Supply

Prior to the commencement of mining, construction water will be needed to construction and upgrading of public and private roads. Pairs of production bores will supply Turkeys Nest (TN) storages along the road alignment, such that the requirement for 8 L/s per TN, will be shared by the two bores closest to each TN.

Cones of depression have been analytically calculated for all production bores operating at their proposed maximum abstraction rates for construction of the haul road (Table 9-2). As noted previously, the production bores will only operate for the duration of time that road construction is in their vicinity. Accordingly 2 months continuous operation has been modelled, using the transmissivities derived from the hydraulic testing.

Table 9-2: Summary of Modelled Operational Drawdown for Road Construction

| Bore ID | CRT Pumping Rate (L/s) | Transmissivity Range (m²/day) | Proposed Pumping Rate (L/s) | Aquifer Drawdown at Bore (m) | Aquifer Drawdown at 1 km radius (m) | Aquifer Drawdown at 5 km radius (m) |
|---------|---------------------------------|-------------------------------------|-----------------------------------|---------------------------------------|--|--|
| CRD0082 | 25 | 190 to 210 | 4.0 | 3.00 | 0.40 | 0.10 |
| CRD0083 | 20 | 200 to 220 | 4.0 | 2.86 | 0.45 | 0.05 |
| CRD0084 | 6 | 47 to 237 | 4.0 | 4.16 | 0.60 | 0.00 |
| CRD0085 | 5 | 100 to 165 | 4.0 | 4.52 | 0.60 | 0.00 |
| CRD0086 | 4 | 395.00 | 3.0 | 1.17 | 0.22 | 0.04 |
| CRD0087 | 15 | 593.00 | 5.0 | 1.33 | 0.29 | 80.0 |
| CRD0088 | 12 | 300 to 440 | 4.0 | 1.67 | 0.30 | 0.06 |
| CRD0089 | 12 | 22 to 54 | 4.0 | 14.58 | 0.13 | 0.00 |

Fractured rock settings are very difficult to analytically model and hydraulic properties derived from hydraulic testing are typically imprecise as the primary assumptions used in classical methods of pumping test analysis, do not apply in fractured rock settings. In particular, fractured rock settings are not homogeneous, isotropic, nor of infinite extent. Compartmentalisation is common and drawdown

Assessment of Potential Impacts

May 16, 2018

distribution and magnitude depends upon how the fractured fabrics and structural features in the rock are connected.

Reference to Table 9-2 shows that for the pumping scenario examined, drawdown impacts 1 km from the bore are generally less than a 0.6 m, and by 5 km radius, they are negligible to zero m.

9.3 Groundwater Dependant Ecosystems

Eleven (11) small permanent or ephemeral pools have been identified in the upper (southern) reaches of the catchment, in the vicinity of the proposed mining areas (Table 9-3 and Figure 9-2). Four of the features have been identified as likely to be supported to some extent by groundwater contributions. In response to hydrogeological queries (received 20/09/2017) raised by the Department of Mines, Industry Regulation and Safety (DMIRS) and DWER on review of the Corunna Downs mining proposal, studies have been undertaken on the nature of these pools in the context of groundwater dependent ecosystems (Stantec, 2018). While a number of pools were identified as being potentially at risk at the operational mine abstraction rates (approximately 30.5 L/s), these combined operational abstraction rates greatly exceed the requirements of abstraction for haul road construction: 8 L/s per TN over 6 months. It is unlikely that abstraction for haul road construction will affect the pools or soak.

Table 9-3: Summary of surface water feature details.

| Location ID | Easting | Northing | Elevation (mAHD) | TDS (mg/L) | Groundwater Source | |
|-------------|----------|----------|------------------|------------|-----------------------|--|
| CO-WS-01 | 778586 | 7630030 | 255.627 | 210 | Likely | |
| CO-WS-02 | 776034 | 7620690 | 371.100 | No sample | Unlikely | |
| CO-WS-03 | 778506 | 7633950 | 227.531 | 180 | Unlikely (dry) | |
| CO-WS-05 | 773504 | 7623870 | 313.184 | 690 | Likely | |
| CO-WS-08 | 774961 | 7625570 | 321.721 | 510 | Unlikely | |
| CO-WS-09 | 776568 | 7622980 | 344.725 | 2800 | Unlikely (dry) | |
| CO-WS-10 | 777461 | 7629400 | 297.225 | No sample | Unlikely | |
| CO-WS-11 | 777517 | 7626870 | 398.728 | 33 | Unlikely | |
| CO-WS-12 | 777092.2 | 7629040 | 373.970 | 100 | Likely | |
| CO-WS-13 | 777092 | 7629040 | 327.170 | 550 | Unlikely | |
| CO-WS-14 | 774623 | 7623940 | 320.990 | 190-210 | Likely | |

Notes: Coordinates are GDA94

The operational raw water requirements were numerically modelled for the life of mine as outlined in (Section 9.1). Table 9-4 lists the drawdown results at specified time steps for each of the key environmental features. Four of the pools CO-WS's 3, 5, 8, and 13 were identified as having drawdowns of over 1 m after a year of abstraction at 30.5 L/s. By the end of mining the model indicated that these same features had been impacted between 2.3 and 3.73 m.

Woodman Environmental Consultants (WEC, 2018a) conducted an assessment of groundwater drawdown impacts to vegetation over the Project area. This assessment evaluated the presence of groundwater dependent vegetation (GDV), both on a landscape scale (VTs) and growing in association with key surface water features (pools), and the project's risk of groundwater drawdown related impact on this vegetation over the life of mine. The assessment identified the following potentially groundwater dependent features that may be at Moderate to High risk of impact and therefore require site specific assessment and potentially monitoring of impacts:

Assessment of Potential Impacts

May 16, 2018

- Moderate risk of impact: 0.15 ha of GDV mapped as VT 3 (vegetation may provide a role as a refuge);
- High risk of impact: 48.79 ha of GDV (VTs classified as being obligate (VT 15) or facultative and may provide a role as a refuge (VT 3);
- Surface water features: CO-WS-05, CO-WS-08 and CO-WS13; due to a combination of GDV presence, groundwater dependence of the pool areas and potential impact on groundwater levels in these areas (as reported by Stantec 2018a).

Given the short project life, the relatively small areas of the VTs at risk of impact and their broader distributions in the project area, the potential impacts are not considered to be significant in a regional context.

Two other important hydrological features have been identified in the vicinity by previous surveys:

- A freshwater wetland system was identified by Golder Associates Pty Ltd (2010). This feature corresponds to identified important surface water features CO-WS-05 and CO-WS-13 already discussed; and
- A feature referred to as a "freshwater soak" has been investigated separately in the context of
 potential impacts of groundwater abstraction (WEC, 2018b), and has been determined to not
 represent groundwater dependent vegetation. This site is characterized as VT 8.

Table 9-4: Drawdown estimates for key environmental locations, at specified time steps

| Key Environmental | Drawdown estimations over the Life of Mine (m) | | | | | | | | | |
|-------------------|--|------|------|------|------|------|------|--|--|--|
| Feature | 0.5 Yr | 1 Yr | 2 Yr | 3 Yr | 4 Yr | 5 Yr | 6 Yr | | | |
| CO-WS-01 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | | | |
| CO-WS-02 | 0.01 | 0.04 | 0.12 | 0.22 | 0.33 | 0.45 | 0.56 | | | |
| CO-WS-03 | 0.91 | 1.34 | 1.79 | 2.01 | 2.15 | 2.24 | 2.30 | | | |
| CO-WS-05* | 0.69 | 1.25 | 2.07 | 2.63 | 3.02 | 3.31 | 3.52 | | | |
| CO-WS-08* | 0.75 | 1.27 | 2.01 | 2.51 | 2.86 | 3.12 | 3.31 | | | |
| CO-WS-09* | 0.01 | 0.02 | 0.04 | 0.07 | 0.09 | 0.10 | 0.11 | | | |
| CO-WS-10 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | | | |
| CO-WS-11* | 0.01 | 0.03 | 0.09 | 0.15 | 0.21 | 0.26 | 0.29 | | | |
| CO-WS-12 | 0.00 | 0.01 | 0.02 | 0.03 | 0.03 | 0.04 | 0.05 | | | |
| CO-WS-13* | 0.91 | 1.48 | 2.30 | 2.85 | 3.24 | 3.52 | 3.73 | | | |
| CO-WS-14* | 0.02 | 0.04 | 0.06 | 0.07 | 0.08 | 0.09 | 0.10 | | | |

^{*} Subject to further hydrogeological characterisation (i.e. drilling and test pumping of proposed water abstraction bores on the range.

While haul road construction is unlikely significantly impact on any of the pools, the numerical model output indicates that there may be significant drawdown impacts and a strict monitoring program will need to be put in place to monitor all the pools and the soak, immediately before operational abstraction begins. The proposed monitoring program is outlined in the Operating Strategy (Appendix H)

Note that studies for the operational impacts for mining are ongoing in consultation with DMIRS and DWER.

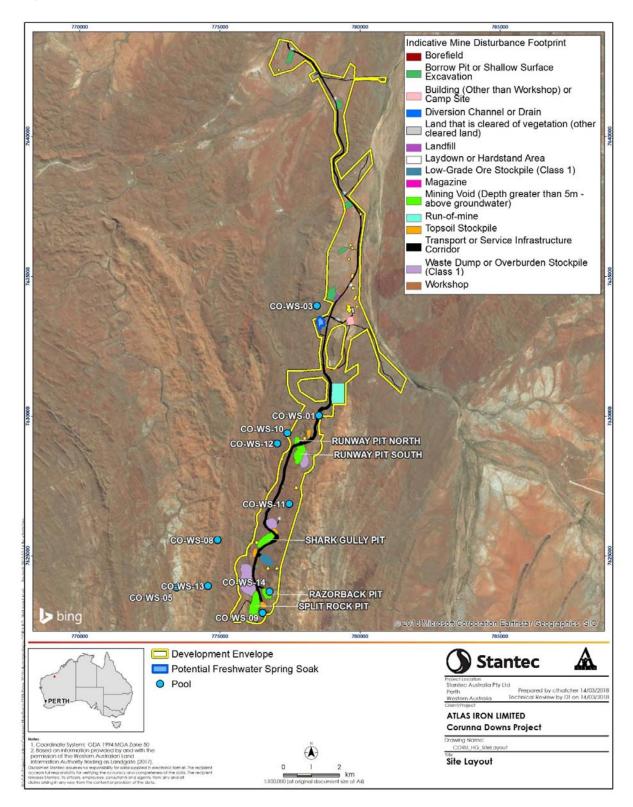


Figure 9-2: Location of Possible Groundwater Dependant Ecosystems

May 16, 2018

9.4 Other Groundwater Users

A search of DWER borehole databases revealed no other groundwater users along the haul road alignment, close enough to be impacted by abstraction for haul road construction. The closest significant other users production bore is Bore 1/99 (DWER Site Reference 71012155) located in the Marble Bar township water supply borefield, approximately 3.2 km north northwest of CRD0088. The location of the Marble Bar borefield is adjacent to the Coongan River and across the geological strike of the country rock between the borefield and CRD0088. It is unlikely that abstraction of 4 L/s from CRD0088 for a portion of the 6 month construction period, will impact upon the borefield.

No other groundwater users have been identified with 5 km of the haul road construction water supply bores or the mining area. Registered bores within 5 km of the production bores are all either abandoned or belong to Atlas.

9.5 Groundwater Quality

Groundwater pumping induced changes groundwater quality was investigated through test pumping on each new production bore. Electrical conductivity was monitored throughout the step and constant rate testing. There were no significant changes observed due to different pumping rates or prolonged pumping for the duration of the tests. A groundwater sample was also collected at the start and the end of testing, these showed no significant changes in any ion concentration.

10. Operating Strategy

A Groundwater Operating Strategy for the Project, prepared in a standalone format to facilitate operational utilisation, and in accordance with DWER's Operational policy 5.08 - Use of operating strategies in the water licensing process (DoW, 2011), is attached in Appendix H.

11. Summary/Recommendations

The key findings from the hydrogeological investigation are as follows:

- Twelve (12) pilot groundwater exploration holes have been drilled along the proposed haul road alignment.
- Eight (8) production bores have been constructed adjacent to the best performing pilot holes, using ND 200 mm (8") Class 12 UPVC blank and slotted casing.
- All production bores have been hydraulically tested by step rate testing (four 100 minute steps at increasing rates), a 72 hour constant rate test (CRT), and a recovery test. Test details are summarised in Table 6-1.
- Groundwater in the study area is fresh to brackish, with TDS ranging from 410 to 1,800 mg/L. The key major ions include sodium (43 to 630 mg/L), chloride (19 to 500 mg/L), and bicarbonate (300 to 700 mg/L). Potassium concentrations are relatively low (0.5 to 2.5 mg/L).
- With the exception of fluoride, arsenic, manganese and nickel, all groundwater sample concentrations for analytes listed in the Australian Drinking Water Guidelines (NHMRC, NRMMC, 2011) are below guideline concentrations.

Summary/Recommendations

May 16, 2018

- CRD0086 is the only production bore in which Australian Drinking Water Guidelines criteria were exceeded and given the groundwater will be used for road construction, the exceedances are not considered to be a risk to livestock or the environment.
- Surface water TDS ranges from 33 to 2,800 mg/L, and is generally characterised by the same major ions as in the groundwater, although in differing relative concentrations.
- The production bores are all hydraulically inefficient to various degrees and they are not likely to be able to sustain the pumping rates selected for the CRTs. The proposed operational pumping rates the production bores are presented in Table 9-2.
- Sustainability at any selected pumping rate for individual bores will be a function or balance between recharge (rainfall), available storage, and the rate of pumping. Accordingly, the time of the year when the six month water supply is required, will affect the operational sustainability of supply.
- There are no other groundwater users along the proposed haul road alignment that could be impacted by abstraction for construction water supply.
- There are a number of surface water pools that may be temporarily impacted by abstraction from nearby production bores. However, the short duration of the haul road construction (6 months) and the even shorter duration of abstraction from individual production bores along the alignment (assumed maximum 2 months), means impacts if any, are likely to be minimal and of short duration. Nevertheless, monitoring of individual pools located near production bores will be carried out. Production bores where this will apply are CRD0082 and CRD0083.
- Abstraction for the mine site operational water requirements over the life of mining may impact
 upon surface water pools CO-WS-03, CO-WS-05, CO-WS-08, and CO-WS-13, and these features will
 be the focus of stringent monitoring during the life of mine operations.
- This report is to be submitted to the Department of Water and Environmental Regulation, in support of an application for a 5C Licence to Take Water, for an annual allocation of 1,100,000 kL.

12. References

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 Unpublished report prepared for Atlas Iron Limited. May, 2018



Appendix A Groundwater Licences



Your Ref: App13211
Our ref: RF10954; wrd352780
Enquiries:insStephanie:Phamia's water future
(08) 6364 6874

Corunna Downs

David Nyquest Atlas Iron PO Box 7071 Cloisters Square WA 6850

Dear David,

Re: Issue of a licence under the Rights in Water and Irrigation Act 1914

Property: L45/408, G45/339, L45/418, E45/4639, L45/407, M45/1257, L45/410 - Corunna Downs Project

Please find enclosed your licence to take groundwater - GWL176960(4).

Please take time to read this document as it contains important information about your rights and responsibilities.

In addition, please note the following:

There are Clearing Regulations Schedule 1 Areas within the tenements. Please be advised that if you wish to undertake any clearing of vegetation within these areas you will need to do so in consultation with the Department of Environment Regulation (DER). Please contact the DER on (08) 6467 5000 for further information.

If you have any queries about this matter please contact Stephanie Pham on (08) 6364 6874.

Yours sincerely,

Kevin Hopkinson

Program Manager - Pilbara District

North West Region

lein Helonon

Department of Water

29 May 2017

Page 1 of 1
Instrument No. GWL176960(4)

LICENCE TO TAKE WATER

Granted by the Minister under section 5C of the Rights in Water and Irrigation Act 1914

| Licensee(s) | Atlas Iron Limited | | | | | |
|----------------------------------|--|--|-----------------|--|--|--|
| Description of Water Resource | Pilbara Pilbara - Fractured Rock | Annual Water Entitlement | 100000 kL | | | |
| Location of Water Source | L45/408, G45/339, L45/418, L45 | /410, L45/407, M45/1257, E45/4 | 1639 | | | |
| Authorised Activities | Taking of water for | Location of Activity | | | | |
| | Dust suppression for earthworks and construction purposes Exploratory drilling operations General campsite purposes Potable Water Supply purposes Road construction purposes Road maintenance purposes | L45/408, G45/339, L45/418, L M45/1257, E45/4639 | 45/410, L45/407 | | | |
| Duration of Licence | From 29 May 2017 to 28 May 20 | 27 | | | | |

This Licence is granted subject to the Rights in Water and Irrigation Regulations 2000



Your Ref: App13998
Our ref: RF10954; wrd358426
Enquiries: Stephanie Phan (08) 6364 6874
Securing Western Australia's water future

David Nyquest Atlas Iron PO Box 7071 Cloisters Square WA 6850

Dear David,

Re: Issue of a licence under the Rights in Water and Irrigation Act 1914

Property: Section 91 Lic 869-2016 A6435862 - Corunna Downs Project

Please find enclosed your licence to take groundwater – GWL184565.

Please take time to read this document as it contains important information about your rights and responsibilities.

In addition, please note the following:

There are registered sites of Aboriginal Heritage Significance within the project area. Please be advised that it is your responsibility to ensure appropriate consultation with any affected Traditional Owners and adequate referral to the Department of Aboriginal Affairs (DAA) is made, to ensure full compliance with the *Aboriginal Heritage Act 1972*.

Clearing Regulations Schedule 1 Areas are within your project area. Please be advised that if you wish to undertake any clearing of vegetation within these areas you will need to do so in consultation with the Department of Environment Regulation (DER). Please contact the DER on (08) 6467 5000 for further information.

Contaminated site ID1335 near Halse Road/Limestone Marble Bar Road has been identified as near or within your project area. The site is listed as "possibly contaminated – investigation required" under the Department of Environment Regulation (DER) contaminated sites classification system. Please consult the DER for additional information and advice and/or any relevant approvals. The DER Contaminated Sites hotline number is 1300 762 982.

Priority fauna are located within the project area. If you have any queries, please contact the Department of Parks and Wildlife's Species and Communities Branch on (08) 9219 9511 for further information.

The Marble Bar Water Reserve was proclaimed in 1972 under the Country Areas Water Supply Act 1947 (CAWS).

A Drinking Water Source Protection Plan was prepared for the Marble Bar Water Reserve in 2000, and updated in 2010. Groundwater is drawn from the Coongan well-field 2-3km west of the town and adjacent to the Coongan River. The Coongan wellfield draws from fractured volcanic rock on the Coongan Rivers eastern bank. Significant recharge occurs during high rainfall events and the direction of groundwater flow is closely related to surface drainage, in a north to north westerly direction.

Given the unconfined nature of the aquifer, it is vulnerable to contamination. Land and water based uses and activities within the catchment can directly affect water quality and treatment. It should be noted that protecting a drinking water supply to provide a safe drinking water source is a cheaper option than both treatment and remediation; furthermore treatment is not 100% reliable.

It is therefore important to ensure any bores are appropriately located to avoid drawdown and constructed to prevent contamination of the public drinking water source. All bores should be constructed in accordance with *Minimum construction requirements for water bores in Australia* (National Minimum Bore Specifications Committee 2003).

Existing and future mining proposals within the water reserve are compatible with conditions, and should adhere to the Department of Water's *Water Quality Protection Guidelines for Mining and Mineral Processing 1-11* and other relevant Water Quality Protection Notes published by the Department of Water

If you have any queries about this matter please contact Stephanie Pham on (08) 6364 6874.

Yours sincerely,

Kevin Hopkinson

Program Manager – Pilbara District

North West Region Department of Water

Keen Hysterson

30 May 2017



Page 1 of 1 Instrument No. GWL184565(1)

LICENCE TO TAKE WATER

Granted by the Minister under section 5C of the Rights in Water and Irrigation Act 1914

| Licensee(s) | Atlas Iron Limited | | | | | | | | | |
|----------------------------------|--|-------------------------------|------------------|--|--|--|--|--|--|--|
| Description of Water Resource | Pilbara Pilbara - Fractured Rock | Annual Water Entitlement | 100000 kL | | | | | | | |
| Location of Water Source | Section 91 of the LAA Lic 00869 | -2016_A6435862 | | | | | | | | |
| Authorised Activities | Taking of water for | Location of Activity | | | | | | | | |
| | Dust suppression for earthworks and construction purposes Exploratory drilling operations Road construction purposes Road maintenance purposes | Section 91 of the LAA Lic 008 | 69-2016_A6435862 | | | | | | | |
| Duration of Licence | From 31 May 2017 to 31 January 2019 | | | | | | | | | |

This Licence is granted subject to the Rights in Water and Irrigation Regulations 2000

Appendix B Type lithology examples

The table below illustrates the different lithology's that were encountered during the Corunna Downs hydrogeological drilling investigation. The table acts as a type example of geological descriptions used in the drill logs presented Appendix C.

| Formation | Type/Weathering | Photo | Description |
|------------------|------------------------|-------|---|
| Mt Roe Basalt | Extremely Weathered | | Extremely weathered, cream/grey powder and clay material. No visible texture or grain size. Photo: CRD0058 4 – 12 mbgl |
| Mt Roe Basalt | Highly Weathered | | Highly weathered, red/yellow/purple colour, chips 1-20 mm. Photo: CRD0050 33 mbgl |
| Mt Roe Basalt | Weathered | | Weathered, black/grey/brown, very hard and angular, chips 1-5 mm. Photo: CRD0050 30 mbgl |
| Mt Roe Basalt | Fresh | | Fresh dark grey/black basalt Photo: CRD0026 74 mbgl |
| Mt Roe Basalt | Doleritic | | Doleritic basalt, dark grey, 40% mafic, 60% quartz. Photo: CRD0026 36 mbgl |

Duffer Formation

Moderately weathered



Photo: CRD0078 32 mbgl

Appendix C Drillhole Graphic Logs





EXPLORATION BORE CRD0038 (Complete)

| CLIE | NT Atlas Iron | n Limited | | | | | PROJECT NAME Corunna Down | ns Hydrogeologica | ıl Investigati | ions | | |
|--------------|---------------|--|----------------------|-----------------|---|----------------------------|---|-----------------------------|---------------------------|--------------------|------------------|--|
| | | R 83503916 | | | | | | | | | | |
| | | | | | | | HOLE DIAMETER _304.8/152.4 r | nm | | | | |
| | | ACTOR (DRILLED B | SY) <u>Fo</u> | raco (l | Rig 8 |) | GROUND WATER LEVELS: | | | | | |
| | | Air Hammer | | | | | | ater Cut)18.00 | m bgl | | | |
| | | I, Atlas Iron | | | | | AFTER DRILLING | | | | | |
| | TING | | NOR | THING | 3 — | | Comments: | | | | | |
| DAT | | | | | | | No construction as CRD0038 is a pilot hol | le. | | | | |
| SWL | . REF. POINT | ELEV. () | i | | | | | | | ı | | |
| DEPTH (m) | | WELL CONSTRUCTION | | TIND | LITHOLOGY | | ATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | pH drilling | ELEVATION (m) | |
| 0 | Steel: +0.2 m | Inclination: -90 (deg) | | , , | 1 | Depth | ub-rounded, silty sand and clay | - 0 m 4 | 320 440 560 680 | 8.8.8.8 2.4.0.8 | | |
| | | 12" Surface Steel Casir - 6 mbgl] | ng [0.2 | | | [6 m] | ub-rounded, silty sand and clay, some | | | | | |
| 10 | | | _ | NOTINE NOTINE | | [10 m] | | | | | | |
| 20 | ¥ | | | | | [10 m] | hly weathered with clay. Water at 18m | | | | | |
| 30 | | 6" Air Hammer Drilling Method [6-60 mbgl] | | KONNY NOEBASALI | 7 < 7 < 7 < 7 < 7 < 7 < 7 < 7 < 7 < 7 < | GRANODIORIT quartz. [16 m] | TE/GRANITE: Moderately weathered, | | | | | |
| | | | | * | | | erately fresh, possible granodiorite and lots | | | | | |





EXPLORATION BORE CRD0038 (Complete)

| CLII | ENT Atlas Iron Limited | | | | | PROJECT NAME Corunna Downs H | /drogeologica | al Investigat | ions | | | | | |
|-------------|--|-----------------------|------------|-----------|-------|--|--|-----------------------------|---------------------|---|---------------|--|--|--|
| PRO | DJECT NUMBER 83503916 | | | | | | LOCATION Corruna Downs | | | | | | | |
| DAT | TE STARTED 9/4/17 | COMF | PLE. | TED . | 10/4/ | 17 | HOLE DIAMETER _304.8/152.4 mm | | | | | | | |
| DRI | LLING CONTRACTOR (DRILLED E | BY) <u>For</u> | raco | (Rig | 8) | | GROUND WATER LEVELS: | | | | | | | |
| DRI | LLING METHOD _Air Hammer | | | | | | ▼ AT TIME OF DRILLING (Water Cut) 18.00 m bgl | | | | | | | |
| LO | GGED BY DN, Atlas Iron | CHEC | KE | D BY | PH, | Stantec | AFTER DRILLING | | | | | | | |
| EAS | STING | NORT | ГНІМ | IG _ | | | | | | | | | | |
| DAT | гим | | | | | | Comments: No construction as CRD0038 is a pilot hole. | | | | | | | |
| sw | L REF. POINT ELEV. () | | | | | | F | | | | | | | |
| G DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | LIND | LITHOLOGY | Layer | МА | TERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | 8 8 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | ELEVATION (m) | | | |
| 60 | mainanat. 90 (deg) | | ROE BASALT | | Depth | BASALT: Moder of quartz. [18 m] (continued | ately fresh, possible granodiorite and lots | | | | | | | |

Bottom of borehole at 60.0 m.





| PROJ | ECT NUMBER | R 83503916 | | | | | | LOCATION Corruna Downs | | | | | | |
|--------------|----------------|-----------------------------------|----------------------|---------------|-----------|----------------|--|--|----------------------------------|------------------------|-----------------------------------|-------------|--|--|
| | | | | | | | | HOLE DIAMETER 203.2/152.4 mm | | | | | | |
| DRILL | ING CONTRA | ACTOR (DRILLED I | BY) <u>Fo</u> | orac | o (Rig | 8) | | GROUND WATER LEVELS: | | | | | | |
| | | | | | | | | AT TIME OF DRILLING (Water Cut) 4.00 m bgl | | | | | | |
| | | Stantec | | | | | | AFTER DRILLING | | | | | | |
| | · | <u> </u> | _ | | | | | Comments: | | | | | | |
| GROU | IND ELEVAI | TION | DAIL | JIVI | | | | Water inject from 11 m due dust. Lots of water at 12 m free flowing. Collar blew out due water erosion. No cor | rod change, n struction as Cf | o water RD0039 | inject from 1: is a pilot hole | 3 m - e. | | |
| DEPIH (m) | | WELL CONSTRUCTION | | LINO | LITHOLOGY | | | MATERIAL DESCRIPTION | dr | SCH. illing _/s) | EC drilling (μS/cm) | | | |
| 0 | Collar: +0.2 m | Inclination: -90 (deg) | | | • | Layer Depth | Colluvium | | | 1 N 8 4 | 040 | - | | |
| | | 8" Surface Steel Casin 2 mbgl] | ng [0.2 - | соптилим | , Pr | 2.0 | [2 m] | | _ | | | | | |
| | | | | 7000 | 0 | 4.0 | Colluvium with [2 m] | extremely weathered khaki basalt | | | | | | |
| 10 | Ţ | | • | | | 10.0 | Basalt, khaki, 6 [6 m] | extremely weathered, soft and damp | | | | | | |
| - | | | | | | 14.0 | competant rock [4 m] | ey to cream with minor khaki, strongly weathered but k, water inject from 11m | _ | | | | | |
| - | | | | | | | rock. Trace cal | ey with minor knaki,weakiy weathered but competant cite veining. Fracture at 17 m (dark khaki water) | | | | | | |
| 20 | | | | | | 24.0 | red-brown wate [4 m] | n weakly weathered, light grey to khaki basalt, dark er to 24 m, but drill good drlling 23 to 24 m | - | | | | | |
| 30 | | | | MT ROE BASALT | | | contamination probably from 2 Fracture (? sof noted. Fracture | ght grey, very fine grained, mostly massive. Uphole by strongly weathered khaki vesicular and massive basalt 20 to 24. Trace to no iron oxides or stainings on joints. t ground and brown water) at 43 m, no increase in flow e (?) 46 to 50m, increased large khaki chips (up to 3 cm) ase. Fracture (?) 58 to 62m with collar blow out | | | | | | |
| - | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | |





| CLIENT | T Atlas Iron Limited | | | | | | PROJECT NAME _Corunna Downs Hydrogeological Investig | gations | |
|---|--|------|---------------|-----------|----------------|--|---|--------------------|-----------|
| | CT NUMBER 83503916 | | | | | | | | |
| DATES | STARTED <u>5/11/17</u> | COMF | PLE | TED | 6/11/ | 17 | HOLE DIAMETER _ 203.2/152.4 mm | | |
| 1 | NG CONTRACTOR (DRILLED E | | | | | | | | |
| DRILLI | NG METHOD Air Hammer | | | | | | AT TIME OF DRILLING (Water Cut) 4.00 m bgl | | |
| | ED BY DT,Stantec | | | | | | - | | |
| | NG 782275 | | | | | | | | |
| | ND ELEVATION | | | | | | Comments: | | 2 |
| J. S. | | | | | | | free flowing. Collar blew out due water erosion. No construction as CRD00 | 139 is a pilot hol | le. |
| DEPTH (m) | WELL CONSTRUCTION | | LINO | LITHOLOGY | | | MATERIAL DESCRIPTION DISCH drilling (L/s) | drilling | ELEVATION |
| 50 | Inclination: -90 (deg) | | | _ | Layer Depth | | T 0 0 | 1080 | 8 |
| 60 70 80 80 100 | 6" Air Hammer Drilling Method [2-102 mbgl] | | MT ROE BASALT | | 70.0 | contamination probably from Fracture (? so noted. Fractur with flow incre [46 m] (contin | light grey, very fine grained, mostly massive. Uphole n by strongly weathered khaki vesicular and massive basalt, 120 to 24. Trace to no iron oxides or stainings on joints. fit ground and brown water) at 43 m, no increase in flow re (?) 46 to 50m, increased large khaki chips (up to 3 cm) ease. Fracture (?) 58 to 62m with collar blow out. | | |
| 100 | | | | | | | | | |



PAGE 3 OF 3

| CLI | ENT Atlas Iron Limited | | | | | PROJECT NAME Corunna Downs Hydrogeologica | al Investigati | ions | | | |
|----------------|--|----------------------|-------|---------------|----------------|--|-----------------------------|---------------------------|---------------|--|--|
| PRO | DJECT NUMBER 83503916 | | | | | LOCATION Corruna Downs | | | | | |
| DAT | TE STARTED <u>5/11/17</u> | СОМ | PLE | TED | 6/11/17 | HOLE DIAMETER _203.2/152.4 mm | | | | | |
| DRI | LLING CONTRACTOR (DRILLED I | 3Y) <u>Fo</u> | oraco | o (Rig | 8) | GROUND WATER LEVELS: | | | | | |
| DRI | LLING METHOD Air Hammer | | | | | _ X AT TIME OF DRILLING (Water Cut) _4.00 r | n bgl | | | | |
| LO | GGED BY DT,Stantec | CHE | CKE | D BY | FC,Stantec | AFTER DRILLING | | | | | |
| EAS | STING 782275 | NOR | THII | NG 76 | 52340 | - | | | | | |
| | DUND ELEVATION | DAT | | | | Comments: Water inject from 11 m due dust. Lots of water at 12 m rod cha free flowing. Collar blew out due water erosion. No construction | | | | | |
| B DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | UNIT | LITHOLOGY | Layer Depth | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | ELEVATION (m) | | |
| | | | | \Rightarrow | 102.0 | | | | | | |

Bottom of borehole at 102.0 m





| | NT Atlas Iron | Limited 8 _ 83503916 | | | | | | | | | |
|--------------|----------------|---------------------------------|----------|--------|----------|----------------|---|---|-----------------------------|--------------------------|-------|
| | | | | | | | | HOLE DIAMETER 203.2/152.4 mm | | | |
| | | ACTOR (DRILLED E | | | | | | | | | |
| | | Air Hammer | , | | | , | | | m bal | | |
| | | Stantec | CHE | CKE | D BY | FC,S | Stantec | | | | |
| | | 2 | | | | | | | | | |
| GRO | OUND ELEVAT | ION | DAT | UM _ | | | | Comments: Issues with hammer during drilling. No construction as CRD0046 |) is a pilot hol | le. | |
| DEPTH (m) | (| WELL CONSTRUCTION | | TINO | гтногову | | | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm | |
| 0 | Collar: +0.2 m | Inclination: -90 (deg) | | | | Layer Depth | | | - 0 m 4 | 1720 1840 1960 | 2080 |
| 10 | ¥ | 8" Surface Steel Casing 2 mbgl] | g [0.2 - | DUFFER | | 17.0 | massive but ex on joints and of [2 m] Basalt, slightly generally mass water in fracture [15 m] Extremely weat penetration [1 m] Basalt, slightly generally mass water in fracture [1 m] Basalt, slightly generally mass water in fracture [1 m] | r weathered to fresh, green grey to grey, very fine grained, sive with iron oxide stains and coats on defect faces. First red interval 12.5 to 13 m athered fractured zone in basalt (as above), rapid r weathered to fresh, green grey to grey, very fine grained, sive with occasional fractures, iron oxide stains and coats | | | |
| | | | | | | 31.0 | Fracture zone | in basalt (as above), notable increase in yield | | \ | |
| 1 | | | | | | 32.0 | [1 m] | weathered to fresh, green grey to grey, very fine grained, | | | 1 |
| - | | | | | | 36.0 | | sive with occasional fractures, iron oxide stains and coats | | | i |
| | | | | | | | Fracture zone [4 m] | in basalt (as above) | | | |
| - | | | | | | | | | | | |
| 40 | | | | | | 40.0 | | weathered to fresh, green grey to grey, very fine grained, sive with occasional fractures, iron oxide stains and coats s | | | |
| 50 | | | | | | | | | | | |





| PRO DAT | STARTED 9/11/17 | СОМРІ | LETED | 10/11/17 | PROJECT NAME Corunna Downs Hydrogeological Investigations LOCATION Corruna Downs HOLE DIAMETER 203.2/152.4 mm GROUND WATER LEVELS: | | | | | | |
|---|--|---------|-----------|---|--|-----------------------------|---|--|--|--|--|
| DRIL | LING METHOD Air Hammer | | | | AT TIME OF DRILLING (Water Cut) | | | | | | |
| | GGED BY DT,Stantec | | | | | | | | | | |
| | TING 785602 DUND ELEVATION | | | | Comments: | CRD0040 is a pilot ho | le. | | | | |
| DEPTH (m) | WELL CONSTRUCTION | FINE | LITHOLOGY | Layer | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | 1720 1840 1860 1860 2080 ELEVATION | | | | |
| 50 | Inclination: -90 (deg) 6" Air Hammer Drilling Method [2-102 mbgl] | | | | | | 1 | | | | |
| | | | | Fracture zone | in basalt (as above) | | | | | | |
| | | | | Basalt, slightl generally mas | y weathered to fresh, green grey to grey, very fine grained, ssive with occasional fractures, iron oxide stains and coats as | | | | | | |
| 60 | | | | 3 cm) chips - [2 m] Basalt, slightl | in basalt (as above). Airlift returned numerous large (up to uphole contamination?. y weathered to fresh, green grey to grey, very fine grained, sive with occasional fractures, iron oxide stains and coats as | | | | | | |
| 70 | | | | 74.0 | | | | | | | |
| 80 | | מזיבורס | DOTTER | 76.0 [2 m] Basalt, slightl | y weathered to fresh, green grey to grey, very fine grained, ssive with occasional fractures, iron oxide stains and coats es | | | | | | |
| | | | | | in basalt (as above) | | | | | | |
| 100 100 | | | | Basalt, variou grained, gene and coats on | sly weathered to fresh, green grey to grey, very fine rally massive with occasional fractures, iron oxide stains defect faces. Difficult to differentiate whether weathered situ or contamination | | | | | | |
| 90 | | | | | | | | | | | |
| | | | | | | | | | | | |
| 100 | | | | | W (2) | | | | | | |



PAGE 3 OF 3

| ١ | | | | | | | | | | | | | |
|-----------|--|----------------------|--------|--------------|----------------|--|-----------------------------|---------------------------|------------------|--|--|--|--|
| | ENT Atlas Iron Limited | | | | | PROJECT NAME Corunna Downs Hydrogeologica | al Investigati | ons | | | | | |
| PRO | DJECT NUMBER <u>83503916</u> | | | | | LOCATION Corruna Downs | | | | | | | |
| DA. | TE STARTED <u>9/11/17</u> | COM | PLE | TED | 10/11/17 | HOLE DIAMETER 203.2/152.4 mm | | | | | | | |
| DRI | LLING CONTRACTOR (DRILLED I | BY) <u>Fo</u> | oraco | o (Rig | 8) | _ GROUND WATER LEVELS: | | | | | | | |
| DRI | LLING METHOD Air Hammer | | | | | AT TIME OF DRILLING (Water Cut) 13.00 m bgl | | | | | | | |
| LO | GGED BY DT,Stantec | CHE | CKE | D BY | FC,Stantec | AFTER DRILLING | | | | | | | |
| EAS | STING 785602 | NOR | THI | NG 76 | 54390 | | | | | | | | |
| GR | OUND ELEVATION | DAT | UM | | | Comments: Issues with hammer during drilling. No construction as CRD00- | 40 is a pilot hol | e. | | | | | |
| | | | | | | | | | | | | | |
| DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | UNIT | LITHOLOGY | Layer Depth | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | ELEVATION (m) | | | | |
| | | | DUFFER | | 102.0 | | | | | | | | |

Bottom of borehole at 102.0 m





| CLIE | NT Atlas Iron | Limited | | | | | | PROJECT NAME Corunna Downs Hydrogeo | ological | Inves | stigat | ions | | |
|---|----------------|--|--------|-------------------------|--------------------|-------|--------------------------------------|--|------------|------------------------------|-----------------|--|------------------------|------------------|
| PRO | JECT NUMBER | 8 83503916 | | | | | | LOCATION Corruna Downs | | | | | | |
| DAT | E STARTED 3 | 3/11/17 | COMP | LET | ED _ | 4/11/ | /17 | HOLE DIAMETER 203.2/152.4 mm | | | | | | |
| | | | | | | | | GROUND WATER LEVELS: | | | | | | |
| | | Air Hammer | | | | | | | 10.00 r | n bgl | | | | |
| LOG | GED BY DT, | Stantec | CHEC | KED | BY | FC, | Stantec | AFTER DRILLING | | | | | | |
| | | 3 | | | | | | Comments: | | | | | | |
| GRO | UND ELEVATI | ION | DATUI | М_ | | | | Delays due to rod handler and hammer sub. No construction | ction as (| CRD00 | 143 is a | a pilot ho | ile. | |
| DEPTH (m) | | WELL CONSTRUCTION | | LINO | LITHOLOGY | Layer | | MATERIAL DESCRIPTION | | DISC drill cas (L/s | ing ed s) | 040 040 080 080 04 04 04 04 04 04 04 04 04 04 04 04 04 | ing ed cm) | ELEVATION (m) |
| 0 | Collar: +0.2 m | Inclination: -90 (deg) 8" Surface Steel Casing | [0.2 - | WOUND. | | Depth | | weathered and fresh basalt lithics | | 7 7 | <u>υ</u> 4 | 5 6 3 | 1 1 | |
| | | 2 mbgl] | | 5 | | 1.5 | [1.5 m] Extremely weat | hered basalt with white clayey (when crushed) calcrete | | | | | | |
| | | | | Ц | | | [3.5 m] | ,,,, | | | | | | |
| | | | | | | 5.0 | Extremely weat grained, massiv [3 m] | hered basalt, fresh chips are light blue grey, very fine basalt | | | | | | |
| 10 | | | | | | 10.0 | given drilling te | hered basalt, khaki, appears vesicular but hard to confirm chnique | | | | | | |
| 10 | ¥ | | | | | 10.0 | [2 m] Weathered bas | alt, light blue grey, massive, iron oxide coatings on | | | | | | |
| + + | | | | Į | | | defects (joints a [8 m] | and fractures) | | | | | | |
| | | | | | | | | | | įį | į į | | ij | |
| 5 | | | | 1 | | | | | | | | | | |
| | | | | İ | | | | | | | | | | |
| <u> </u> | | | | Į | | 18.0 | Pacalt accassi | onally weathered and occasional iron oxide stains and | | 1 | | | | |
| 20 | | | | K | X | | | and defects. Uphole contamination from weathered khaki | | ij | į į | | i i l | |
| | | | | X | | | [34 m] | | | | | | | |
| | | | | K | \pm | | | | | | | | | |
| - | | | | <u>,</u> } | \rightleftarrows | | | | 7 | | | | | |
| | | | | MT ROE BASALT | \Rightarrow | | | | | \i i | į į | | | |
| | | | | MTRO | | | | | | \\ | | | | |
| | | | | X | \Rightarrow | | | | | \ | | | | |
| 30 | | | | 3 | \Rightarrow | | | | | | | | | |
| | | | | 3 | \Rightarrow | | | | | ijį | į į | | į | |
| | | | | 3 | \Rightarrow | | | | | | | | | |
| - 1 | | | | 3 | \Rightarrow | | | | | | | | | |
| <u> </u> | | | | } | \Rightarrow | | | | | | | | | |
| 20 30 30 30 30 30 30 30 30 30 30 30 30 30 | | | | 3 | Ξ | | | | | ili. | įį | | į [i | |
| | | | | 3 | Ξ | | | | | | | | | |
| 40 | | | | $\langle \cdot \rangle$ | ** | | | | | | 1 1 | | | |
| | | | | K | X | | | | | İ | | | | |
| | | 6" Air Hammer Drilling Method [2-84 mbgl] | | K | X | | | | | | | | | |
| | | | | 3 | \Rightarrow | | | | | | 1 | | | |
| <u> </u> | | | | 3 | \Rightarrow | | | | | | | | | |
| | | | | 3 | \Rightarrow | | | | | | | | | |
| 50 | | | | 3 | \exists | | | | | | | | ij | |
| \$ 50 | 1 1 | | ı | | | | (Continue | ed Next Page) | 1 | 1 1 | 1 1 | 1 1 1 | 17.1 | ı |





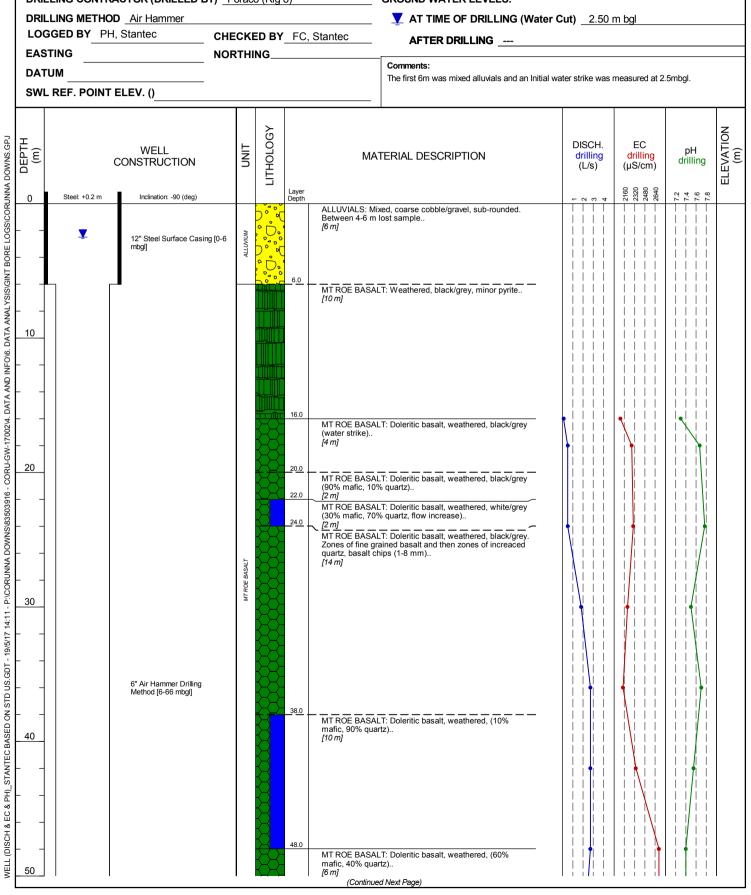
| EASTING 782368 GROUND ELEVATION HL (E) CONS | NOI | RTHII | NG 76 | | AFTER DRILLING | | | |
|---|-------------------|-------------|----------|----------------|--|-----------------------------|---------------------------|---------------|
| | DA1 | TUM _ | | | Comments: | | | |
| H (E) CONS | | | | | Delays due to rod handler and hammer sub. No construct | ion as CRD0043 is a | a pilot hole. | |
| | WELL STRUCTION | TINU | ГТНОГОСУ | Layer Depth | MATERIAL DESCRIPTION | DISCH. drilling cased (L/s) | EC drilling cased (µS/cm) | ELEVATION (m) |
| 60 | | MTROEBASALT | | 52.0 | red zone in basalt (as above), water turned khaki over interval and khaki vesicular basalt chips (>4 cm) recovered (contamination?) Tresh, light blue grey, with khaki weathered basalt uphole mination throughout. Trace iron oxide coatings, also possibly mination Bottom of borehole at 84.0 m | | | |





EXPLORATION BORE CRD0044 (Complete)

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations |
|--------------------------------|--------------------------|---|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs |
| DATE STARTED 10/4/17 | COMPLETED 11/4/17 | HOLE DIAMETER 304.8/152.4 mm |
| DRILLING CONTRACTOR (DRILLED I | BY) Foraco (Rig 8) | GROUND WATER LEVELS: |
| DRILLING METHOD Air Hammer | | ▼ AT TIME OF DRILLING (Water Cut) _ 2.50 m bgl |
| LOGGED BY PH, Stantec | CHECKED BY FC, Stantec | AFTER DRILLING |
| EASTING | NORTHING | |
| DATUM | | Comments: The first 6m was mixed alluvials and an Initial water strike was measured at 2.5mbgl. |
| SWL REF. POINT ELEV. () | | |







EXPLORATION BORE CRD0044 (Complete)

| CLII | ENT Atlas Iron Limited | | | | | | PROJECT NAME Corunna Downs | -lydrogeologica | al Investigat | ions | |
|-------------|--|----------------------|---------------|-----------|----------------|---------------------------------|---|-----------------------|---------------------------|---------------------------------------|---------------|
| PRC | DJECT NUMBER <u>83503916</u> | | | | | | LOCATION Corruna Downs | | | | |
| DAT | TE STARTED _10/4/17 | COM | PLE | TED . | 11/4/ | 17 | HOLE DIAMETER 304.8/152.4 mm | | | | |
| DRII | LLING CONTRACTOR (DRILLED E | 3Y) <u>Fo</u> | oraco | (Rig | 8) | | GROUND WATER LEVELS: | | | | |
| | LLING METHOD Air Hammer | | | | | | ▼ AT TIME OF DRILLING (Wate) | r Cut) 2.50 | m bgl | | |
| LO | GGED BY PH, Stantec | CHE | CKE | D BY | FS, | Stantec | AFTER DRILLING | , | | | |
| EAS | STING | NOR | | | | | | | | | |
| DAT | L REF. POINT ELEV. () | | | | | | Comments: The first 6m was mixed alluvials and an Initial | water strike was | measured at 2 | .5mbgl. | |
| S DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | UNIT | LITHOLOGY | Layer Depth | MA | TERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | 7.2 7.4 7.6 Hdillind 7.8 7.8 | ELEVATION (m) |
| 60 | | | MT ROE BASALT | | 54.0 | mafic, 40% qua [6 m] (continued | LT: Doleritic basalt, weathered, (90% | | | | |

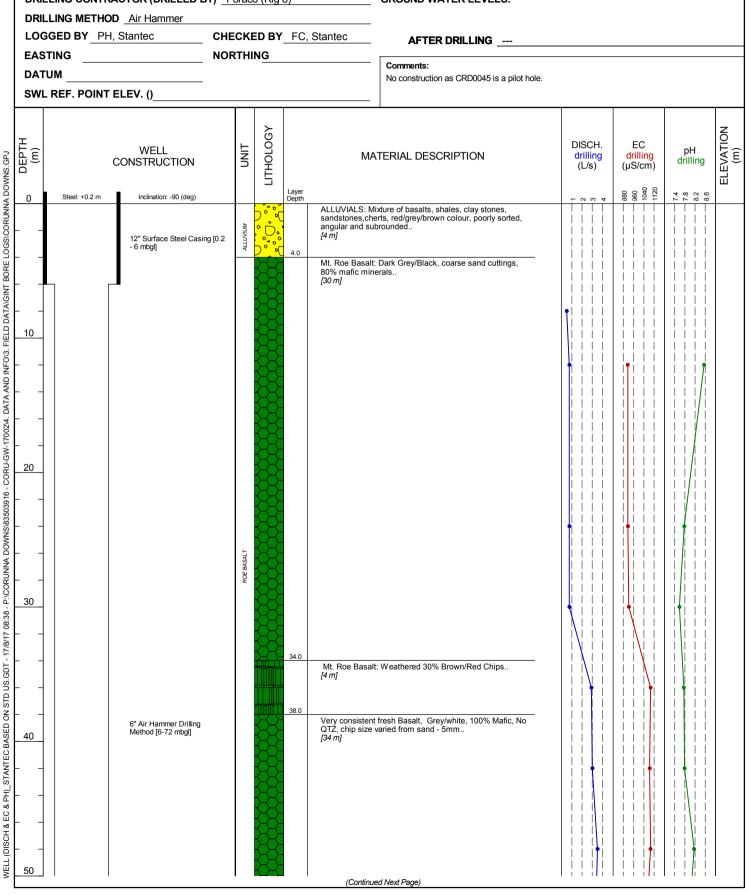
Bottom of borehole at 66.0 m.





EXPLORATION BORE CRD0045 (Complete)

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs H | /drogeologica | al Investigati | ons | |
|------------------------------|------------------------|--|---------------|----------------|-----|-------------|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs | | | | |
| DATE STARTED 12/4/17 | COMPLETED | HOLE DIAMETER 304.8/152.4 mm | | | | |
| DRILLING CONTRACTOR (DRILLEI | DBY) Foraco (Rig 8) | GROUND WATER LEVELS: | | | | |
| DRILLING METHOD Air Hammer | | <u> </u> | | | | |
| LOGGED BY PH, Stantec | CHECKED BY FC, Stantec | AFTER DRILLING | | | | |
| EASTING | NORTHING | | | | | |
| DATUM | | Comments: No construction as CRD0045 is a pilot hole. | | | | |
| SWL REF. POINT ELEV. () | | | | | | |
| H (c) WELL | NLOGY | MATERIAL DESCRIPTION | DISCH. | EC drilling | pН | ATION n) |







EXPLORATION BORE CRD0045 (Complete)

| 0.15 | TAIT Add to locate I too too d | | | | | PROJECT NAME COMMON POWER IN | alan an alla ad an | -1 los | | |
|-----------|--|----------------------|------------|-----------|---------------------------------|--|-----------------------------|---------------------------|-------|------------------|
| | | | | | | PROJECT NAME Corunna Downs Hy | | | | |
| | | | | | | | | | | |
| | | | | | | HOLE DIAMETER 304.8/152.4 mm | | | | |
| DRII | LLING CONTRACTOR (DRILLED E | 3Y) <u>Fo</u> | oraco | o (Rig | 8) | GROUND WATER LEVELS: | | | | |
| DRII | LLING METHOD Air Hammer | | | | | | | | | |
| | GGED BY PH, Stantec | | CKE | D BY | FC, Stantec | AFTER DRILLING | | | | |
| EAS | 7645380 7645380 | NOR | THI | NG | | Comments: | | | | |
| DAT | TUM | | | | | No construction as CRD0045 is a pilot hole. | | | | |
| SWL | REF. POINT ELEV. () | | | | | | | | | |
| OEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | TINN | LITHOLOGY | Layer Depth | TERIAL DESCRIPTION fresh Basalt, Grey/white, 100% Mafic, No | DISCH. drilling (L/s) | EC drilling (µS/cm) | 4:7 H | ELEVATION (m) |
| 60 | | | ROE BASALT | | QTZ, chip size [34 m] (continue | varied from sand - 5mm | | | | |

Bottom of borehole at 72.0 m.





| | ENT Atlas Iron | | | | | | | | | |
|--------------|----------------|---------------------------------|------|--------|----------------|---|---|-----------------------------|------------------------------|---------------|
| | | ER 83503916 | | | | | LOCATION Corruna Downs HOLE DIAMETER 203.2/152.4 mm | | | |
| | | | | | | | | | | |
| | | RACTOR (DRILLED E | | | | | | | | |
| | | | | | | 011- | - <u>-</u> ` ` <i>'</i> — | _ | | |
| | | r,Stantec | | | | ,Stantec | AFTER DRILLING | | | |
| | | 84 | | HING_ | | | Comments: | | | |
| GR | OUND ELEVA | TION | DATU | М | | | Water inject until 24m rod change. No construction as C | RD0051 is a pilot hole |) . | |
| DEPTH (m) | | WELL CONSTRUCTION | | UNIT | | | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | ELEVATION (m) |
| 0 | Collar: +0.2 m | Inclination: -90 (deg) | | | Layer Depth | | | - N N 4 | 1720 1840 1960 2080 | |
| 10 | | 8" Surface Steel Casing 2 mbgl] | | | 23.9 | occasional irr (to lighter gre blebs of gree [23.9 m] | y fresh, grey to green grey, very fine grained, massive with on oxide coated joints and fractures. Occasional alteration y) and occasional medium to coarse (0.6 to 1mm) grains or n feldspar (?) | | | |
| - | | | | DUFFER | | occasional iro (to lighter gre | y fresh, grey to green grey, very fine grained, massive with on oxide coated joints and fractures. Occasional alteration y) and occasional medium to coarse (0.6 to 1mm) grains or n feldspar (?) | | | |
| 20 | | | | | | [4.9 m] | | | | |
| 30 | | | | | | water went bi [0.1 m] Basalt, mostl occasional iro (to lighter gre | dremely weathered interval in basalt (as above). Drilling rown y fresh, grey to green grey, very fine grained, massive with on oxide coated joints and fractures. Occasional alteration y) and occasional medium to coarse (0.6 to 1mm) grains or n feldspar (?) | | | |
| 40 | | | | | | | | | | |





| LIENT Atlas Iron Limited ROJECT NUMBER 83503916 | | | | | | PROJECT NAME Corunna Downs Hydrogeological Investigations LOCATION Corruna Downs | |
|--|-------|------|-----------|------------------------------|--|--|------------------|
| | | | | | | HOLE DIAMETER _203.2/152.4 mm | |
| | | | | | | GROUND WATER LEVELS: | |
| RILLING METHOD _Air Hamm | | | | | | | |
| DGGED BY DT,Stantec | | | | | | AFTER DRILLING | |
| ASTING 785884 | | | | | | | |
| ROUND ELEVATION_ | | | | | | Comments: Water inject until 24m rod change. No construction as CRD0051 is a pilot hole. | |
| WELL CONSTRUCT | ON | LINU | LITHOLOGY | | | MATERIAL DESCRIPTION drilling (L/s) drilling (μ/s) | C ling (cm) (cm) |
| Inclination: - | (deg) | | | Layer Depth | | resh, grey to green grey, very fine grained, massive with | 1960 |
| 6" Air Hamme Method [2-10 | | ă | | 75.0 75.5 84.5 85.0 | Fracture or ext water went ver hydrogeologic [0.5 m] Basalt, mostly occasional iro (to lighter grey blebs of green (feldspar?) 82 [9 m] Fracture zone penetration rat [0.5 m] Basalt, mostly occasional iro (to lighter grey lighter) and penetration rat [0.5 m] | emely weathered interval in basalt (as above). Drilling dark green and quality thereafter improved - different domain (?). Tesh, grey to green grey, very fine grained, massive with oxide coated joints and fractures. Occasional alteration and occasional medium to coarse (0.6 to 1mm) grains or eldspar (?). Minor pink alteration and/or veining driller described "broken gravel") with increased Tesh, grey to green grey, very fine grained, massive with oxide coated joints and fractures. Occasional alteration and occasional medium to coarse (0.6 to 1mm) grains or eldspar (?). Minor pink alteration and/or veining or eldspar (?). | |



PAGE 3 OF 3

| CLI | ENT Atlas Iron Limited | | | | | PROJECT NAME Corunna Downs Hydrogeologica | al Investigat | ions | |
|-----------|--|----------------|--------|-----------|----------------|---|-----------------------|---------------------------|------------------|
| PRO | DJECT NUMBER 83503916 | | | | | LOCATION Corruna Downs | | | |
| DA | TE STARTED10/11/17 | COM | IPLE | TED | 11/11/17 | HOLE DIAMETER 203.2/152.4 mm | | | |
| DRI | LLING CONTRACTOR (DRILLED | BY) _F | orac | o (Rig | 8) | GROUND WATER LEVELS: | | | |
| DRI | LLING METHOD Air Hammer | | | | | ▼ AT TIME OF DRILLING (Water Cut) _24.00 | m bgl | | |
| LO | GGED BY DT,Stantec | CHE | CKE | D BY | FC,Stantec | AFTER DRILLING | | | |
| | STING 785884 DUND ELEVATION | NOR DAT | | | 554307 | Comments: Water inject until 24m rod change. No construction as CRD005 | i1 is a pilot hole | 3 . | |
| DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | TINO | LITHOLOGY | Layer Depth | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | ELEVATION (m) |
| | | | DUFFER | | 102.0 | | | | |

Bottom of borehole at 102.0 m





| CLIE | NT Atlas Iron | Limited | | | | | PROJECT NAME Corunna Downs Hydrogeolo | gical Investigat | ions | |
|--------------|----------------|--------------------------------------|--------|---------------|----------------|--|--|-----------------------------|------------------------------|-----------|
| PRO. | JECT NUMBER | R 83503916 | | | | | LOCATION Corruna Downs | | | |
| DATE | E STARTED _ | 6/11/07 | COMP | LETED | 7/11/ | 17 | HOLE DIAMETER 203.2/152.4 mm | | | |
| DRIL | LING CONTRA | ACTOR (DRILLED BY | Y) For | aco (Rig | 8) | | GROUND WATER LEVELS: | | | |
| DRIL | LING METHO | Air Hammer | | | | | ▼ AT TIME OF DRILLING (Water Cut) _30 |).50 m bgl | | |
| LOG | GED BY DT, | Stantec | CHEC | KED BY | FC, | Stantec | | _ | | |
| | | | | HING | | | - | | | |
| | - | | | | | | Comments: Inject from surface as in competant rock from start. No cor | estruction as CRD0 | 056 is a pilor ho | ole. |
| DEPTH (m) | (| WELL CONSTRUCTION | H. | LITHOLOGY | | | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (μS/cm) | ELEVATION |
| 0 | Collar: +0.2 m | Inclination: -90 (deg) | | | Layer Depth | | | - 0 E 4 | 1080 1160 1240 1320 | |
| 10 | | 8" Surface Steel Casing [2 mbg[] | | MI ROE BASALT | | grey, very fine jointed/fractur Common iron | e highly weathered to fresh, light to dark grey and green to fine grained, pillow textured, massive to highly ed (difficult to characterise with hammered chips). oxide coats and staining on joints and fractures. Fractures and 33 to 34 m, brown water. | | | |
| 20 | Ţ | | | | 42.0 | increased we (manganese? [6 m] Basalt, highly fine to fine gralron oxide coa [4 m] Fracture zone [1 m] Basalt, weath | weathered to fresh, light to dark grey and green grey, very ained, pillow textured, massive to highly jointed/fractured. within basalt (as above), red brown drilling water | | | |





| PROJECT NUMBER 83503916 | COMPLETE ED BY) Foraco (I CHECKED NORTHING | LOCAT HOLE | DIAMETER _203.2/152.4 mm ND WATER LEVELS: IT TIME OF DRILLING (Water Cut) _30 IFTER DRILLING | 9.50 m bgl | |
|--|---|---|---|-----------------------------|--|
| H (E) WELL CONSTRUCTI | | MATE | RIAL DESCRIPTION | DISCH. drilling (L/s) | 1080 (m) (320) (1080 (m) (320) |
| 50 Inclination: -90 6" Air Hammer Method [2-102] | Drilling | fracture coatings, dark bro [4 m] Basalt, fresh, light to dark massive to highly jointed/f staining on joints and fract [26 m] 80.0 Fracture zone in basalt (as drilling water brown [1 m] Basalt, fresh, light to dark massive to highly jointed/f | grey and green grey, very fine to fine grained, ractured. Occasional iron oxide coats and | 1 | |



PAGE 3 OF 3

| PROJE DATE S DRILLII DRILLII LOGGI | T Atlas Iron Limited CCT NUMBER 83503916 STARTED 6/11/07 ING CONTRACTOR (DRILLED ING METHOD Air Hammer ED BY DT,Stantec ING 782732 | BY) F | orace CKE | o (Rig ED BY NG 76 | 7/11/17 8) FC,Stantec | PROJECT NAME Corunna Downs Hydrogeologica LOCATION Corruna Downs HOLE DIAMETER 203.2/152.4 mm GROUND WATER LEVELS: AT TIME OF DRILLING (Water Cut) 30.50 AFTER DRILLING Comments: | | ons | |
|------------------------------------|--|-------|--------------|--------------------------|-----------------------------|---|-----------------------|---------------------|--------------------|
| HL(W) | WELL CONSTRUCTION Inclination: -90 (deg) | DAT | LINO | ТТНОГОСУ | Layer Depth | Inject from surface as in competant rock from start. No constru | DISCH. drilling (L/s) | EC drilling (µS/cm) | ole. ELEVATION (m) |

Bottom of borehole at 102.0 m





EXPLORATION BORE CRD0057 (Complete)

| | :NT <u>Atlas Iron</u> JECT NUMBEF | | | | | | | PROJECT NAME Corunna Downs LOCATION Corruna Downs | s Hydrogeologic | | | |
|--------------|--------------------------------------|--|--------------------|---------------|-----------|----------|-----------------------------------|---|------------------|---------------|----------|-----------|
| | | | | | | | | HOLE DIAMETER 304.8/152.4 m | | | | |
| | | |) <u>Fo</u> | racc | o (Rig | 8) | | GROUND WATER LEVELS: | | | | |
| | .LING METHOD Ged by DN, | Air Hammer Atlas Iron | CHEC | CKE | D BY | PH, Star | ntec | AFTER ROULING | | | | |
| | | | NORT | | | | | AFTER DRILLING | | | | |
| DAT | | | | | | | | Comments: No construction as CRD0057 is a pilot hole | e. No water cut. | | | |
| SWL | REF. POINT I | ELEV. () | | | | | | | | <u> </u> | <u> </u> | |
| _ | | | | | ĞΥ | | | | | | | NO |
| DEPTH (m) | (| WELL CONSTRUCTION | | LNN | LITHOLOGY | | MA | TERIAL DESCRIPTION | DISCH. (L/s) | EC (µS/cm) | pН | ELEVATION |
| | | | | | 自 | | | | | | | ELE |
| 0 | Steel: +0.2 m | Inclination: -90 (deg) | | |)° « | | LUVIALS: Si | Ity clay | | 0000 | | +- |
| _ | | 12" Surface Steel Casing | m 2 | | | [8] | m] | | | | | |
| - | | - 6 mbgl] | - | > 1 | | | | | | | | |
| _ | | J | | ₹ | | | | | | | | |
| | | | | | ° Do | | | | | | | |
| 10 | | | | | | qu | T ROE BASA ıartz, clay 6 m] | LT: Highly weathered, some iron staining, | | | | |
| | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | |
| + | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | |
| - | | | | | | | | | | | | |
| | | | | | | | | LT: Weathered, hard, light grey (no water) | | | | |
| | | | | | | [48 | 8 m] | | | | | |
| | | | | 4SALT | | | | | | | | |
| 30 | | | | MT ROE BASALT | | | | | | | | |
| | | | | < | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| 40 | | 6" Air Hammer Drilling Method [6-72 mbgl] | | | | | | | | | | |
| 40 | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| . | | | | | | | | | | | | |
| 50 | | | | | | | | | | | | |





EXPLORATION BORE CRD0057 (Complete)

| CLIENT Atlas Iron Limited | | | | | | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | | | | |
|---|--|---------------------------------|------------------------|-----------|----------------|--------------------------------|---|-----------------|---------------|----|------------------|--|
| PROJECT NUMBER 83503916 | | | | | | | LOCATION Corruna Downs | | | | | |
| DAT | E STARTED 10/4/17 | COMPLETED <u>10/4/17</u> | | | | | HOLE DIAMETER 304.8/152.4 mm | | | | | |
| DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) | | | | | | GROUND WATER LEVELS: | | | | | | |
| DRII | LLING METHOD _Air Hammer | | | | | | | | | | | |
| LOGGED BY DN, Atlas Iron | | | CHECKED BY PH, Stantec | | | | AFTER DRILLING | | | | | |
| EASTING | | | THI | NG | | | | | | | | |
| DATUM | | | | | | | Comments: No construction as CRD0057 is a pilot hole. No v | vater cut | | | | |
| SWL REF. POINT ELEV. () | | | | | | | The constituction as Grabous is a pilot noise. No v | rater cut. | | | | |
| 05 DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | TINO | LITHOLOGY | Layer Depth | MA | TERIAL DESCRIPTION | DISCH. (L/s) | EC (µS/cm) | рН | ELEVATION (m) | |
| | | | | | | MT ROE BASAI [48 m] (continued | .T: Weathered, hard, light grey (no water) | | | | | |

MT ROE BASALT

Bottom of borehole at 72.0 m.

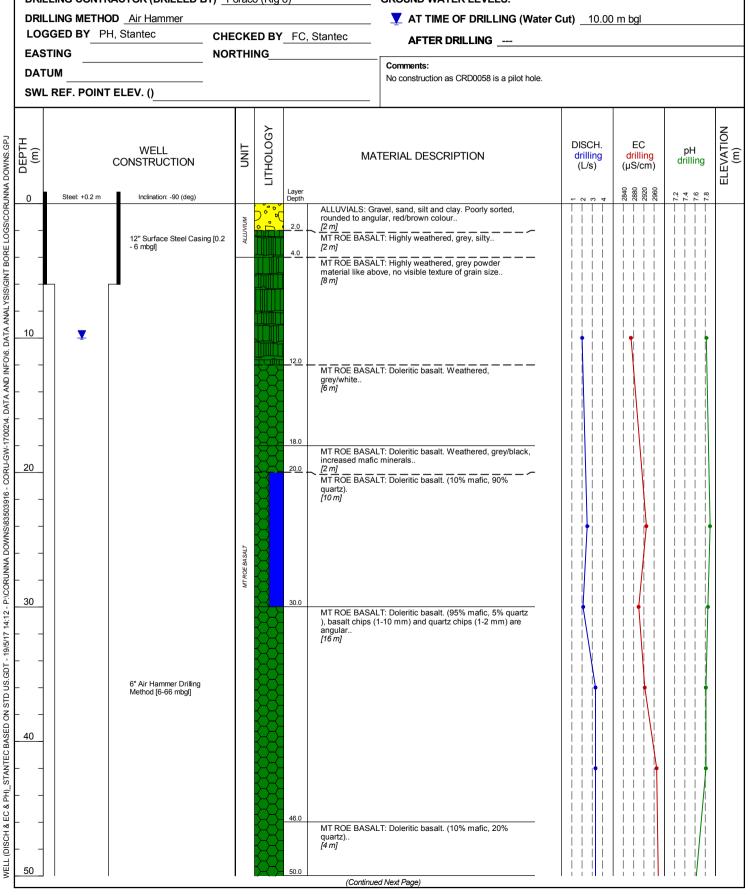
70





EXPLORATION BORE CRD0058 (Complete)

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | |
|--------------------------------|--------------------------|--|--|--|
| Atias non Limited | | PROJECT NAME COlumna Downs Trydrogeological Investigations | | |
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs | | |
| DATE STARTED 11/4/17 | COMPLETED 12/4/17 | HOLE DIAMETER 304.8/152.4 mm | | |
| DRILLING CONTRACTOR (DRILLED I | SY) Foraco (Rig 8) | _ GROUND WATER LEVELS: | | |
| DRILLING METHOD Air Hammer | | AT TIME OF DRILLING (Water Cut) 10.00 m bgl | | |
| LOGGED BY PH, Stantec | CHECKED BY FC, Stantec | AFTER DRILLING | | |
| EASTING | NORTHING | | | |
| | | Comments: | | |
| DATUM | | No construction as CRD0058 is a pilot hole. | | |
| SWL REF. POINT ELEV. () | | - | | |







EXPLORATION BORE CRD0058 (Complete)

| CLII | ENT Atlas Iron Limited | | | | | | PROJECT NAME Corunna Downs H | ydrogeologica | al Investigat | ions | |
|-------------------------|--|--------|---------------|-----------|-----------------------|------------------------|--|-----------------------|---------------------------|-----------------------------|---------------|
| PROJECT NUMBER 83503916 | | | | | | LOCATION Corruna Downs | | | | | |
| DAT | TE STARTED 11/4/17 | СОМ | IPLE | TED | 12/4/17 | | HOLE DIAMETER _304.8/152.4 mm | | | | |
| DRII | LLING CONTRACTOR (DRILLED I | BY) Fo | oraco | o (Rig | 8) | | GROUND WATER LEVELS: | | | | |
| DRII | LLING METHOD Air Hammer | | | | | | ▼ AT TIME OF DRILLING (Water) | Cut) 10.00 |) m bgl | | |
| | GGED BY PH, Stantec | CHE | | | FC, Stantec | | AFTER DRILLING | , | | | |
| DAT | L REF. POINT ELEV. () | | | | | | Comments: No construction as CRD0058 is a pilot hole. | | | | |
| G DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | TINO | LITHOLOGY | Layer Depth | MA | TERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | bH drilling bH 8.7 | ELEVATION (m) |
| 60 | | | MT ROE BASALT | | MT ROE quartz) [16 m] | | LT: Doleritic basalt. (10% mafic, 40% | | | | |

Bottom of borehole at 66.0 m.

PAGE 1 OF 2



EXPLORATION BORE CRD0078 (Complete)

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | | | |
|--------------------------------|------------------------|---|--|--|--|--|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs | | | | |
| DATE STARTED 8/5/17 | COMPLETED 8/5/14 | HOLE DIAMETER _ 304.8/152.4 mm | | | | |
| DRILLING CONTRACTOR (DRILLED B | BY) Foraco (Rig 8) | GROUND WATER LEVELS: | | | | |
| DRILLING METHOD Air Hammer | | AT TIME OF DRILLING (Water Cut) 36.00 m bgl | | | | |
| LOGGED BY PH, Stantec | CHECKED BY FC, Stantec | AFTER DRILLING | | | | |
| EASTING | NORTHING | | | | | |
| DATUM | | Comments: No construction as CRD0078 is a pilot hole. | | | | |
| SWL REF. POINT ELEV. () | | | | | | |
| | <u> </u> | | | | | |

ELEVATION (m) LITHOLOGY DEPTH (m) WELL (DISCH & EC & PH)_STANTEC BASED ON STD US.GDT - 19/5/17 14/13 - P./CORUNNA DOWNS/83503916 - CORU-GW-170024. DATA AND INFO%. DATA ANALYSIS/GINT BORE LOGS/CORUNNA DOWNS. GPJ DISCH. LNS WELL EC drilling (L/s) MATERIAL DESCRIPTION рΗ CONSTRUCTION (µS/cm) 0 Steel: +0.2 m Inclination: -90 (deg) DETRITAL SEDIMENTS: Grey silt powder (90%), highly weathered yellow/white/brown angular claystones/mudstones chips (10%).. 12" Surface Steel Casing [0.2 - 6 mbgl] DETRITAL SEDIMENTS: Light brown silt powder. [8 m] DETRITALS 10 DUFFER FORMATION: Grey silt powder (90%), red/white angular jasperlitic chert chips (10%)... [2 m] DUFFER FORMATION: Red silt powder (90%), highly weathered, grey, pitted volcanic rock (10%).. [4 m] D 20 20.0 DUFFER FORMATION: Red/brown silt powder (95%), highly weathered, grey, pitted volcanic rock (50%) (SEE PHOTO).. [10 m] b 1 30 DUFFER FORMATION: Red clay powder (98%), grey/green fine grained, very well sorted with minor red fleck (2%) (SEE PHOTO).. **DUFFER FORMATION** 40 6" Air Hammer Drilling Method [6-82 mbgl] DUFFER FORMATION: Grey powder, no solid cuttings... 50 (Continued Next Page)





EXPLORATION BORE CRD0078 (Complete)

| Layer Depth DUFFER FORMATION: Grey powder, no solid cuttings | EC (μS/cm) pH |
|--|---------------|
| Layer Depth | |
| DUFFER FORMATION: Grey powder, no solid cuttings DUFFER FORMATION: Grey powder, no solid cuttings | 0 0 0 0 |
| 70 To To To To To To To T | |
| Bottom of borehole at 82.0 m. | |





EXPLORATION BORE CRD0081

| PROJECT DATE STA DRILLING DRILLING LOGGED EASTING GROUND | T NUMBER <u>83503916</u> ARTED <u>11/11/17</u> | 3 | | · · · | | | |
|---|---|----------------------|---|--|----------------------------|--|--|
| DATE STA DRILLING DRILLING LOGGED EASTING GROUND | ARTED 11/11/17 | | | | | | |
| DRILLING DRILLING LOGGED EASTING GROUND HLdg 0 Coll | | COMPLETED | 12/11/17 HOLE DIAMETER 203.2/152.4 mm | HOLE DIAMETER _203.2/152.4 mm | | | |
| DRILLING LOGGED EASTING GROUND HLdag 0 Coll | ::::::::::::::::::::::::::::::::::: | LLED BY) Foraco (Rig | | | | | |
| LOGGED EASTING GROUND HLdad O Colle | • METHOD _Air Hamm | | AT TIME OF DRILLING (Water Cur | t) 24.00 m bal | | | |
| EASTING GROUND HLGEO O Coll | DBY DT,Stantec | | FC,Stantec AFTER DRILLING | | | | |
| GROUND HLdad O Coll. | 785348 | | | | | | |
| 0 Coll. | DELEVATION | | Comments: | Water Injection necessary for large component of the drilling. No construction as CRD0081 is a | | | |
| | WELL CONSTRUC | NNIT LITHOLOGY | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | | |
| | ollar: +0.2 m Inclination: - | | Layer Depth | - N W 4 | 760 920 1080 1240 | | |
| 10 | 8" Surface Si 2 mbgl] | teel Casing [0.2 - | Colluvium, basalt chips, iron oxides common but otherwise fresh [1 m] Basalt, light to dark grey and green grey, very fine grained, massive to weakly foliated, iron oxide coats common [17 m] | | | | |
| 20 | ¥ | | Basalt, altered to light tan to green grey, very fine grained, massive to weakly foliated, iron oxide coats common [14 m] | | | | |
| 30 | | DUFFER | Basalt, light to dark grey and green grey, very fine grained, massive to weakly foliated, iron oxide coats common [12 m] | | | | |
| 50 | | | 44.0 Fractured zone in basalt (as above), but with greatly increased iron ox | ;;;; | | | |

(Continued Next Page)





EXPLORATION BORE CRD0081

| PROJECT DATE STATEMENT OF THE PROJECT DRILLIN LOGGE EASTIN | CLIENT Atlas Iron Limited PROJECT NUMBER 83503916 DATE STARTED 11/11/17 COMPLETED 12/11/17 DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) DRILLING METHOD Air Hammer LOGGED BY DT, Stantec CHECKED BY FC, Stantec EASTING 785348 NORTHING 7654094 GROUND ELEVATION DATUM | | | | LOCATION Corruna Downs HOLE DIAMETER 203.2/152.4 mm GROUND WATER LEVELS: AT TIME OF DRILLING (Water Cut) AFTER DRILLING Comments: | LOCATION Corruna Downs HOLE DIAMETER 203.2/152.4 mm GROUND WATER LEVELS: AT TIME OF DRILLING (Water Cut) 24.00 m bgl AFTER DRILLING Comments: Water Injection necessary for large component of the drilling. No construction as CRD0081 is a | | | |
|---|--|--------|-----------|-------|---|--|---------------------|--|--|
| DEPTH (m) | WELL CONSTRUCTION | FNO | ГІТНОГОСУ | Layer | MATERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | | |
| 50 50 60 60 60 60 60 60 60 60 60 60 60 60 60 | 6" Air Hammer Drilling Method [2-102 mbgl] | DUIFER | | Depth | Basalt, light to dark grey and green grey, very fine grained, massive to weakly foliated, iron oxide coats common. Water injection while drilling throughout. Fracture zones at 50 to 52 m and 54 to 56 m, but no increase in yields. Trace large chips of vesicular basalt with iron oxide coats throughout but likely to be uphole contamination, and no increase in yields [54 m] (continued) | | 22 | | |
| WELL (DISCAR REG) - STAN BE GRAED ON STD US. SDT - 9/2/18 18:13 - DISCORUNNA DOWNS GAD 000 000 000 000 000 000 000 | | | | | (Continued Next Page) | | | | |



EXPLORATION BORE CRD0081

PAGE 3 OF 3

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations |
|---|---------------------------|--|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs |
| DATE STARTED _11/11/17 | COMPLETED 12/11/17 | |
| DRILLING CONTRACTOR (DRILLED I | BY) Foraco (Rig 8) | GROUND WATER LEVELS: |
| DRILLING METHOD Air Hammer | | AT TIME OF DRILLING (Water Cut) 24.00 m bgl |
| LOGGED BY DT,Stantec | CHECKED BY FC,Star | ntec AFTER DRILLING |
| EASTING 785348 GROUND ELEVATION | 785348 DATUM | Comments: Water Injection necessary for large component of the drilling. No construction as CRD0081 is a pilot hole. |
| WELL CONSTRUCTION Inclination: -90 (deg) | LITHOLOGY Petty | MATERIAL DESCRIPTION DISCH. drilling (L/s) (L/s) (EC drilling (µS/cm) (PS/cm) (EX V V V V V V V V V |
| | 102.0 BW W | Basalt, light to dark grey and green grey, very fine grained, massive to veakly foliated, iron oxide coats common. Water injection while drilling hroughout. Fracture zones at 50 to 52 m and 54 to 56 m, but no norease in yields. Trace large chips of vesicular basalt with iron oxide coats throughout but likely to be uphole contamination, and no increase in yields 54 m] (continued) |

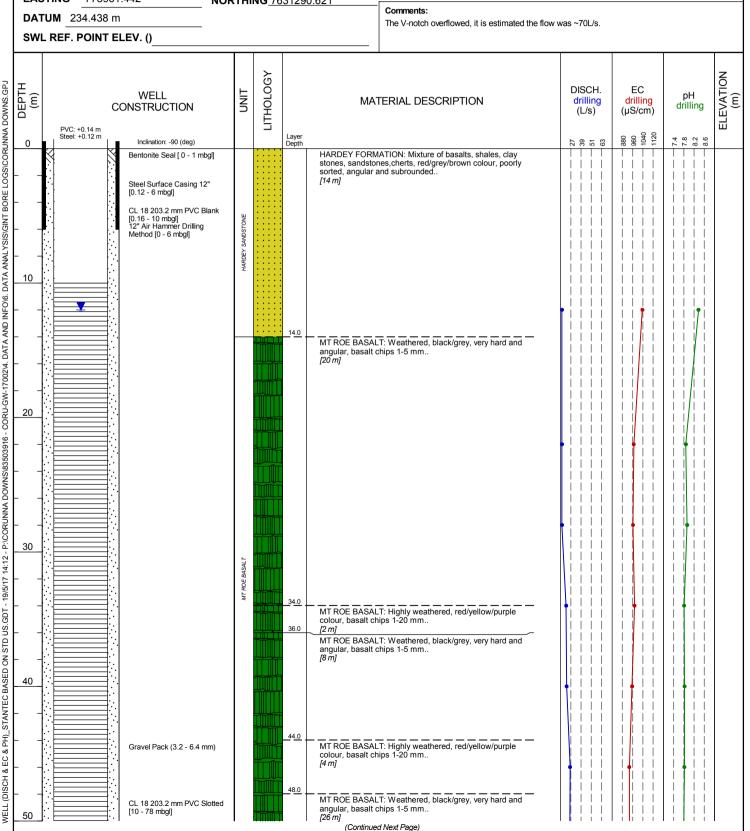
Bottom of borehole at 102.0 m

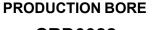




PRODUCTION BORE CRD0082

PROJECT NAME Corunna Downs Hydrogeological Investigations **CLIENT** Atlas Iron Limited PROJECT NUMBER 83503916 LOCATION Corruna Downs DATE STARTED 13/4/17 HOLE DIAMETER 304.8/254 mm **COMPLETED** 16/4/17 DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **GROUND WATER LEVELS: DRILLING METHOD** Air Hammer ▼ AT TIME OF DRILLING (Water Cut) 12.00 m bgl LOGGED BY PH, Stantec CHECKED BY FC, Stantec AFTER DRILLING _---**EASTING** 778961.442 NORTHING 7631290.621 Comments: **DATUM** 234.438 m The V-notch overflowed, it is estimated the flow was ~70L/s.





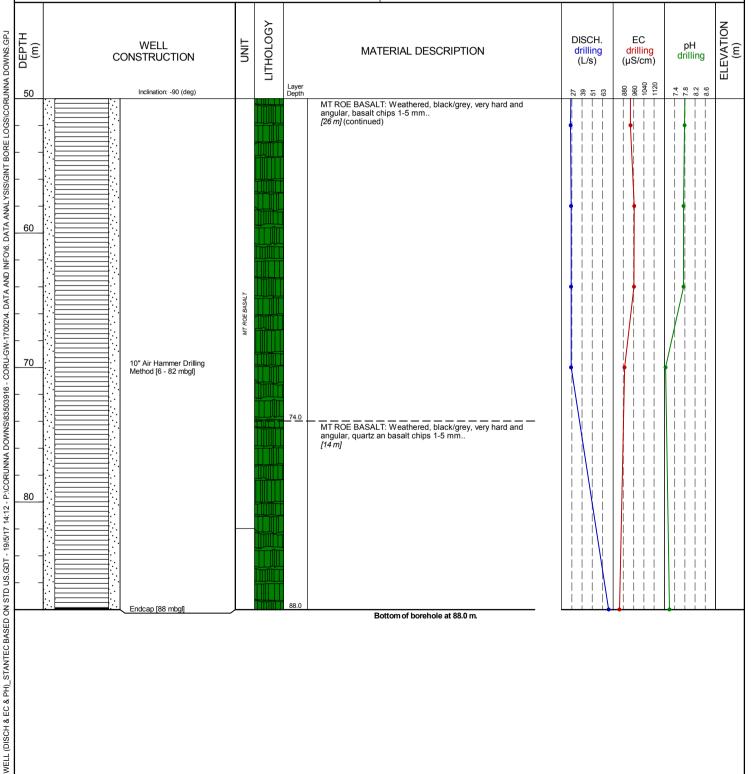


Stantec

CRD0082

PAGE 2 OF 2

CLIENT Atlas Iron Limited PROJECT NAME Corunna Downs Hydrogeological Investigations PROJECT NUMBER 83503916 LOCATION Corruna Downs DATE STARTED 13/4/17 **COMPLETED** 16/4/17 HOLE DIAMETER 304.8/254 mm DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **GROUND WATER LEVELS: DRILLING METHOD** Air Hammer ▼ AT TIME OF DRILLING (Water Cut) 12.00 m bgl LOGGED BY PH, Stantec CHECKED BY FC, Stantec AFTER DRILLING _---**EASTING** 778961.442 NORTHING 7631290.621 Comments: **DATUM** 234.438 m The V-notch overflowed, it is estimated the flow was ~70L/s. SWL REF. POINT ELEV. ()





Stantec

PRODUCTION BORE CRD0083

CLIENT Atlas Iron Limited PROJECT NAME Corunna Downs Hydrogeological Investigations PROJECT NUMBER 83503916 LOCATION Corruna Downs DATE STARTED 17/4/17 HOLE DIAMETER 304.8/254 mm **COMPLETED** 23/4/17 DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **GROUND WATER LEVELS: DRILLING METHOD** Air Hammer ▼ AT TIME OF DRILLING (Water Cut) 22.00 m bgl LOGGED BY PH/FC, Stantec CHECKED BY FC, Stantec **EASTING** 778575.622 NORTHING 7632987.081 Comments: **DATUM** 231 m Delays due to damaged spacer on drill bit and two early stoppages for lightning.

SWL REF. POINT ELEV. (0.16) ELEVATION (m) LITHOLOGY DEPTH (m) WELL (DISCH & E.C. & PH)-STANTEC BASED ON STD US.GDT - 19/5/17 14:11 - P./CORUNNA DOWNS/83503916 - CORU-GW-170024, DATA AND INFO/6. DATA ANALYSIS/GINT BORE LOGS/CORUNNA DOWNS, GPJ DISCH. EC LNS WELL рΗ MATERIAL DESCRIPTION drilling (L/s) drilling drilling CONSTRUCTION (uS/cm) PVC: +0.16 m Steel: +0.22 m 640 680 720 760 7.4 7.8 8.2 8.2 2 2 2 Inclination: -90 (deg) Bentonite seal [0.5 - 0 m] ALLUVIALS: Gravel, sand, silt and clay. Poorly sorted, rounded to angular, red/brown colour.. [4 m] Steel Surface Casing 12" (0.22 - 6 mbgl) CL 18 203.2 mm PVC Blank (0.16 - 6 mbgl) 12" Air Hammer Drilling Method [0 - 6mbgl] ∇ MT ROE BASALT: Extremely weathered, dry powder... 20 20.0 MT ROE BASALT: Doleritic basalt. Highly weathered, clay with basalt frgaments 1-20 mm. (60% mafic, 30% quartz, 10% clay).. MT ROE BASALT: Doleritic basalt. Weathered, light grey (10% mafic, 90% quartz)... [12 m] MT ROE BASALT 30 36.0 MT ROE BASALT: Doleritic basalt. Weathered, darker grey (40% mafic, 60% quartz). [16 m] 40 Gravel Pack (3.2-6.4mm) [0.5 - 82mbgl] CL 18 203.2 mm PVC Slotted [6 - 78 mbgl] (Continued Next Page)



SWL REF. POINT ELEV. (0.16)

PRODUCTION BORE CRD0083

PAGE 2 OF 2

CLIENT Atlas Iron Limited

PROJECT NUMBER 83503916

DATE STARTED 17/4/17 COMPLETED 23/4/17

DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8)

DRILLING METHOD Air Hammer

LOGGED BY PH/FC, Stantec CHECKED BY FC, Stantec

EASTING 778575.622 NORTHING 7632987.081

DATUM 231 m

PROJECT NAME Corunna Downs Hydrogeological Investigations

LOCATION Corruna Downs

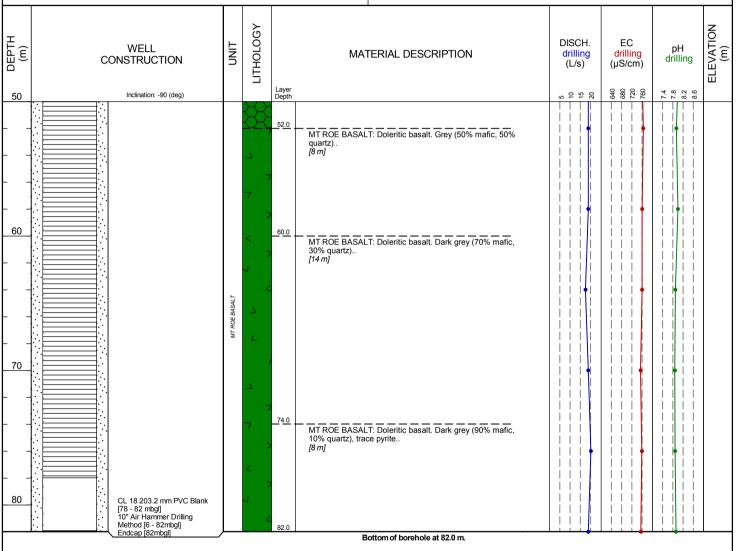
HOLE DIAMETER 304.8/254 mm

GROUND WATER LEVELS:

▼ AT TIME OF DRILLING (Water Cut) 22.00 m bgl

Comments:

Delays due to damaged spacer on drill bit and two early stoppages for lightning.



WELL (DISCH & EC & PH)_STANTEC BASED ON STD US.GDT - 19/5/17 14:11 - P./CORUNNA DOWNS/83503916 - CORU-GW-1700214. DATA AND INFO/6. DATA ANALYSIS/GINT BORE LOGS/CORUNNA DOWNS. GPJ





PRODUCTION BORE CRD0084

CLIENT Atlas Iron Limited PROJECT NAME Corunna Downs Hydrogeological Investigations PROJECT NUMBER 83503916 LOCATION Corruna Downs DATE STARTED 24/4/17 HOLE DIAMETER 304.8/254 mm **COMPLETED** <u>26/4/17</u> DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **GROUND WATER LEVELS: DRILLING METHOD** Air Hammer AT TIME OF DRILLING (Water Cut) 24.00 m bgl LOGGED BY FC, Stantec CHECKED BY PH, Stantec 3.77 m brp= RL 199.37 m (30/04/2017 7:30:00 AM) **▼** AFTER DRILLING **EASTING** 778983.549 NORTHING 7641951.676 Comments: **DATUM** 203.135 m At 26m hit possible fractured zone as the water came out from the monitoring bore on the same pad.

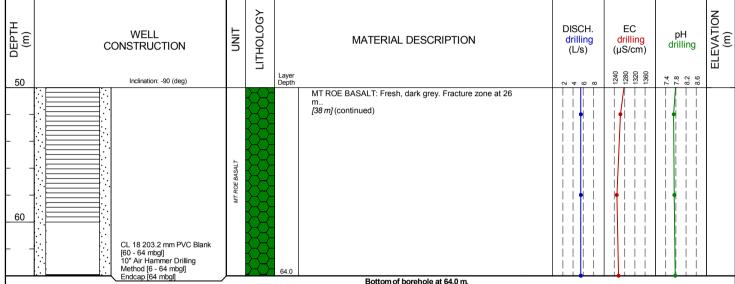
SWL REF. POINT ELEV. (0.32) ELEVATION (m) LITHOLOGY DEPTH (m) WELL (DISCH & E.C. & PH)_STANTEC BASED ON STD US.GDT - 19/5/17 14:13 - P:\CORUNNA DOWNS\83503916 - CORU-GW-170024. DATA AND INFO\8. DATA AND INFO\8. DATA ANALYSIS\GINT BORE LOGS\CORUNNA DOWNS\.GPJ DISCH. EC LIND WELL рΗ MATERIAL DESCRIPTION drilling (L/s) drilling CONSTRUCTION drilling (µS/cm) PVC: +0.32 m Steel: +0.51 m 1240 1280 1320 1360 7.4 7.8 8.2 8.2 Inclination: -90 (deg) Bentonite Seal [0.5 - 0 mbgl] ALLUVIALS: Gravel, sand, silt and clay. Poorly sorted, rounded to angular, red/brown colour. Calcrete at 6 m.. [8 m] CL 18 203.2 mm PVC Blank CL 18 203.2 mm PVC Bla [0.32 - 6 mbgl] Steel Surface Casing 12" [0.51 - 6.5 mbgl] 12" Air Hammer Drilling Method [0 - 6.5 mbgl] ∇ ALLUVIUM MT ROE BASALT: Highly weathered with grey clay, basalt chips (1-20 mm).. $[18\,m]$ 20 26.0 MT ROE BASALT: Fresh, dark grey. Fracture zone at 26 [38 m] WT ROE BASAL1 30 Gravel pack (3.2 - 6.4 mm) CL 18 203.2 mm PVC Slotted [6 - 60 mbgl] 40 (Continued Next Page)



PRODUCTION BORE CRD0084

PAGE 2 OF 2

CLIENT Atlas Iron Limited PROJECT NAME Corunna Downs Hydrogeological Investigations PROJECT NUMBER 83503916 LOCATION Corruna Downs DATE STARTED 24/4/17 **COMPLETED** 26/4/17 HOLE DIAMETER 304.8/254 mm DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **GROUND WATER LEVELS: DRILLING METHOD** Air Hammer ▼ AT TIME OF DRILLING (Water Cut) 24.00 m bgl LOGGED BY FC, Stantec CHECKED BY PH, Stantec **EASTING** 778983.549 **NORTHING** 7641951.676 Comments: **DATUM** 203.135 m At 26m hit possible fractured zone as the water came out from the monitoring bore on the same pad. SWL REF. POINT ELEV. (0.32)



Bottom of borehole at 64.0 m.





PRODUCTION BORE CRD0085

CLIENT Atlas Iron Limited PROJECT NUMBER 83503916 DATE STARTED 27/4/17 **COMPLETED** <u>30/4/17</u> **DRILLING CONTRACTOR (DRILLED BY)** Foraco (Rig 8) **DRILLING METHOD** Air Hammer LOGGED BY RK2, Stantec CHECKED BY FC, Stantec **EASTING** 780807.982 **NORTING** 7642040.047 **DATUM** 204.917 m

PROJECT NAME Corunna Downs Hydrogeological Investigations

LOCATION Corruna Downs

HOLE DIAMETER 304.8/254 mm

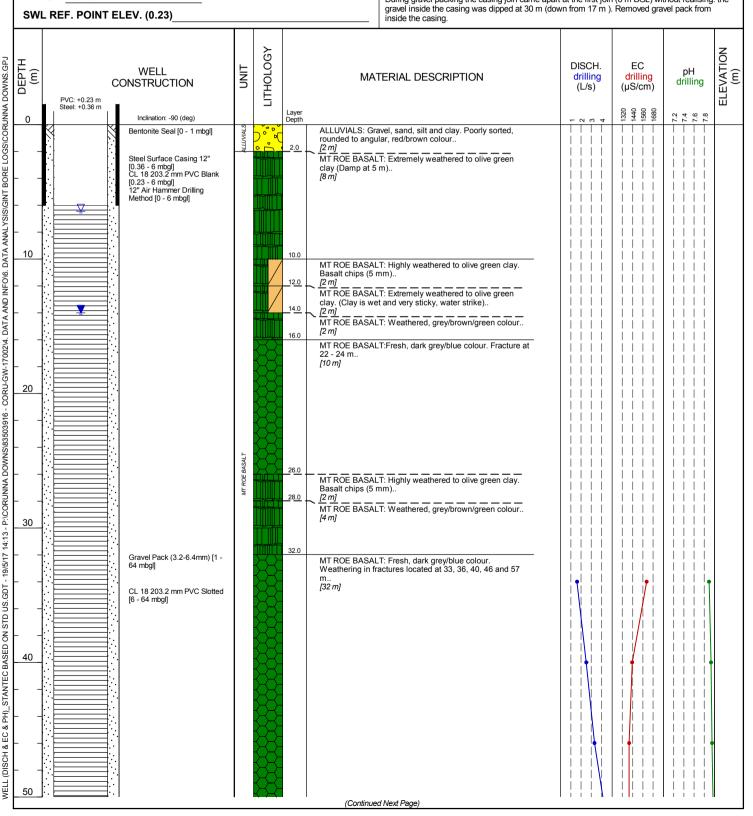
GROUND WATER LEVELS:

AT TIME OF DRILLING (Water Cut) 14.00 m bgl

✓ **AFTER DRILLING** 6.70 m brp= RL 198.217 m (01/05/2017 7:44:00 AM)

Comments:

During gravel packing the casing join came apart at the first join (6 m BGL) without realising. the







SWL REF. POINT ELEV. (0.23)

PRODUCTION BORE **CRD0085**

CLIENT Atlas Iron Limited PROJECT NUMBER 83503916 DATE STARTED 27/4/17 **COMPLETED** 30/4/17 DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) **DRILLING METHOD** Air Hammer LOGGED BY RK2, Stantec CHECKED BY FC, Stantec **EASTING** 780807.982 **NORTHING** 7642040.047 **DATUM** 204.917 m

PROJECT NAME Corunna Downs Hydrogeological Investigations

LOCATION Corruna Downs

HOLE DIAMETER 304.8/254 mm

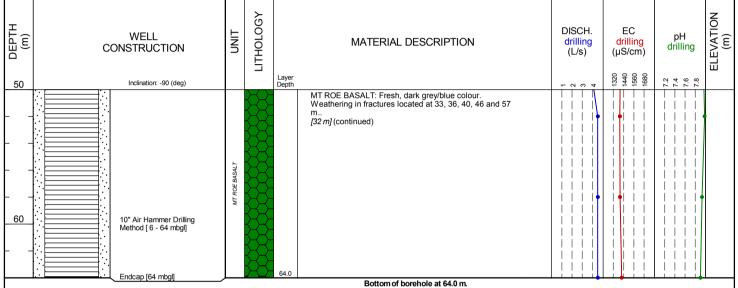
GROUND WATER LEVELS:

AT TIME OF DRILLING (Water Cut) 14.00 m bgl

✓ **AFTER DRILLING** 6.70 m brp= RL 198.217 m (01/05/2017 7:44:00 AM)

Comments:

During gravel packing the casing join came apart at the first join (6 m BGL) without realising. the gravel inside the casing was dipped at 30 m (down from 17 m). Removed gravel pack from inside the casing.

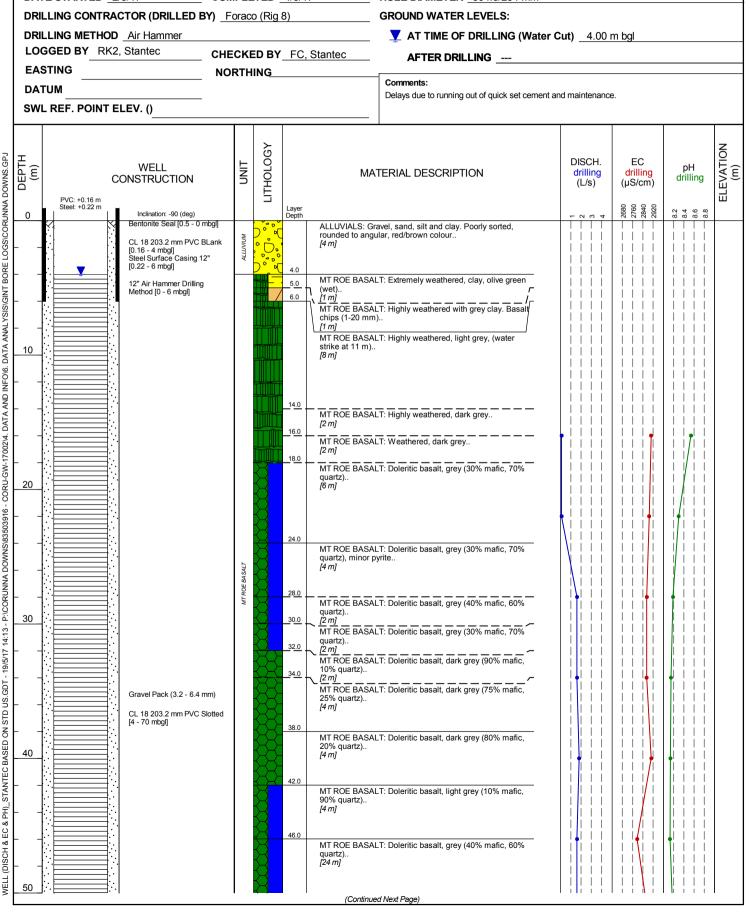


PAGE 1 OF 2

Stantec

PRODUCTION BORE **CRD0086**

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | | |
|---|------------------------|---|--|--|--|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs | | | |
| DATE STARTED 2/5/17 | COMPLETED 4/5/17 | HOLE DIAMETER 304.8/254 mm | | | |
| DRILLING CONTRACTOR (DRILLED I | BY) Foraco (Rig 8) | GROUND WATER LEVELS: | | | |
| | | | | | |
| DRILLING METHOD Air Hammer | | AT TIME OF DRILLING (Water Cut) | | | |
| DRILLING METHOD Air Hammer LOGGED BY RK2, Stantec | CHECKED BY FC, Stantec | AT TIME OF DRILLING (Water Cut) 4.00 m bgl AFTER DRILLING | | | |
| | CHECKED BY FC, Stantec | | | | |
| LOGGED BY RK2, Stantec | | | | | |

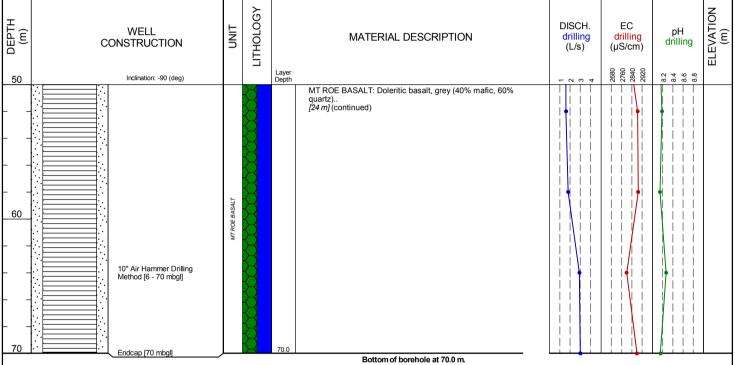




Stantec

PRODUCTION BORE CRD0086

| CLIENT Atlas Iron Limited | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | |
|--------------------------------|------------------------|---|--|--|
| PROJECT NUMBER 83503916 | | LOCATION Corruna Downs | | |
| DATE STARTED _2/5/17 | COMPLETED 4/5/17 | HOLE DIAMETER 304.8/254 mm | | |
| DRILLING CONTRACTOR (DRILLED E | SY) Foraco (Rig 8) | GROUND WATER LEVELS: | | |
| DRILLING METHOD Air Hammer | | ▼ AT TIME OF DRILLING (Water Cut) _ 4.00 m bgl | | |
| LOGGED BY RK2, Stantec | CHECKED BY FC, Stantec | AFTER DRILLING | | |
| EASTING | NORTHING | | | |
| DATUM | <u>-</u> | Comments: Delays due to running out of quick set cement and maintenance. | | |
| SWL REF. POINT ELEV. () | | Soldyo dad to raining out or quick out contains and maintenance. | | |
| | | | | |

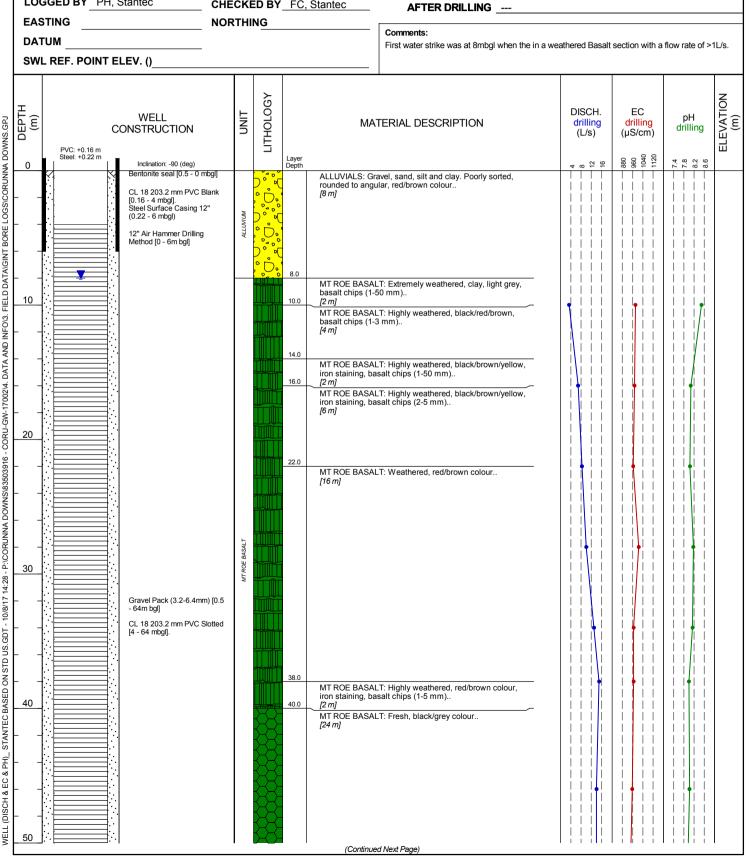






PRODUCTION BORE CRD0087

| CLIENT Atlas Iron Limited | | | PROJECT NAME Corunna Downs Hydrogeological Investigations | | | | |
|------------------------------|---------------------------|------------|--|-----------------------------|---------------------------|----------------|----------------|
| PROJECT NUMBER 83503916 | | | LOCATION Corruna Downs | | | | |
| DATE STARTED 5/5/17 | COMPLETED 8/5 | 5/17 | HOLE DIAMETER 304.8/254 mm | | | | |
| DRILLING CONTRACTOR (DRILLED | 3Y) Foraco (Rig 8) | | GROUND WATER LEVELS: | | | | |
| DRILLING METHOD _Air Hammer | | | AT TIME OF DRILLING (Water Cut) 8.00 m bgl | | | | |
| LOGGED BY PH, Stantec | CHECKED BY_F | C, Stantec | AFTER DRILLING | | | | |
| EASTING | NORTHING | | | | | | |
| DATUM | | | Comments: First water strike was at 8mbgl when the in a weathered Basalt section with a flow rate of >1L/s. | | | | |
| SWL REF. POINT ELEV. () | | | | | | | |
| WELL CONSTRUCTION | UNIT | MA | TERIAL DESCRIPTION | DISCH. drilling (L/s) | EC drilling (µS/cm) | pH drilling | EVATION (m) |







10" Air Hammer Drilling Method [6 - 64 mbgl]

Endcap [64 mbgl]

PRODUCTION BORE CRD0087

| CI II | ENT Atlan Iron Limited | | | | | | DDO IECT NAME Corumna Douma III | dragalagia | al lavasticati | iono. | |
|-----------------------|--|---------------------|------------------------|---------------|----------------|-------------------------------|---|------------------|---------------------------|---|------------------|
| | ENT Atlas Iron Limited | | | | | | PROJECT NAME Corunna Downs H | /urogeologica | ı mvesugau | Oris | |
| | DJECT NUMBER <u>83503916</u> | | | | | | LOCATION Corruna Downs | | | | |
| DAT | TE STARTED <u>5/5/17</u> | COM | PLE | TED | 8/5/1 | 7 | HOLE DIAMETER 304.8/254 mm | | | | |
| DRII | LLING CONTRACTOR (DRILLED E | 3Y) <u>F</u> | oracc | (Rig | 8) | | GROUND WATER LEVELS: | | | | |
| DRII | LLING METHOD Air Hammer | | | | | | AT TIME OF DRILLING (Water | Cut) 8.00 | m bgl | | |
| LOGGED BY PH, Stantec | | | CHECKED BY FC, Stantec | | | Stantec | AFTER DRILLING | | | | |
| EAS | EASTING NORTHING | | | A TENDIALENCE | | | | | | | |
| DAT | гим | | | | | | Comments: | andbarrad Danald | | fla | 41 /- |
| | L REF. POINT ELEV. () | | | | | | First water strike was at 8mbgl when the in a w | eathered Basan | section with a | now rate or > | IL/S. |
| | | | | | | | | 1 | 1 | | 1 |
| ы DEPTH (m) | WELL CONSTRUCTION Inclination: -90 (deg) | | TINO | LITHOLOGY | Layer Depth | MA | TERIAL DESCRIPTION | DISCH. | EC drilling (µS/cm) | 4 K K K K K K K K K K K K K K K K K K K | ELEVATION (m) |
| | | | ASAL T | | | MT ROE BASAI [24 m] (continue | .T: Fresh, black/grey colour d) | | | | |

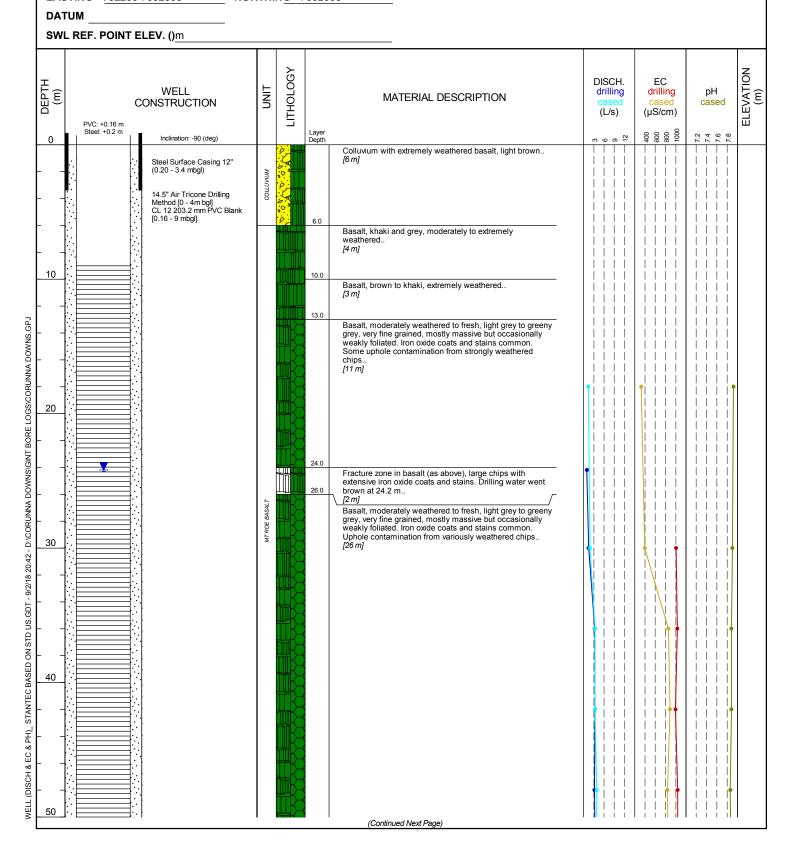
Bottom of borehole at 64.0 m.





PRODUCTION BORE CRD0088

| CLIENT Atlas Iron Limited | PROJECT NAME Corunna Downs Hydrogeological Investigations |
|---|---|
| PROJECT NUMBER 83503916 | LOCATION Corruna Downs |
| DATE STARTED 14/11/17 COMPLETED 17/11/17 | HOLE DIAMETER 368.3/304.8 mm |
| DRILLING CONTRACTOR (DRILLED BY) Foraco (Rig 8) | GROUND WATER LEVELS: |
| DRILLING METHOD Air Hammer | ▼ AT TIME OF DRILLING (Water Cut) 24.20 m bgl |
| LOGGED BY DT, Stantec CHECKED BY FC, Stantec | AFTER DRILLING |
| EASTING 782285 7652335 NORTHING 7652335 | ALIENDIALENO |







PRODUCTION BORE CRD0088

| PRC | DJECT NUMBER 83503916 | | | | | LOCATION Corruna Downs | | | | |
|------|-------------------------------|------------------------|------------|------------------|--------------------------------------|---|---|------------------------------------|--------------------------|-----------|
| | | | | | | HOLE DIAMETER 368.3/304.8 mm | 1 | | | |
| DRII | LLING CONTRACTOR (DRILLE | D BY) <u>Fo</u> | oracc | (Rig | 8) | GROUND WATER LEVELS: | | | | |
| DRII | LLING METHOD Air Hammer | | | | | AT TIME OF DRILLING (Water | er Cut)24.2 | 20 m bgl | | |
| LOC | GGED BY DT, Stantec | CHE | CKE | DBY | FC,Stantec | AFTER DRILLING | | | | |
| EAS | 782285 | NOR | THI | NG 7 | 7652335 | | | | | |
| | TUM L REF. POINT ELEV. ()m | _ | | | | | | | | |
| | (<u>/</u> | | | | | | | | | |
| m) | WELL CONSTRUCTION | ı | LINO | LITHOLOGY | M.A | ATERIAL DESCRIPTION | DISCH. drilling cased (L/s) | EC drilling cased (μS/cm) | pH cased | ELEVATION |
| 50 | Inclination: -90 (de | 3) | | _ | Layer Depth | | 8 9 6 7 | 400 600 800 1000 | 7.2 7.4 7.6 7.8 | |
| | Gravel Pack (3.2-6 | .4mm) [1 - | | | 52.0 | | | | | |
| | 102m bgl] | | | | 53.0 Fracture zone i | n basalt (as above), large chips with oxide coats and stains. Drilling water went | | | | |
| - | CL 12 203.2 mm P ¹ | /C Slotted | | | brown [1 m] | | | | | |
| 4 | | | | | grey, very fine | ately weathered to fresh, light grey to greeny grained, mostly massive but occasionally . Iron oxide coats and stains common. | | | | |
| | | | | | | ination from variously weathered chips | | | | |
| 60 | 12" Air Hammer Dr | illing | | | | | | | | |
| 00_ | Method [4 - 102 mb | gl] | | | | | | | | |
| _ | | | | | | | / | | | |
| | | | | | | | - | | | |
| | | | | | 66.0 | | | | | |
| | | | | | extensive iron of | (?) in basalt (as above), sample brown with oxide coats and stains | | | | |
| _ | | | | | 68.0 [2 m] Basalt, modera | ately weathered to fresh, light grey to greeny grained, mostly massive but occasionally | | | | |
| 70_ | | | | | weakly foliated | I from oxide coats and stains common. Interpretation from variously weathered chips | | | | |
| | | | | | [5.5 m] | , | | | | |
| | | | 7.7 | | 73.5 74.0 Fractured or in | record weathering word in boods (or | | | | |
| | | | ROE BASAL1 | | Tractured of the | reeased weathering zone in basalt (as bund and sample brown with extensive iron d stains | | | | |
| | | | MT RC | | [0.5 m] Basalt, modera | ately weathered to fresh, light grey to greeny | | | | |
| - | | | | | weakly foliated | grained, mostly massive but occasionally I from oxide coats and stains common. | i i i | | | |
| 80_ | | | | | [12 m] | ination from variously weathered chips | | | | |
| • | | | | | | | | | | |
| | | | | | | | | | | |
| - | | | | | | | | | | |
| | | | | | 86.0 | | | | | |
| | | | | | [2 m] | n basalt (as above), large chips | | | | |
| | | | | | Basalt, modera grey, very fine | ately weathered to fresh, light grey to greeny grained, mostly massive but occasionally | | | | |
| 90 | | | | | Uphole contam | . Iron oxide coats and stains common. ination from variously weathered chips | | | | |
| - | | | | | 92.0 [4 m] | n basalt (as above), drilling water brown | | | | |
| | | | | | [1 m] | ately weathered to fresh, light grey to greeny | - <u> </u> | | | |
| | | | | | grey, very fine g weakly foliated | grained, mostly massive but occasionally (96 to 98). Iron oxide coats and stains | | | | |
| - | | | | | common. Upho | ole contamination from variously weathered | | | | |
| - | | | | | | n basalt (as above), large chips (10 to 20 | | | | |
| | r · L | I | | шК) | | ain whether from uphole, but notable Id indicates structure intersected. Drilling | | | | 1 |

(Continued Next Page)



PRODUCTION BORE CRD0088

PAGE 3 OF 3

| CLIENT Atlas Iron Limited | | | | PROJECT NAME Corunna Dow | ns Hydro | ogeologica | l Investigati | ons | |
|---|-----------|-----------|-----------------------------------|--|----------|-----------------------------|------------------------------------|----------|---------------|
| PROJECT NUMBER 83503916 | | | | LOCATION Corruna Downs | | | | | |
| DATE STARTED 14/11/17 | COMPLI | ETED | 17/11/17 | HOLE DIAMETER 368.3/304.8 | mm | | | | |
| DRILLING CONTRACTOR (DRILLED E | SY) Forac | o (Rig | 8) | GROUND WATER LEVELS: | | | | | |
| DRILLING METHOD Air Hammer | | | | X AT TIME OF DRILLING (W | later Cu | t) <u>24.20</u> | m bgl | | |
| LOGGED BY DT, Stantec | CHECK | ED BY | FC,Stantec | AFTER DRILLING | | | | | |
| EASTING 782285 | NORTH | ING 76 | 52335 | | | | | | |
| DATUM | | | | | | | | | |
| SWL REF. POINT ELEV. ()m | | | | | | | | | |
| WELL CONSTRUCTION 100 Inclination: -90 (deg) | TINU | LITHOLOGY | M./ Layer Depth | ATERIAL DESCRIPTION | | DISCH. drilling cased (L/s) | EC drilling cased (µS/cm) | pH cased | ELEVATION (m) |
| CL 12 203.2 mm PVC E [99 - 102 mbgl]. | Blank | | grey, very fine weakly foliate | ately weathered to fresh, light grey to greenly grained, mostly massive but occasionally d (96 to 98). Iron oxide coats and stains ole contamination from variously weathered | r _ | | | | |

Bottom of borehole at 102.0 m.





PRODUCTION BORE CRD0089

| - | Y) For | raco (Rig | g 8) Y _FC | ,Stantec | HOLE DIAMETER _368.3/304.8 mr GROUND WATER LEVELS: | n | | | |
|--|-----------------|---------------|---|---|---|-----------------------------|------------------------------------|-------------------------|---------------|
| WELL CONSTRUCTION PVC: +0.16 m Steel: +0.2 m Inclination: -90 (deg) | 1 | UNIT | Layer Depth | | MATERIAL DESCRIPTION | DISCH. drilling cased (L/s) | EC drilling cased (µS/cm) | bH drilling cased b.7.8 | ELEVATION (m) |
| Cement seal [0 - 0.5 mbg Steet Surface Casing 12' (0.20 - 3.4 mbgl) Natural pack [0.5 - 4 mbg 114.5" Air Tricone Drilling Method [0 - 4m bgl] Bentonite seal [4 - 5 mbg 10.16 - 12.3 mbgl] 10 | ij IJ ank | MI ROE BASALT | 9.0 22.0 24.0 26.0 38.0 42.0 | Weathered [2 m] Weathered [2 m] Weathered [2 m] Weathered [2 m] Weathered [2 m] Gray staining [10 m] Cherty bas: [2 m] Basalt bect [4 m] Qtz dike [4 m] Basalt, fres [2 m] | basalt, color change to darker gray/brown. a. No flow basalt, fractured, Fe staining. No flow basalt, minor fractures, Fe staining | | | | |

(Continued Next Page)



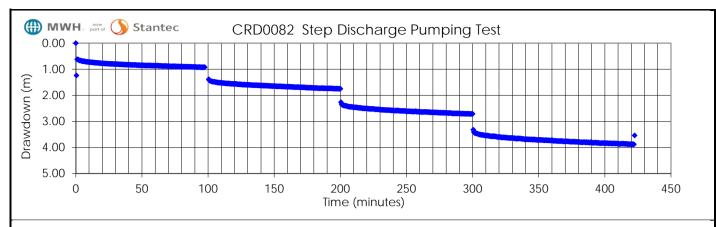


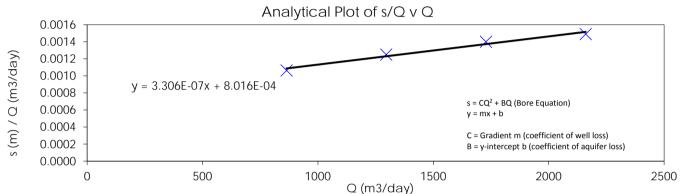
PRODUCTION BORE CRD0089

| PROJECT NUMBER <u>83503916</u> DATE STARTED <u>18/11/17</u> | COMPLE) Forac | ETED co (Rig | PROJECT NAME Corunna Downs LOCATION Corruna Downs 21/11/17 HOLE DIAMETER 368.3/304.8 GROUND WATER LEVELS: FC,Stantec AFTER DRILLING | mm | | |
|---|----------------|-----------------|---|-----------------------------|---------------------------|-------------------------|
| DATUM SWL REF. POINT ELEV. ()m | NORTH | IN <u>G</u> 76 | 52280 | | | |
| WELL CONSTRUCTION 50 Inclination: -90 (deg) | TINU | LITHOLOGY | MATERIAL DESCRIPTION Layer Depth | DISCH. drilling cased (L/s) | EC drilling cased (µS/cm) | pH drilling cased |
| Gravel Pack (3.2-6.4mm) 100m bgl] CL 12 203.2 mm PVC Slo [12.3 - 96.3 mbgl]. 12" Air Hammer Drilling Method [4 - 100 mbgl] CL 12 203.2 mm PVC Bla [96.3 - 99.3 mbgl]. Endcap [99.3 mbgl]. | tted | | Basalt, gray, fresh. Sump leaking [10 m] Basalt, fresh, minor fractures [34 m] | | | |

Bottom of borehole at 100.0 m.

Appendix D Step Rate Test Results





Gradient (C)
Intercept (B)

3.306E-07 8.016E-04

| ANALYSIS TABLE | Bierschenk & Wilson (1961) |
|----------------|----------------------------|

| 7 11 17 12 1 0 10 17 12 | | | | Biologicon | | 0.7 | | |
|----------------------------------|--------------------|-------------------------|-----------------------------------|------------------------------------|---|--|-------------------------|----------------------------------|
| | Ca | alculation of well | efficiency and | comparison | of observed and | predicted drawd | owns | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulativ e Analysed drawdow n (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) % |
| 1 | 10.0 | 864 | 0.92 | 0.92 | 0.94 | 0.92 | 0.0011 | 73.7 |
| 2 | 15.0 | 1296 | 0.70 | 1.62 | 1.59 | 1.75 | 0.0013 | 65.2 |
| 3 | 20.0 | 1728 | 0.80 | 2.42 | 2.37 | 2.71 | 0.0014 | 58.4 |
| 4 | 25.0 | 2160 | 0.80 | 3.22 | 3.27 | 3.54 | 0.0015 | 52.9 |
| ANIAL VOIC COMMAN | TNITO | | | | | | | |
| ANALYSIS COMME | :N15: | | | | | | | |

Analysis Date: 14/07/2017 By Hydro: F Cronjé

 $s_{w(n)} = BQ_n + CQ_n^P$ (Rorabaugh's equation) Where: B = Interce

/here: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)

C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss. They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

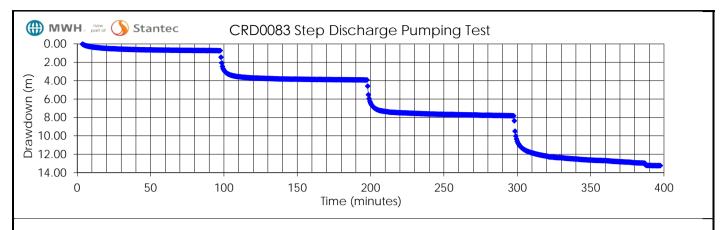
Please note: 1. In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer

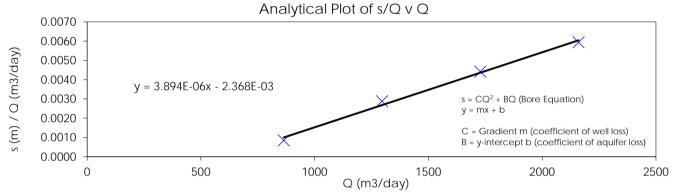
rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss. In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





Analysis Date:

13/07/2017

By Hydro:

3.894E-06 Gradient (C) Intercept (B)

F Cronjé

| ANALYSIS TAB | LE | | | Bierschenk | : & Wilson (19 | 61) | | |
|----------------------------------|--------------------|-------------------------|-----------------------------------|---|---|---|-------------------------|----------------------------------|
| | Ca | lculation of well | efficiency and | comparison | of observed and | predicted draws | lowns | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) % |
| 1 | 10.0 | 864 | 0.73 | 0.73 | 4.95 | 0.73 | 0.0008 | 41.3 |
| 2 | 15.0 | 1296 | 3.00 | 3.73 | 9.61 | 3.92 | 0.0029 | 31.9 |
| 3 | 20.0 | 1728 | 3.90 | 7.63 | 15.72 | 7.82 | 0.0044 | 26.0 |
| 4 | 25.0 | 2160 | 5.20 | 12.83 | 23.28 | 13.24 | 0.0059 | 22.0 |
| | | | | | | | | |
| ANALYSIS COMM | ENTS: First step | was 97.5 mins. | | | | | | |

 $s_{w(n)} = BQ_n + CQ_n^P$ (Rorabaugh's equation) Where: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)

C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss.

They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

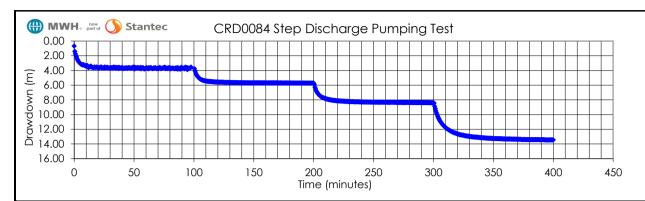
Please note: 1. In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

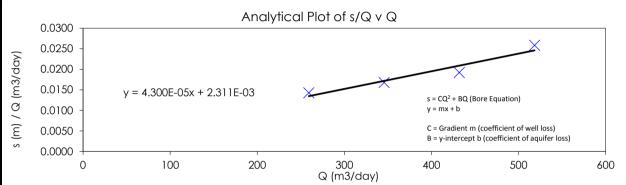
In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





ANALYSIS TABLE Bierschenk & Wilson (1961)

Gradient (C) 4.300E-05 Intercept (B) 2.311E-03

| Discharge (l/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) |
|--------------------|-------------------------|---------------------------------------|---|---|--|---|---|
| 3.0 | 259 | 3.70 | 3.70 | 3.49 | 3.70 | 0.0143 | 17.2 |
| 4.0 | 346 | 2.10 | 5.80 | 5.93 | 5.73 | 0.0168 | 13.5 |
| 5.0 | 432 | 2.50 | 8.30 | 9.02 | 8.40 | 0.0192 | 11.1 |
| 6.0 | 518 | 5.10 | 13.40 | 12.75 | 13.45 | 0.0258 | 9.4 |
| | | | | | | | |
| | 3.0 4.0 5.0 | (l/s) (m³/d) 3.0 259 4.0 346 5.0 432 | (Vs) (m³/d) incremental drawdown (m) 3.0 259 3.70 4.0 346 2.10 5.0 432 2.50 | Analysed Analysed | (Vs) (m³/d) Analysed incremental drawdown (m) Analysed drawdown (m) Analysed drawdown (m) Bore Equation (m) 3.0 259 3.70 3.70 3.49 4.0 346 2.10 5.80 5.93 5.0 432 2.50 8.30 9.02 | Analysed Analysed | Analysed Analysed |

25/07/2017 F Cronjé Analysis Date: By Hydro:

 $s_{w(n)} = BQ_n + CQ_n^P$ (Rorabaugh's equation) Where: B = Interesting

B = Intercept with y axis (coefficient of aquifer loss or laminar flow)

C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss.

They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

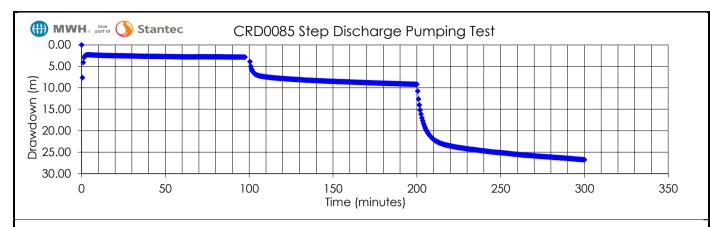
In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer Please note: 1. rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

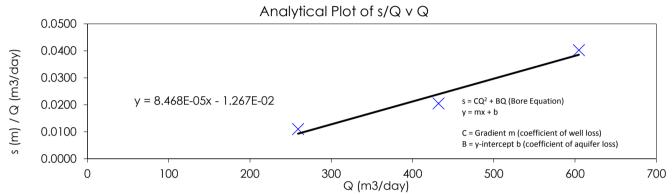
In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





| Gradient (C) | |
|---------------|-----------|
| Intercept (B) | 1.267E-02 |
| | |

F Cronjé

| ANALYSIS TAI | | | | | : & Wilson (196 | | | |
|----------------------------------|--------------------|-------------------------|-----------------------------------|--|---|---|-------------------------|----------------------------------|
| | Ca | alculation of wel | I efficiency and | comparison | of observed and | predicted drawdo | owns | |
| Step (100 minute duration) | Discharge (l/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) % |
| 1 | 3.0 | 259 | 2.85 | 2.85 | 8.97 | 0.92 | 0.0110 | 36.6 |
| 2 | 5.0 | 432 | 6.00 | 8.85 | 21.28 | 1.75 | 0.0205 | 25.7 |
| 3 | 7.0 | 605 | 15.50 | 24.35 | 38.64 | 2.71 | 0.0403 | 19.8 |
| | | | | | | | | |
| ANALYSIS COMMI | ENTS: | | | | | | | |

Analysis Date:

25/07/2017

By Hydro:

 $s_{w(n)} = BQ_n + CQ_n^P$ (Rorabaugh's equation) Where: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)

C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ2 are the drawdown due aquifer loss and drawdown due to apparent well loss.

They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

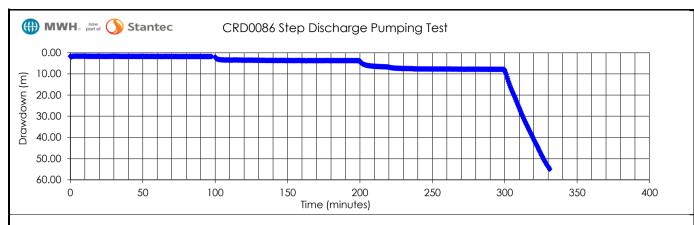
Please note: 1. In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss

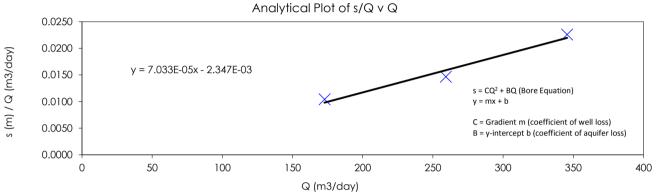
In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





7 033F-05 Gradient (C) 2.347E-03 Intercept (B)

F Cronjé

| ANALYSIS TAI | BLE | | | Bierschenk | : & Wilson (196 | 61) | | | | |
|----------------------------------|--|-------------------------|-----------------------------------|--|---|---|-------------------------|----------------------------------|--|--|
| | С | alculation of we | ll efficiency and | comparison | of observed and p | predicted drawdo | wns | | | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) % | | |
| 1 | 2.0 | 173 | 1.80 | 1.80 | 2.51 | 1.80 | 0.0104 | 16.2 | | |
| 2 | 3.0 | 259 | 2.00 | 3.80 | 5.33 | 3.75 | 0.0147 | 11.4 | | |
| 3 | 4.0 | 346 | 4.00 | 7.80 | 9.21 | 7.85 | 0.0226 | 8.8 | | |
| 4 | 5.0 | 432 | 46.00 | 53.80 | 14.14 | 54.93 | 0.1245 | 7.2 | | |
| ANALYSIS COMME | NALYSIS COMMENTS: Last step was 31 minutes | | | | | | | | | |
| | | | | | | | | | | |

 $s_{w(n)} = BQ_n + CQ_n^P$ (Rorabaugh's equation) Where: B = Interc

equation)
B = Intercept with y axis (coefficient of aquifer loss or laminar flow)
C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss.

They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

Analysis Date:

03/08/2017

By Hydro:

In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

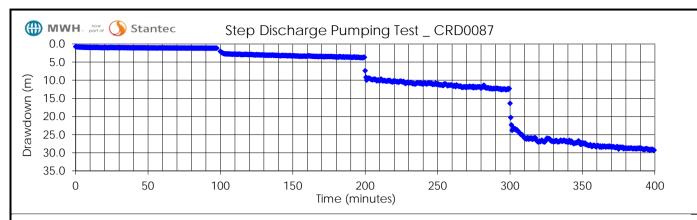
Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

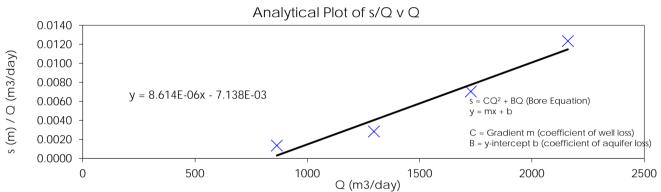
A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.

 $Ew = (BQ/(BQ + CQ^{P}) \times 100$ (%)

2

Please note: 1.





| Gradient (C) | 8.614E-06 |
|---------------|-----------|
| Intercept (B) | 7.138E-03 |

F Cronjé

| ANALYSIS TAB | | | : & Wilson (19 | | | | | | |
|---|--------------------|-------------------------|-----------------------------------|---|---|---|-------------------------|----------------------------------|--|
| Calculation of well efficiency and comparison of observed and predicted drawdowns | | | | | | | | | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) % | |
| 1 | 10.0 | 864 | 1.16 | 1.16 | 12.60 | 1.16 | 0.0013 | 49.0 | |
| 2 | 15.0 | 1296 | 2.50 | 3.66 | 23.72 | 3.66 | 0.0028 | 39.0 | |
| 3 | 20.0 | 1728 | 8.50 | 12.16 | 38.06 | 12.27 | 0.0070 | 32.4 | |
| 4 | 25.0 | 2160 | 14.50 | 26.66 | 55.61 | 29.28 | 0.0123 | 27.7 | |
| | | | | | | | | | |
| ANALYSIS COMMENTS: | | | | | | | | | |

 $s_{\omega(n)}$ = BQ_n + CQ_n^P (Rorabaugh's equation) Where: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)

C = Gradient (coefficient of turbulent flow loss or apparent well loss)

s = Drawdown in the borehole

P = Value determined using Rorabaugh's method of superposition

Components of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss. They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

> Please note: 1. In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer

rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

Analysis Date:

03/08/2017

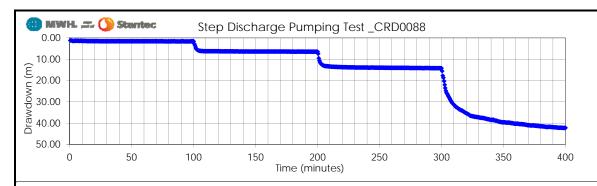
By Hydro:

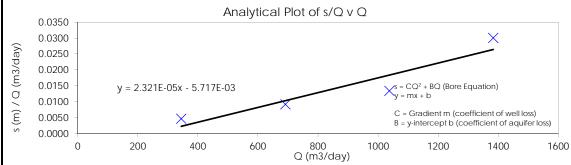
In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





2.321E-05 5.717E-03 Gradient (C)

| ANALYSIS TABLE | | | | | |
|----------------|--|--|--|--|--|
| | | | | | |
| | | | | | |

| | | | | | | | intercept (b) | 3.717E-U |
|--|--------------------|-------------------------|-----------------------------------|---|---|---|-------------------------------|--------------------------|
| ANALYSIS TABLE | | | | Bierschenl | | | | |
| Calculation of well efficiency and comparison of observed and predicted drawdo | | | | | | | lowns | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) |
| 1 | 4.0 | 345 | 1.61 | 1.61 | 4.73 | 1.61 | 0.0047 | 41.7 |
| 2 | 8.0 | 691 | 4.76 | 6.37 | 15.04 | 6.46 | 0.0092 | 26.3 |
| 3 | 12.0 | 1038 | 7.57 | 13.94 | 30.92 | 14.17 | 0.0134 | 19.2 |
| 4 | 16.0 | 1383 | 27.64 | 41.58 | 52.32 | 42.24 | 0.0301 | 15.1 |
| | | | | | | | | |
| | | | | | | | | |
| ANALYSIS COMME | NTS: First step | was 97.5 mins. | | | | | | |

Analysis Date:

13/07/2017

By Hydro:

F Cronjé

- $s_{w(n)} = BQ_n + CQ_n^{\ \ p}$ (Rorabaugh's equation) Where: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)
 - C = Gradient (coefficient of turbulent flow loss or apparent well loss)

 - s = Drawdown in the borehole
 P = Value determined using Rorabaugh's method of superposition

its of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss. They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

Please note: 1.

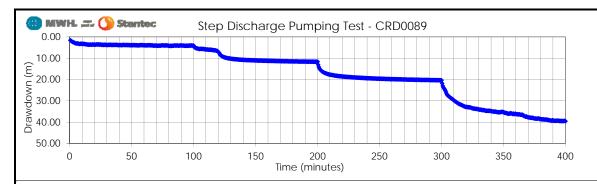
In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

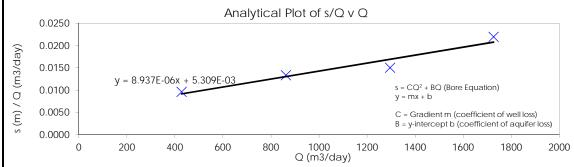
In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often

2 relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.





Gradient (C) 8.937E-06 5.309E-03

| ANALYSIS | TABLE |
|----------|-------|

Bierschenk & Wilson (1961)

| to teroio in tale | | | | | | | | | |
|---|--------------------|-------------------------|-----------------------------------|---|---|---|-------------------------------|--------------------------|--|
| Calculation of well efficiency and comparison of observed and predicted drawdowns | | | | | | | | | |
| Step (100 minute duration) | Discharge (I/s) | Discharge (Q) (m³/d) | Analysed incremental drawdown (m) | Cumulative Analysed drawdown (m) | Predicted drawdown using Bore Equation (m) | Actual total pump-test drawdown (m) | Analysed cumulative s/Q | Apparent Efficiency (Ew) | |
| 1 | 5.0 | 428 | 4.10 | 4.10 | 3.91 | 4.10 | 0.0096 | 58.1 | |
| 2 | 10.0 | 862 | 7.37 | 11.47 | 11.22 | 11.67 | 0.0133 | 40.8 | |
| 3 | 15.0 | 1296 | 7.96 | 19.43 | 21.88 | 20.36 | 0.0150 | 31.4 | |
| 4 | 20.0 | 1727 | 18.40 | 37.83 | 35.81 | 39.60 | 0.0219 | 25.6 | |
| | | | | | | | | | |
| | | | | | | | | | |
| NALYSIS COMMENTS: First step was 97.5 mins. | | | | | | | | | |

Analysis Date: 13/07/2017

By Hydro:

F Cronjé

- $s_{w(n)} = BQ_n + CQ_n^{\ \ p}$ (Rorabaugh's equation) Where: B = Intercept with y axis (coefficient of aquifer loss or laminar flow)
 - C = Gradient (coefficient of turbulent flow loss or apparent well loss)

 - s = Drawdown in the borehole
 P = Value determined using Rorabaugh's method of superposition

its of Jacob's (1947) equation BQ and CQ² are the drawdown due aquifer loss and drawdown due to apparent well loss. They give an indication of the proportion of total drawdown caused by laminar and turbulent flow.

Please note: 1.

In thin or fissured aquifers large components of well loss are due to high flow velocities in the aquifer rather than inefficient bore design. Therefore, the term "apparent well loss" is better than well loss.

2

In aquifers where the flow horizons are vertically anisotropic, changes in bore performance often relate to changes in the rest water level with respect to the primary aquifer horizons.

Ew or Well Efficiency represents the proportion of drawdown caused by laminar flow.

A high percent efficiency indicates a larger proportion of drawdown is due to the aquifer properties rather than the well construction.

Appendix E Constant Rate Pumping Test Results

CRD0082

Test pumping of CRD0082 was undertaken between 27/6/2017 and 4/7/2017. A calibration test indicated the maximum pumping rate the pump could achieve was 28 L/s. Therefore four 100 minute steps at 10, 15, 20 and 25 L/s were selected. The total drawdown observed in the pumping bore after the test was 3.8 m. Analysis of the test results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 8.01 x 10^{-4} and 3.3×10^{-7} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 74% at 10 L/s to 53% at 25 L/s.

The constant rate test was conducted at a rate of 25 L/s, resulting in a maximum drawdown of 6.13 m. The drawdown did not reach steady state conditions with groundwater levels continuing to fall at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded best estimates for transmissivity values of around 200 m²/day (190 to 211) while derived specific yield values are not considered reliable.

Electrical conductivity remained steady throughout the test oscillating diurnally (due to temperature change) between $1035 - 1307 \,\mu\text{S/cm}$.

Following the CRT, the groundwater level took 2800 minutes to achieve 95% recovery.

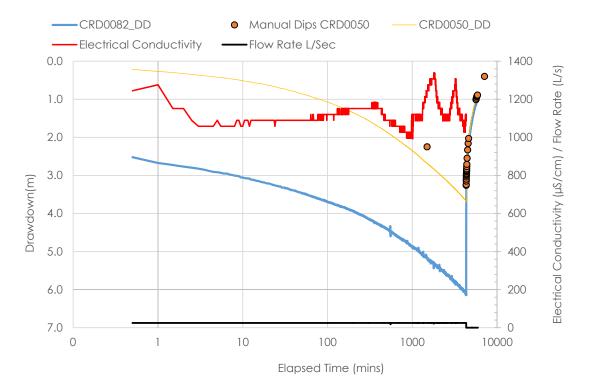


Figure D1: Observations of water level and electrical conductivity during the constant rate test of CRD0082

CRD0083

Test pumping of CRD0083 was undertaken between 5/7/2017 and 9/7/2017. A calibration test indicated the bore was capable of a pumping rate of 20 L/s and four 100 minute steps at 10, 15, 20, 25 L/s were selected for the step rate test. The total drawdown observed in the pumping bore after the test was 13.24 m. The test results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 2.368×10^{-3} and 3.89×10^{-6} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 41% at 10 L/s to 22% at 20 L/s.

The constant rate test was conducted at a rate of 20 L/s. The shape of the drawdown plot suggests an unconfined aquifer response in the pumping bore. The water level throughout the pumping test did not reach steady state conditions, but showed a plateauing around the middle of the test, consistent with a delayed yield response, before the drawdown commenced increasing at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded best estimates for transmissivity values of around 200 m²/day (170 to 220 m²/day). Derived specific yield values ranged from 7 x 10^{-3} to 7×10^{-6} but are not considered reliable..

Electrical conductivity fluctuated with diurnal temperature change and there was a slight reduction in throughout the test from 995 to 710 µS/cm.

Following the CRT water level recovery was monitored for 390 minutes, during which time 89% recovery was observed.

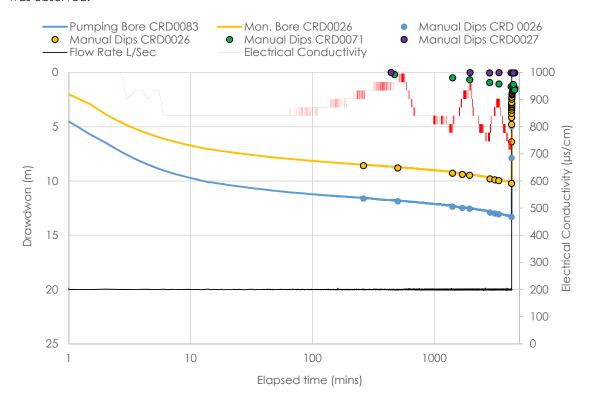


Figure D2: Observations of water level and electrical conductivity during the constant rate test of CRD0083

CRD0084

Test pumping of CRD0084 was undertaken between 10/7/2017 and 16/7/2017. A calibration test indicated a pumping rate of 8 L/s was unsustainable for the bore. Therefore four 100 minute steps at 3, 4, 5, and 6 L/s were selected. The total drawdown observed in the pumping bore after the test was 13.45 m. The test

results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 2.311×10^{-3} and 4.30×10^{-5} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 17.2% at 3 L/s to 9% at 6 L/s.

The constant rate test was conducted at a rate of 6 L/s. The drawdown response was unsteady, showing a plateauing around the middle of the test, consistent with a delayed yield response, before the drawdown commenced increasing at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded best estimates for transmissivity values of around 200 m²/day (155 to 237 m²/day). A good curve fit was achieved using Moench's analysis method, but the derived transmissivity was relatively low at 47 m²/day. The derived specific yield was 5 x 10^{-3} but it is not considered reliable. Electrical conductivity fluctuated with diurnal temperature change but remained steady ranging between 1867 and 1338 μ S/cm. Following the CRT, a water level recovery of 95% was achieved in 20 minutes.

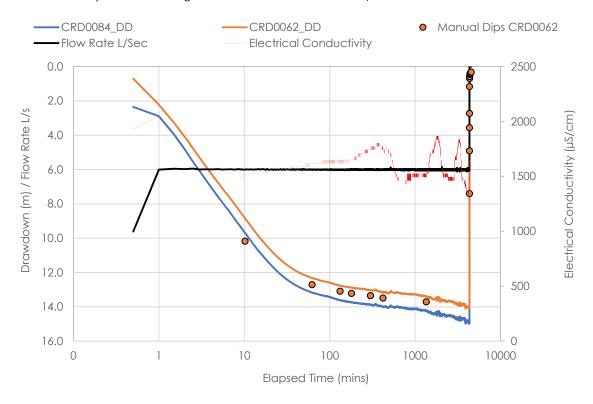


Figure D3: Observations of water level and electrical conductivity during the constant rate test of CRD0084

CRD0085 Test

Test pumping of CRD0085 was undertaken between 16/7/2017 and 21/7/2017. The calibration indicated that a pumping rate of 17 L/s was significantly too high for the bore. Four 100 minute steps at 3, 5, 7, and 9 L/s were selected, however during the final step the drawdown was excessive and the test was abandoned after 306 minutes.

The results of the first three steps yielded coefficients of aquifer loss (B) and apparent well loss (C) of $1.267 \, \text{x}$ 10^{-2} and $8.468 \, \text{x}$ 10^{-5} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 37% at $3 \, \text{L/s}$ to 20% at $7 \, \text{L/s}$.

The constant rate test was conducted at a rate of 5 L/s, for a maximum drawdown of 16.6 m. The drawdown response was unsteady, showing a slight plateauing about ten minutes into the test, consistent with a delayed yield response, before the drawdown commenced increasing at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded best estimates for transmissivity values of around 100 m²/day.

Electrical conductivity fluctuated with diurnal temperature change and there was a slight reduction throughout the test from 1617 to 1281 μ S/cm. Following the CRT, the water level recovered to 95% in 66 mins.

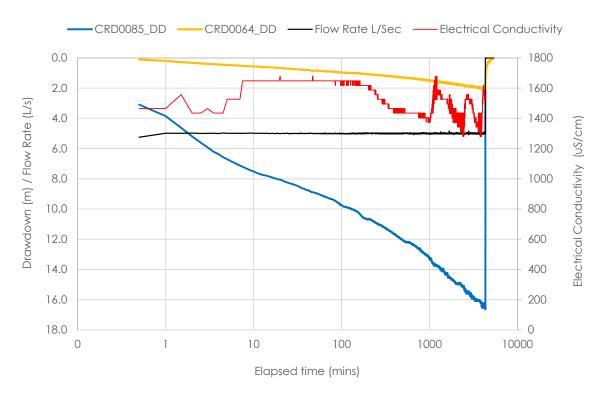


Figure D4: Observations of water level and electrical conductivity during the constant rate test of CRD0085

CRD0086 Test

Test pumping of CRD0086 was undertaken between 23/7/2017 and 27/7/2017. No calibration test was undertaken before the step test. Four 100 minute steps at 2, 3, 4, and 5 L/s were selected, however during the final step the drawdown was excessive and the test was abandoned after 330 minutes.

The results of the first three steps yielded coefficients of aquifer loss (B) and apparent well loss (C) of 2.34×10^{-3} and 7.033×10^{-5} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 16% at 2 L/s to 9% at 4 L/s.

The constant rate test was conducted at a rate of 4 L/s. The drawdown response in the pumping bore was erratic, with s intervals of apparent recovery (up to 0.6 m over 6.5 minutes). Maximum drawdown was 8.27m. Given the pumping rate was measured as constant for the duration of the test, the cause of these recoveries is not known but could be due to development effects such as when saturated fractures suddenly drain as the differential head between the water level in the well and the water in the fracture, increases to a point where hydraulic connection with the well is established (i.e. developing). Alternatively and/or simultaneously, the recoveries could be due to the aquifer material settling in response to reducing heads during the test (storage reducing). Hydraulic analysis yielded unreliable estimates for transmissivity values of around 400 m²/day.

The drawdown response in the monitoring bore indicates poor connectivity with the pumping bore as the drawdown curve was smooth and almost linear, but with a slowly increasing rate of drawdown. The maximum drawdown in the monitoring bore was 0.88 m.

Electrical conductivity fluctuated with diurnal temperature change but remained steady ranging between 3143 and 2899 μ S/cm.

Following the CRT recovery to 95% was achieved within 107mins.

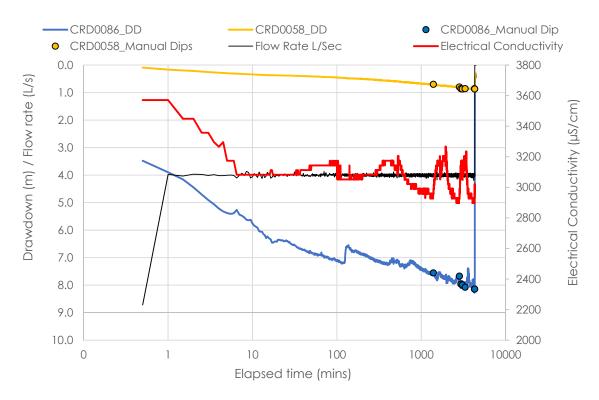


Figure D5: Observations of water level and electrical conductivity during the constant rate test of CRD0086

CRD0087 Test

Test pumping of CRD0087 was undertaken between 28/7/2017 and 1/8/2017. A calibration test indicated that a pumping rate of 27 L/s was unsustainable for the bore. Therefore four 100 minute steps at 10, 15, 20 and 25 L/s were selected. The total drawdown observed in the pumping bore after the test was 29.3 m. The test results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 7.138×10^{-3} and 8.61×10^{-6} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 49% at 10 L/s to 28% at 25 L/s. In the fourth step Airwell reported they were struggling to keep a constant pumping rate (25 L/s)

The constant rate test was conducted at a rate of 15 L/s, for a maximum drawdown of 31.3 m. The drawdown did not reach steady state conditions with groundwater levels continuing to fall at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded poor estimates for transmissivity due to the nature of the drawdown curve while no specific yield values could be determined.

Electrical conductivity fluctuated with diurnal temperature change and there was a slight reduction throughout the test from 1250 to 730 μ S/cm

Following the CRT, recovery was rapid, achieving 94% in 15 mins and 95% in 110 mins. Recovery analysis gave an unreliably high transmissivity value of around $600 \text{ m}^2/\text{day}$,

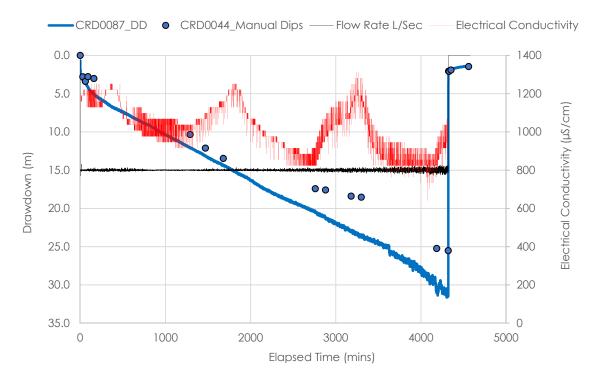


Figure D6: Observations of water level and electrical conductivity during the constant rate test of CRD0087

CRD0088 Test

Test pumping of CRD0088 was undertaken between 19/11/2017 and 23/11/2017. A Step Rate Test was undertaken for four 100 minute steps at 4, 8, 12 and 16 L/s were selected. The total drawdown observed in the pumping bore after the test was 41.58 m. The test results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 5.717×10^{-3} and 2.32×10^{-5} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 42% at 4 L/s to 15.1% at 16 L/s.

The constant rate test was conducted at a rate of 12 L/s, for a maximum drawdown of 16.2 m. The drawdown did not reach steady state conditions with the water level in pumping well linear after about 101 minutes and 12 m drawdown. The curve remains essentially linear until about 2000 minutes, where it begins to increase in gradient, not quite "falling over" during the test but indicating the commencement of a strip aquifer response, but in a fractured rock setting. Hydraulic analysis indicated transmissivities around $300 \, \text{m}^2/\text{day}$ while storage properties could not be determined due to non-classical theory (porous media) water level responses in the monitoring bore.

Recovery of 95% was achieved in 2 minutes, followed by a small rebound then linear recovery back to 99% in 13 hours, indicating high head losses during pumping, and some mining of water as storage was depleted during the constant rate test.

Electrical conductivity fluctuated with diurnal temperature change between 534 and 840 μ S/cm.

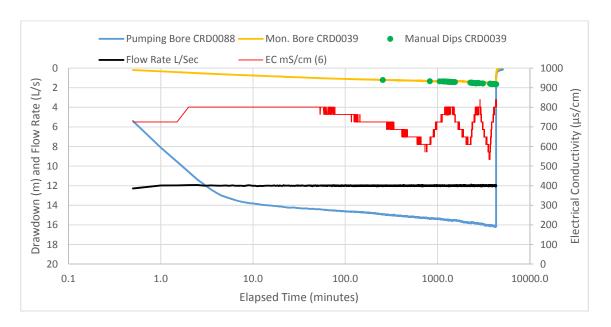


Figure D7: Observations of water level and electrical conductivity during constant rate test of CRD0088

CRD0089 Test

Test pumping of CRD0089 was undertaken between 23/11/2017 and 27/11/2017. A Step Rate Test was undertaken for four 100 minute steps at 5, 10, 15 and 20 L/s were selected. The total drawdown observed in the pumping bore after the test was 37.83 m. The test results yielded coefficients of aquifer loss (B) and apparent well loss (C) of 5.309×10^{-3} and 8.937×10^{-6} respectively. The apparent efficiency of the bore operating at these flow rates ranged from 58% at 5 L/s to 25.61% at 20 L/s.

The constant rate test was conducted at a rate of 12 L/s, for a maximum drawdown of 21.50 m. The drawdown did not reach steady state conditions with groundwater levels plateauing off between 10 and about 1000 minutes, in a delayed yield style of response, before continuing to fall at an increasing rate, similar to a strip aquifer response, but in a fractured rock setting. Hydraulic analysis yielded poor estimates for transmissivity of around 50 m²/day, due to the nature of the drawdown curve while no specific yield values could be determined.

Recovery of 84% was achieved in approximately 6 hours, indicating high head losses during pumping, and some mining of water as storage was depleted during the constant rate test.

Electrical conductivity fluctuated with diurnal temperature change and there was a slight reduction throughout the test from 880 to 610 μ S/cm.

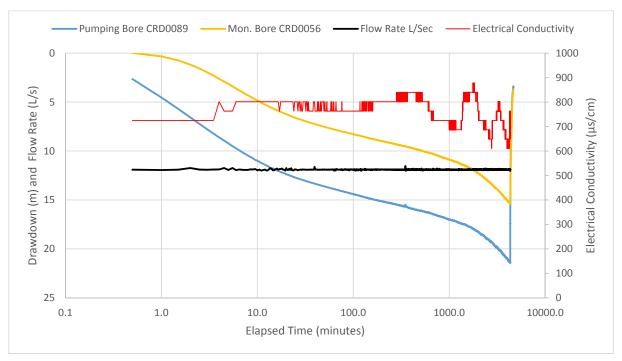


Figure D8: Observations of water level and electrical conductivity during constant rate test of CRD0089

Appendix F Water Chemistry Database and Laboratory Analysis Reports

| / Database |
|-------------|
| r Chemistry |
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| ter and Sur |
| Groundwat |

| Chloride mg/L 1 1 1 1 1 1 1 1 1 | 77 [NT] 57 77 77 76 4 |
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| Carbonate CO32 SC CaCO33 | \$ \$ \$ \$ \$ |
| arbonate HCO3 as CaCO3 an mg/L 5 arbonate HCO3 arbonate HC | 390 380 380 380 400 400 400 0.9 |
| Silica Bic Bic Silica Bic Bic Silica Bic Bic Bic Bic Bic Bic Bic Bic Bic Bic | 32 33 32 32 30 |
| Sodium Dissolved | 120 71 71 72 83 83 83 11,4 |
| Magnesium Dissolved Diss | 28 30 31 29 25 25 25 25 0.6 |
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| Calcium Dissolved Dissol | 93 94 97 97 97 94 94 94 94 94 94 94 94 94 94 94 94 94 |
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| Lead Mal mg/L 0.001 0 Lead Mal 0.001 0 C.0.001 0 | 40.02 40.02 40.001 | 0.0001 0.000001 0.0001 | | |
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| Boron Dissolved Dissolved Dissolved Dissolved O.005 O.005 O.007 O.01 O.007 | | 0.092 0.092 0.32 0.32 0.32 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 | 0.36 0.36 0.23 0.23 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 | |
| c Barlum od Dissolved Diss | +++++++++ | 0.043 0.021 0.008 0.008 0.016 0.016 0.017 0.017 0.007 0.007 0.007 | 0.002 0.084 0.084 0.002 0.002 0.002 0.003 0.003 0.004 | |
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| Antimony Dissolved Dissolv | | 6.000 | (0.007) (0.007 | |
| Aluminium Dissolved | 40.02 40.01 40.02 40.02 40.01 | 6.001 6. | 40.01 40.01 40.01 40.01 40.01 60 | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0 |
| Hardness as CaCO3 and Lardness 13 Hardness 130 150 170 260 260 27 40 450 331 130 130 150 170 170 170 170 170 170 170 170 170 17 | 180 430 20 260 210 300 | 360 280 280 280 300 340 340 430 430 430 330 330 330 230 | 560 310 270 350 350 300 300 190 260 260 260 260 260 260 260 260 260 26 | 350 270 280 280 210 210 210 210 340 440 440 440 480 320 320 320 320 320 320 320 32 |
| Sum of Cations med/L 0 Sum of Cations 3.75 4.09 2.66 15.5 45.8 7.47 7.47 12.2 12.3 0.297 1.47 1.47 1.25 2.34 3.53 | 5.1 13.9 0.774 7.83 6.44 8.8 | 12.8 10.2 8.82 8.82 7.94 10 10 17 17 17 9.84 9.75 9.84 9.75 9.84 | 17.3 9.39 8.18 15.3 15.3 16.3 9.64 30.6 1.22 1.2 1.2 1.2 1.2 1.2 1.2 1. | 11 8.18 11 6.44 6.44 11.6 14.5 16.3 16.3 16.3 17.7 15.7 15.7 15.7 16.3 31.3 31.3 31.2 31.2 31.2 31.2 31.2 31.2 31.2 31.3 31.2 31.3 31.3 11.6 |
| Sum of Anions med/L 0 0 0 0 Sum of Anions 3.3 3.3 3.3 3.4 4.8 7.47 11.7 [INT] 0.332 1.24 1.24 1.24 1.24 1.20 3.03 | 4.97 13.2 0.595 6 6 | 12 9 8 6 6 8.22 15.6 15.6 15.6 15.6 8.33 8.48 8.48 8.48 8.48 | 15 8 8 13.9 13.9 13.9 9.09 9.09 27 27 11 11 7 7 | 10.4 10.4 10.4 8 6 6 1.2 1.2.9 1.2.9 1.4.6 1.3.7 1.3.6 2.8.2 2.8.2 2.8.2 2.8.2 2.8.2 8 8 10.1 |
| Nonic Balance % | -2.3 -4.2 -4.2 1.9 -6.9 -6.9 -4.3 1.6 | -2 -1.3 -1.1 1.2 2.6 -0.75 -0.75 -0.36 -0. | 1.1 1.2 -5.9 -0.47 -0.47 -4.4 -4.4 -1.5 -1.1 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.7 -1.5 | -3.9 -3.9 -5.9 -6.9 -6.9 -6.9 -6.9 -6.1 -6.2 -6.2 -6.2 -6.2 -6.2 -6.3 |
| Sulphate as SO4 mg/L 1 1 Sulphate 17 17 12 21 21 49 49 29 21 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 70 73 73 75 75 75 75 75 75 75 75 75 75 75 75 75 | 28 88 2 3 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | 77 77 74 74 74 74 74 74 74 74 74 74 74 7 | 36 36 44 44 49 49 49 49 49 49 49 49 |
| Sample ID CO-WS-Of CO-WS-Of CO-WS-Of CO-WS-Of CO-WS-10 CO-WS-10 CO-WS-11 CO-WS-11 CO-WS-11 CO-WS-14 | CRD0003 (CDRC0014) CRD0004 (CDWB0001 Camp Bore) CRD0005 CRD00016 CRD0024 CRD0028 CRD0028 CRD0028 CRD0028 CRD0028 CRD0028 | CRD0033 CRD0034 CRD0035 CRD0036 CRD0038 CRD0039 CRD0040 CRD0040 CRD0043 CRD0043 CRD0043 CRD0043 CRD0043 CRD0043 CRD0044 CRD0044 | CRD0048 CRD0046 CRD0050 CRD0051 CRD0051 CRD0056 CRD0056 CRD0068 CRD0068 CRD0068 CRD0060 CRD0060 CRD0060 CRD0060 CRD0060 CRD0071 CRD0071 CRD0071 CRD0071 | CRD0081 CRD0082 CRD0082 CRD0083 CRD0083 CRD0083 CRD0084 CRD0084 CRD0085 CRD0085 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0086 CRD0087 CRD0086 CRD0087 CRD0087 CRD0088 CRD0089 CRD0089 CRD0089 CRD0089 CRD0089 CRD0089 |



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> email: lab@mpl.com.au envirolab.com.au

Envirolab Services (WA) Pty Ltd trading as MPL Laboratories | ABN 53 140 099 207

CERTIFICATE OF ANALYSIS 194600

Client:

Atlas Iron Limited Level 18, 300 Murray Street PERTH WA 6000

Attention: David Nyquest

Sample log in details:

Your Reference: Corunna Downs

No. of samples: 3 Water

Date/Time samples received: 13/04/2017 / 15:20

Date completed instructions received: 13/04/2017

Location:

Analysis Details:

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last pages of this report for any comments relating to the results.

Report Details:

Date results requested by: 21/04/17
Date of Preliminary Report: Not issued Issue Date: 21/04/17

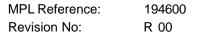
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Tests not covered by NATA are denoted with *.

Results Approved By:

Joshua Lim Operations Manager





| Miscellaneous Inorganics | | | | |
|-------------------------------|----------|------------|------------|------------|
| Our Reference: | UNITS | 194600-1 | 194600-2 | 194600-3 |
| Your Reference | | CRD0038 | CRD0044 | CRD0058 |
| Date Sampled | | 10/04/2017 | 11/04/2017 | 12/04/2017 |
| Type of sample | | Water | Water | Water |
| Time Sampled | | 09:00 | 14:50 | 10:30 |
| Date prepared | - | 18/04/2017 | 18/04/2017 | 18/04/2017 |
| Date analysed | - | 18/04/2017 | 18/04/2017 | 18/04/2017 |
| рН | pH Units | 8.0 | 8.4 | 8.3 |
| Electrical Conductivity (EC) | μS/cm | 700 | 2,700 | 3,000 |
| Total Dissolved Solids (grav) | mg/L | 420 | 1,500 | 1,600 |
| Total Suspended Solids | mg/L | 2,400 | 780 | 950 |
| Fluoride | mg/L | 0.1 | 1.4 | 1.8 |
| Nitrate as N | mg/L | 1.2 | 1.2 | 1.5 |
| Nitrite as N | mg/L | <0.005 | <0.005 | <0.005 |
| NOx as N | mg/L | 1.2 | 1.2 | 1.5 |

| Ionic Balance Our Reference: Your Reference Date Sampled Type of sample Time Sampled | UNITS | 194600-1 CRD0038 10/04/2017 Water 09:00 | 194600-2 CRD0044 11/04/2017 Water 14:50 | 194600-3 CRD0058 12/04/2017 Water 10:30 |
|--|-------|---|---|---|
| Date prepared | - | 18/04/2017 | 18/04/2017 | 18/04/2017 |
| Date analysed | - | 18/04/2017 | 18/04/2017 | 18/04/2017 |
| Calcium - Dissolved | mg/L | 34 | 18 | 23 |
| Potassium - Dissolved | mg/L | 1.5 | 1 | 1.9 |
| Magnesium - Dissolved | mg/L | 52 | 23 | 32 |
| Sodium - Dissolved | mg/L | 43 | 570 | 610 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 350 | 650 | 690 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | 22 | 7 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | <5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 350 | 670 | 700 |
| Chloride | mg/L | 19 | 400 | 460 |
| Sulphate | mg/L | 7 | 99 | 130 |
| Ionic Balance | % | 1.2 | 1.4 | 1.5 |
| Sum of Anions | meq/L | 6.00 | 25.0 | 27.0 |
| Sum of Cations | meq/L | 7.94 | 27.4 | 30.6 |
| Hardness as CaCO ₃ | mg/L | 300 | 140 | 190 |

| Dissolved Metals in Water | | | | |
|---------------------------|-------|------------|------------|------------|
| Our Reference: | UNITS | 194600-1 | 194600-2 | 194600-3 |
| Your Reference | | CRD0038 | CRD0044 | CRD0058 |
| Date Sampled | | 10/04/2017 | 11/04/2017 | 12/04/2017 |
| Type of sample | | Water | Water | Water |
| Time Sampled | | 09:00 | 14:50 | 10:30 |
| Date prepared | - | 21/04/2017 | 21/04/2017 | 21/04/2017 |
| Date analysed | - | 21/04/2017 | 21/04/2017 | 21/04/2017 |
| Silica* | mg/L | 53 | 50 | 50 |
| Aluminium-Dissolved | mg/L | 0.02 | <0.01 | 0.02 |
| Antimony-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.013 | 0.008 | 0.012 |
| Barium-Dissolved | mg/L | 0.008 | 0.021 | 0.031 |
| Boron-Dissolved | mg/L | 0.1 | 0.80 | 0.91 |
| Cadmium-Dissolved | mg/L | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.02 | 0.01 | <0.01 |
| Lead-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.078 | 0.067 | 0.018 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.006 | 0.013 | 0.026 |
| Nickel-Dissolved | mg/L | 0.002 | 0.001 | <0.001 |
| Selenium-Dissolved | mg/L | <0.001 | 0.003 | 0.003 |
| Strontium-Dissolved | mg/L | 0.15 | 0.25 | 0.30 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |

| MethodID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110 -B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| INORG-055 | Nitrate - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | Nitrite - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-022 | Determination of various metals by ICP-MS. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |

| Client Reference: Corunna Downs | | | | | | | | |
|---|----------|-------|----------------|----------------|---------------|---------------------------|-----------|---------------------|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Miscellaneous Inorganics | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 18/04/ 2017 | 194600-1 | 18/04/2017 18/04/2017 | LCS-1 | 18/04/2017 |
| Date analysed | - | | | 18/04/ 2017 | 194600-1 | 18/04/2017 18/04/2017 | LCS-1 | 18/04/2017 |
| рН | pH Units | | INORG-001 | [NT] | 194600-1 | 8.0 8.0 RPD: 0 | LCS-1 | 102% |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 194600-1 | 700 700 RPD:0 | LCS-1 | 106% |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 194600-1 | 420 420 RPD:0 | LCS-1 | 88% |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 194600-1 | 2400 [N/T] | LCS-1 | 97% |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 194600-1 | 0.1 0.1 RPD: 0 | LCS-1 | 98% |
| Nitrate as N | mg/L | 0.005 | INORG-055 | <0.005 | 194600-1 | 1.2 1.2 RPD:0 | LCS-1 | 99% |
| Nitrite as N | mg/L | 0.005 | INORG-055 | <0.005 | 194600-1 | <0.005 <0.005 | LCS-1 | 100% |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 194600-1 | 1.2 1.2 RPD:0 | LCS-1 | 99% |
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Ionic Balance | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 18/04/ 2017 | 194600-1 | 18/04/2017 18/04/2017 | LCS-1 | 18/04/2017 |
| Date analysed | - | | | 18/04/ 2017 | 194600-1 | 18/04/2017 18/04/2017 | LCS-1 | 18/04/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 194600-1 | 34 [N/T] | LCS-1 | 101% |
| Potassium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 194600-1 | 1.5 [N/T] | LCS-1 | 103% |
| Magnesium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 194600-1 | 52 [N/T] | LCS-1 | 101% |
| Sodium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 194600-1 | 43 [N/T] | LCS-1 | 102% |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 194600-1 | 350 [N/T] | LCS-1 | 101% |
| Carbonate CO3 ² - as CaCO 3 | mg/L | 5 | INORG-006 | <5 | 194600-1 | <5 [N/T] | LCS-1 | 101% |
| Total Alkalinity as CaCO3 | mg/L | 5 | INORG-006 | <5 | 194600-1 | 350 [N/T] | LCS-1 | 101% |
| Chloride | mg/L | 1 | INORG-081 | <1 | 194600-1 | 19 19 RPD:0 | LCS-1 | 92% |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 194600-1 | 7 7 RPD:0 | LCS-1 | 94% |
| Hardness as CaCO3 | mg/L | 3 | METALS- 008 | <3 | 194600-1 | 300 [N/T] | [NR] | [NR] |

| Client Reference: Corunna Downs | | | | | | | | | |
|---------------------------------|-------|-------------|----------------|----------------|---------------|---------------------------|-----------|---------------------|--|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery | |
| Dissolved Metals in Water | | | | | | Base II Duplicate II %RPD | | Recovery | |
| Date prepared | - | | | 21/04/ 2017 | [NT] | [NT] | LCS-1 | 21/04/2017 | |
| Date analysed | - | | | 21/04/ 2017 | [NT] | [NT] | LCS-1 | 21/04/2017 | |
| Silica* | mg/L | 0.2 | METALS- 020 | <0.2 | [NT] | [NT] | LCS-1 | 103% | |
| Aluminium-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | [NT] | [NT] | LCS-1 | 99% | |
| Antimony-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 99% | |
| Arsenic-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 100% | |
| Barium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 100% | |
| Boron-Dissolved | mg/L | 0.02 | METALS- 022 | <0.02 | [NT] | [NT] | LCS-1 | 89% | |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS- 022 | <0.000 | [NT] | [NT] | LCS-1 | 101% | |
| Chromium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 103% | |
| Cobalt-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 103% | |
| Copper-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 99% | |
| Iron-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | [NT] | [NT] | LCS-1 | 104% | |
| Lead-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 100% | |
| Manganese- Dissolved | mg/L | 0.005 | METALS- 022 | <0.005 | [NT] | [NT] | LCS-1 | 98% | |
| Mercury-Dissolved | mg/L | 0.0000 5 | METALS- 021 | <0.000 05 | [NT] | [NT] | LCS-1 | 99% | |
| Molybdenum- Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 100% | |
| Nickel-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 98% | |
| Selenium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [ПП] | LCS-1 | 101% | |
| Strontium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [ПЛ] | LCS-1 | 105% | |
| Tin-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 99% | |
| Zinc-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | [NT] | [NT] | LCS-1 | 101% | |

Report Comments:

Definitions:

NT: Not tested NA: Test not required INS: Insufficient sample for this test PQL: Practical Quantitation Limit

<: Less than >: Greater than RPD: Relative Percent Difference LCS: Laboratory Control Sample

NS: Not Specified NEPM: National Environmental Protection Measure NR: Not Reported

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011

Quality Control Definitions

Blank: This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.

Duplicate: This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.

Matrix Spike: A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory Control Sample): This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike: Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.



ENVIROLAB SERVICES

GROUP

CONTROLAB

CONTRO

email: lab@mpl.com.au envirolab.com.au Envirolab Services (WA) Pty Ltd trading as

MPL Laboratories | ABN 53 140 099 207

CERTIFICATE OF ANALYSIS 195634

Client:

Atlas Iron Limited Level 18, 300 Murray Street PERTH WA 6000

Attention: D Nyquest

Sample log in details:

Your Reference: Water Analysis - Corunna Downs

No. of samples: 7 Water

Date/Time samples received: 10/05/2017 / 11:10

Date completed instructions received: 11/05/2017

Location:

Analysis Details:

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last pages of this report for any comments relating to the results.

Report Details:

Date results requested by: 17/05/17

Date of Preliminary Report: Not issued Issue Date: 17/05/17

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Accredited for compliance with ISO/IEC 17025 - Testing

Tests not covered by NATA are denoted with *.

Results Approved By:

Joshua Lim Operations Manager



| Miscellaneous Inorganics | | | | | | |
|-------------------------------|----------|------------|------------|------------|------------|------------|
| Our Reference: | UNITS | 195634-1 | 195634-2 | 195634-3 | 195634-4 | 195634-5 |
| Your Reference | | CRD0045 | CRD0050 | CRD0026 | CRD0062 | CRD0064 |
| Inviron ID | | 1830977 | 1830978 | 1830979 | 1830980 | 1830981 |
| Date Sampled | | 13/04/2017 | 16/04/2017 | 24/04/2017 | 26/04/2017 | 30/04/2017 |
| Type of sample | | Water | Water | Water | Water | Water |
| Time Sampled | | 10:00 | 14:00 | 11:00 | 15:40 | 11:40 |
| Date prepared | - | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 |
| Date analysed | - | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 |
| рН | pH Units | 8.1 | 8.0 | 7.7 | 7.9 | 8.0 |
| Electrical Conductivity (EC) | μS/cm | 970 | 850 | 690 | 1,300 | 1,400 |
| Total Dissolved Solids (grav) | mg/L | 580 | 510 | 410 | 660 | 720 |
| Total Suspended Solids | mg/L | 1,300 | <5 | <5 | <5 | 21 |
| Fluoride | mg/L | 0.7 | 0.2 | 0.4 | 0.3 | 0.7 |
| Nitrate as N | mg/L | 1.5 | <0.005 | 1.1 | 1.4 | 0.81 |
| Nitrite as N | mg/L | 0.017 | <0.005 | <0.005 | 0.008 | 0.008 |
| NOx as N | mg/L | 1.5 | <0.005 | 1.1 | 1.4 | 0.82 |

| Miscellaneous Inorganics | | | |
|-------------------------------|----------|------------|------------|
| Our Reference: | UNITS | 195634-6 | 195634-7 |
| Your Reference | | CRD0058 | CRD0045 |
| Inviron ID | | 1830982 | 1830983 |
| Date Sampled | | 04/05/2017 | 07/05/2017 |
| Type of sample | | Water | Water |
| Time Sampled | | 15:00 | 11:30 |
| Date prepared | - | 12/05/2017 | 12/05/2017 |
| Date analysed | - | 12/05/2017 | 12/05/2017 |
| рН | pH Units | 8.1 | 8.0 |
| Electrical Conductivity (EC) | μS/cm | 2,900 | 900 |
| Total Dissolved Solids (grav) | mg/L | 1,700 | 540 |
| Total Suspended Solids | mg/L | 200 | <5 |
| Fluoride | mg/L | 2.0 | 0.7 |
| Nitrate as N | mg/L | <0.005 | 1.2 |
| Nitrite as N | mg/L | <0.005 | <0.005 |
| NOx as N | mg/L | <0.005 | 1.2 |

| Ionic Balance | | | | | | |
|--|-------|------------|------------|------------|------------|------------|
| Our Reference: | UNITS | 195634-1 | 195634-2 | 195634-3 | 195634-4 | 195634-5 |
| Your Reference | | CRD0045 | CRD0050 | CRD0026 | CRD0062 | CRD0064 |
| Inviron ID | | 1830977 | 1830978 | 1830979 | 1830980 | 1830981 |
| Date Sampled | | 13/04/2017 | 16/04/2017 | 24/04/2017 | 26/04/2017 | 30/04/2017 |
| Type of sample | | Water | Water | Water | Water | Water |
| Time Sampled | | 10:00 | 14:00 | 11:00 | 15:40 | 11:40 |
| Date prepared | - | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 |
| Date analysed | - | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 | 12/05/2017 |
| Calcium - Dissolved | mg/L | 41 | 56 | 56 | 63 | 58 |
| Potassium - Dissolved | mg/L | <0.5 | 1.8 | <0.5 | 1 | 2.5 |
| Magnesium - Dissolved | mg/L | 28 | 31 | 17 | 44 | 43 |
| Sodium - Dissolved | mg/L | 120 | 63 | 52 | 110 | 160 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 390 | 310 | 300 | 310 | 390 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | <5 | <5 | <5 | <5 |
| Hydroxide OH ⁻ as CaCO ₃ | mg/L | <5 | <5 | <5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 390 | 310 | 300 | 310 | 390 |
| Chloride | mg/L | 77 | 72 | 37 | 180 | 200 |
| Sulphate | mg/L | 25 | 44 | 19 | 91 | 56 |
| Ionic Balance | % | -5.9 | -5.9 | -6.9 | -6.2 | -3.4 |
| Hardness as CaCO ₃ | mg/L | 220 | 270 | 210 | 340 | 320 |
| Sum of Anions | meq/L | 9.00 | 8.00 | 6.00 | 12.0 | 13.0 |
| Sum of Cations | meq/L | 9.42 | 8.18 | 6.44 | 11.6 | 13.6 |

| Ionic Balance | | | |
|--|---------|------------|------------|
| Our Reference: | UNITS | 195634-6 | 195634-7 |
| Your Reference | | CRD0058 | CRD0045 |
| Inviron ID | | 1830982 | 1830983 |
| Date Sampled | | 04/05/2017 | 07/05/2017 |
| Type of sample | | Water | Water |
| Time Sampled | | 15:00 | 11:30 |
| Date prepared | - | 12/05/2017 | 12/05/2017 |
| Date analysed | - | 12/05/2017 | 12/05/2017 |
| Calcium - Dissolved | mg/L | 21 | 49 |
| Potassium - Dissolved | mg/L | 1.5 | <0.5 |
| Magnesium - Dissolved | mg/L 27 | | 26 |
| Sodium - Dissolved | mg/L | 480 | 100 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 700 | 390 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | <5 |
| Hydroxide OH ⁻ as CaCO ₃ | mg/L | <5 | <5 |
| Total Alkalinity as CaCO3 | mg/L | 700 | 390 |
| Chloride | mg/L | 480 | 60 |
| Sulphate | mg/L | 140 | 20 |
| Ionic Balance | % | -11 | -4.0 |
| Hardness as CaCO₃ | mg/L | 160 | 230 |
| Sum of Anions | meq/L | 28.0 | 8.00 |
| Sum of Cations | meq/L | 24.2 | 9.09 |

| Dissolved Metals in Water | | | | | | |
|---|-------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|
| Our Reference: Your Reference InvironID | UNITS | 195634-1 CRD0045 1830977 | 195634-2 CRD0050 1830978 | 195634-3 CRD0026 1830979 | 195634-4 CRD0062 1830980 | 195634-5 CRD0064 1830981 |
| Date Sampled Type of sample Time Sampled | | 13/04/2017 Water 10:00 | 16/04/2017 Water 14:00 | 24/04/2017 Water 11:00 | 26/04/2017 Water 15:40 | 30/04/2017 Water 11:40 |
| Date prepared | - | 16/05/2017 | 16/05/2017 | 16/05/2017 | 16/05/2017 | 16/05/2017 |
| Date analysed | - | 16/05/2017 | 16/05/2017 | 16/05/2017 | 16/05/2017 | 16/05/2017 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
| Arsenic-Dissolved | mg/L | 0.002 | 0.004 | <0.001 | <0.001 | 0.002 |
| Barium-Dissolved | mg/L | 0.003 | 0.084 | 0.007 | 0.046 | 0.013 |
| Boron-Dissolved | mg/L | 0.28 | 0.23 | 0.1 | 0.24 | 0.33 |
| Cadmium-Dissolved | mg/L | <0.0001 | <0.0001 | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | <0.001 | 0.001 | <0.001 | 0.001 | <0.001 |
| Iron-Dissolved | mg/L | <0.01 | <0.01 | <0.01 | <0.01 | 0.02 |
| Lead-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | <0.005 | 0.076 | <0.005 | 0.016 | 0.007 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.003 | <0.001 | <0.001 | 0.002 | 0.006 |
| Nickel-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Selenium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | 0.001 | <0.001 |
| Antimony-Dissolved | mg/L | <0.001 | 0.003 | <0.001 | <0.001 | <0.001 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.36 | 0.30 | 0.40 | 0.57 | 0.46 |
| Zinc-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |

| Dissolved Metals in Water | | | |
|-----------------------------|-------|----------------|----------------|
| Our Reference: | UNITS | 195634-6 | 195634-7 |
| Your Reference | | CRD0058 | CRD0045 |
| Inviron ID | | 1830982 | 1830983 |
| Date Sampled | | 04/05/2017 | 07/05/2017 |
| Type of sample Time Sampled | | Water 15:00 | Water 11:30 |
| Time Sampled | | | 11.30 |
| Date prepared | - | 16/05/2017 | 16/05/2017 |
| Date analysed | - | 16/05/2017 | 16/05/2017 |
| Aluminium-Dissolved | mg/L | 0.01 | 0.02 |
| Arsenic-Dissolved | mg/L | 0.012 | 0.002 |
| Barium-Dissolved | mg/L | 0.038 | 0.009 |
| Boron-Dissolved | mg/L | 0.97 | 0.27 |
| Cadmium-Dissolved | mg/L | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | <0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.02 | 0.04 |
| Lead-Dissolved | mg/L | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.013 | <0.005 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.027 | 0.002 |
| Nickel-Dissolved | mg/L | <0.001 | <0.001 |
| Selenium-Dissolved | mg/L | 0.003 | <0.001 |
| Antimony-Dissolved | mg/L | <0.001 | <0.001 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.31 | 0.46 |
| Zinc-Dissolved | mg/L | 0.003 | 0.008 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110 -B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| INORG-055 | Nitrate - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | Nitrite - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-022 | Determination of various metals by ICP-MS. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |

| | | C | lient Refere | nce: | Water Analysis - Corunna Downs | | | | |
|--|----------|-------|----------------|----------------|--------------------------------|----------------------------|-----------|---------------------|--|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery | |
| Miscellaneous Inorganics | | | | | | Base II Duplicate II %RPD | | | |
| Date prepared | - | | | 12/05/ 2017 | 195634-1 | 12/05/2017 12/05/2017 | LCS-1 | 12/05/2017 | |
| Date analysed | - | | | 12/05/ 2017 | 195634-1 | 12/05/2017 12/05/2017 | LCS-1 | 12/05/2017 | |
| рН | pH Units | | INORG-001 | [NT] | 195634-1 | 8.1 8.1 RPD: 0 | [NR] | [NR] | |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 195634-1 | 970 970 RPD:0 | [NR] | [NR] | |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 195634-1 | 580 580 RPD:0 | LCS-1 | 87% | |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 195634-1 | 1300 [N/T] | LCS-1 | 110% | |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 195634-1 | 0.7 0.7 RPD:0 | LCS-1 | 101% | |
| Nitrate as N | mg/L | 0.005 | INORG-055 | <0.005 | 195634-1 | 1.5 [N/T] | LCS-1 | 102% | |
| Nitrite as N | mg/L | 0.005 | INORG-055 | <0.005 | 195634-1 | 0.017 [N/T] | LCS-1 | 104% | |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 195634-1 | 1.5 [N/T] | LCS-1 | 103% | |
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery | |
| Ionic Balance | | | | | | Base II Duplicate II % RPD | | | |
| Date prepared | - | | | 12/05/ 2017 | 195634-1 | 12/05/2017 12/05/2017 | LCS-1 | 12/05/2017 | |
| Date analysed | - | | | 12/05/ 2017 | 195634-1 | 12/05/2017 12/05/2017 | LCS-1 | 12/05/2017 | |
| Calcium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 195634-1 | 41 [N/T] | LCS-1 | 90% | |
| Potassium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 195634-1 | <0.5 [N/T] | LCS-1 | 94% | |
| Magnesium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 195634-1 | 28 [N/T] | LCS-1 | 90% | |
| Sodium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 195634-1 | 120 [N/T] | LCS-1 | 95% | |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 195634-1 | 390 400 RPD:3 | [NR] | [NR] | |
| Carbonate CO3 ² - as CaCO 3 | mg/L | 5 | INORG-006 | <5 | 195634-1 | <5 <5 | [NR] | [NR] | |
| Total Alkalinity as CaCO3 | mg/L | 5 | INORG-006 | <5 | 195634-1 | 390 400 RPD:3 | [NR] | [NR] | |
| Chloride | mg/L | 1 | INORG-081 | <1 | 195634-1 | 77 77 RPD:0 | LCS-1 | 98% | |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 195634-1 | 25 25 RPD:0 | LCS-1 | 106% | |
| Hardness as CaCO3 | mg/L | 3 | METALS- 008 | <3 | 195634-1 | 220 [N/T] | [NR] | [NR] | |

Client Reference: Water Analysis - Corunna Downs QUALITYCONTROL UNITS PQL METHOD Duplicate Sm# Blank **Duplicate results** Spike Sm# Spike % Recovery Dissolved Metals in Base II Duplicate II % RPD Water Date prepared 16/05/ 195634-1 16/05/2017 | 16/05/2017 LCS-1 16/05/2017 2017 Date analysed 16/05/ 195634-1 16/05/2017 || 16/05/2017 LCS-1 16/05/2017 2017 METALS-Aluminium-Dissolved 0.01 195634-1 0.01 || 0.01 || RPD: 0 LCS-1 92% mg/L < 0.01 022 Arsenic-Dissolved mg/L 0.001 METALS-< 0.001 195634-1 0.002 | 0.002 | RPD: 0 LCS-1 98% 022 Barium-Dissolved 0.001 METALS-195634-1 0.003 | 0.003 | RPD: 0 LCS-1 102% mg/L < 0.001 022 Boron-Dissolved METALS-195634-1 0.28 | 0.28 | RPD: 0 LCS-1 97% mg/L 0.02 < 0.02 022 Cadmium-Dissolved 0.0001 METALS-< 0.000 195634-1 <0.0001 || <0.0001 LCS-1 mg/L 101% 022 1 Chromium-Dissolved METALS-0.001 < 0.001 195634-1 <0.001 || <0.001 LCS-1 93% mg/L 022 METALS-Cobalt-Dissolved mg/L 0.001 < 0.001 195634-1 <0.001 || <0.001 LCS-1 100% 022 Copper-Dissolved 0.001 METALS-LCS-1 mg/L < 0.001 195634-1 <0.001 || <0.001 97% 022 195634-1 Iron-Dissolved mg/L 0.01 METALS-< 0.01 <0.01||<0.01 LCS-1 106% 022 METALS-Lead-Dissolved mg/L 0.001 < 0.001 195634-1 <0.001 || <0.001 LCS-1 98% 022 METALS-Manganese-0.005 < 0.005 195634-1 <0.005 || <0.005 LCS-1 94% mg/L Dissolved 022 METALS-Mercury-Dissolved 0.0000 < 0.000 195634-1 <0.00005||<0.00005 LCS-1 98% mg/L 5 021 05 Molybdenummg/L 0.001 METALS-< 0.001 195634-1 0.003 | 0.003 | RPD: 0 LCS-1 102% Dissolved 022 Nickel-Dissolved 0.001 METALS-195634-1 <0.001 || <0.001 LCS-1 94% mg/L < 0.001 022 METALS-Selenium-Dissolved 0.001 195634-1 0.001 || 0.001 || RPD: 0 LCS-1 103% mg/L < 0.001 022 Antimony-Dissolved 0.001 METALS-<0.001 195634-1 <0.001 || <0.001 LCS-1 101% mg/L 022 Tin-Dissolved 0.001 METALS-<0.001 || <0.001 LCS-1 < 0.001 195634-1 105% mg/L 022 METALS-0.36 || 0.34 || RPD: 6 Strontium-Dissolved mg/L 0.001 < 0.001 195634-1 LCS-1 94% 022 Zinc-Dissolved 0.001 METALS-< 0.001 195634-1 <0.001 || <0.001 LCS-1 97% mg/L 022

| | | Client Reference | e: water Analysis - C | Water Analysis - Corunna Downs | | |
|--|-------|------------------|--------------------------------------|--------------------------------|------------------|--|
| QUALITY CONTROL Dissolved Metals in Water | UNITS | Dup. Sm# | Duplicate Base + Duplicate + %RPD | Spike Sm# | Spike % Recovery | |
| Date prepared | - | [NT] | [NT] | 195634-2 | 15/05/2017 | |
| Date analysed | - | [NT] | [NT] | 195634-2 | 15/05/2017 | |
| Aluminium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 84% | |
| Arsenic-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 94% | |
| Barium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 102% | |
| Boron-Dissolved | mg/L | [NT] | [NT] | 195634-2 | # | |
| Cadmium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 101% | |
| Chromium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 86% | |
| Cobalt-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 90% | |
| Copper-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 84% | |
| Iron-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 95% | |
| Lead-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 91% | |
| Manganese-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 86% | |
| Mercury-Dissolved | mg/L | [NT] | [NT] | [NR] | [NR] | |
| Molybdenum-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 103% | |
| Nickel-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 83% | |
| Selenium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 97% | |
| Antimony-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 98% | |
| Tin-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 101% | |
| Strontium-Dissolved | mg/L | [NT] | [NT] | 195634-2 | # | |
| Zinc-Dissolved | mg/L | [NT] | [NT] | 195634-2 | 89% | |

Report Comments:

Definitions:

NT: Not tested NA: Test not required INS: Insufficient sample for this test PQL: Practical Quantitation Limit

<: Less than >: Greater than RPD: Relative Percent Difference LCS: Laboratory Control Sample

NS: Not Specified NEPM: National Environmental Protection Measure NR: Not Reported

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011

MPL Reference: 195634 Revision No: R 00 Page 10 of 11

Quality Control Definitions

Blank: This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.

Duplicate: This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.

Matrix Spike: A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory Control Sample): This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike: Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.



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> email: lab@mpl.com.au envirolab.com.au

Envirolab Services (WA) Pty Ltd trading as MPL Laboratories | ABN 53 140 099 207

CERTIFICATE OF ANALYSIS 198030

Client:

Atlas Iron Limited Level 18, 300 Murray Street PERTH WA 6000

Attention: David Nyquest

Sample log in details:

Your Reference: Corunna Downs

No. of samples: 3 waters

Date/Time samples received: 10/07/2017 / 08:00

Date completed instructions received: 11/07/2017

Location:

Analysis Details:

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last pages of this report for any comments relating to the results.

Report Details:

Date results requested by: 18/07/17

Date of Preliminary Report: Not issued Issue Date: 18/07/17

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Accredited for compliance with ISO/IEC 17025 - Testing

Tests not covered by NATA are denoted with *.

Results Approved By:

Joshua Lim Operations Manager



| Miscellaneous Inorganics | | | | |
|-------------------------------|----------|------------|------------|------------|
| Our Reference: | UNITS | 198030-1 | 198030-2 | 198030-3 |
| Your Reference | | CRD0050 | CRD0082 | CRD0071 |
| Date Sampled | | 29/06/2017 | 2/07/2017 | 6/07/2017 |
| Type of sample | | water | water | water |
| Time Sampled | | 10:10 | | 07:20 |
| Date prepared | - | 12/07/2017 | 12/07/2017 | 12/07/2017 |
| Date analysed | - | 12/07/2017 | 12/07/2017 | 12/07/2017 |
| рН | pH Units | 7.1 | 7.0 | 7.0 |
| Electrical Conductivity (EC) | μS/cm | 840 | 950 | 790 |
| Total Dissolved Solids (grav) | mg/L | 510 | 570 | 480 |
| Total Suspended Solids | mg/L | <5 | <5 | <5 |
| Fluoride | mg/L | 0.3 | 0.4 | 0.4 |
| Nitrate as NO ₃ | mg/L | <0.5 | <0.5 | 4.6 |
| Nitrite as NO ₂ | mg/L | <0.5 | <0.5 | <0.5 |
| NOx as N | mg/L | 0.007 | 0.086 | 0.98 |

| Ionic Balance Our Reference: Your Reference Date Sampled Type of sample Time Sampled | UNITS | 198030-1 CRD0050 29/06/2017 water 10:10 | 198030-2 CRD0082 2/07/2017 water | 198030-3 CRD0071 6/07/2017 water 07:20 |
|--|-------|---|---|--|
| Date prepared | - | 13/07/2017 | 13/07/2017 | 13/07/2017 |
| Date analysed | - | 13/07/2017 | 13/07/2017 | 13/07/2017 |
| Calcium - Dissolved | mg/L | 61 | 66 | 79 |
| Potassium - Dissolved | mg/L | 1.6 | 1.3 | <0.5 |
| Magnesium - Dissolved | mg/L | 31 | 32 | 19 |
| Sodium - Dissolved | mg/L | 66 | 72 | 56 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 330 | 340 | 360 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | <5 | <5 |
| Hydroxide OH ⁻ as CaCO ₃ | mg/L | <5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 330 | 340 | 360 |
| Chloride | mg/L | 71 | 95 | 40 |
| Sulphate | mg/L | 42 | 49 | 22 |
| Ionic Balance | % | -5.2 | -6.9 | -5.0 |
| Hardness as CaCO ₃ | mg/L | 280 | 300 | 270 |

| Dissolved Metals in Water | | | | |
|---------------------------|-------|------------|------------|------------|
| Our Reference: | UNITS | 198030-1 | 198030-2 | 198030-3 |
| Your Reference | | CRD0050 | CRD0082 | CRD0071 |
| Date Sampled | | 29/06/2017 | 2/07/2017 | 6/07/2017 |
| Type of sample | | water | water | water |
| Time Sampled | | 10:10 | | 07:20 |
| Date prepared | - | 17/07/2017 | 17/07/2017 | 17/07/2017 |
| Date analysed | - | 17/07/2017 | 17/07/2017 | 17/07/2017 |
| Silica* | mg/L | 41 | 36 | 28 |
| Aluminium-Dissolved | mg/L | <0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.002 | 0.001 | 0.001 |
| Arsenic-Dissolved | mg/L | 0.003 | 0.002 | <0.001 |
| Barium-Dissolved | mg/L | 0.050 | 0.044 | 0.005 |
| Boron-Dissolved | mg/L | 0.22 | 0.23 | 0.1 |
| Cadmium-Dissolved | mg/L | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | 0.001 | 0.002 |
| Iron-Dissolved | mg/L | <0.01 | <0.01 | <0.01 |
| Lead-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.21 | 0.21 | 0.013 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Nickel-Dissolved | mg/L | 0.017 | 0.014 | 0.022 |
| Selenium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.32 | 0.38 | 0.43 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.016 | 0.003 | 0.021 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110 -B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-022 | Determination of various metals by ICP-MS. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |

| Client Reference: Corunna Downs | | | | | | | | |
|--|----------|-------|----------------|----------------|---------------|---------------------------|-----------|---------------------|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Miscellaneous Inorganics | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 12/07/ 2017 | 198030-1 | 12/07/2017 12/07/2017 | LCS-1 | 12/07/2017 |
| Date analysed | - | | | 12/07/ 2017 | 198030-1 | 12/07/2017 12/07/2017 | LCS-1 | 12/07/2017 |
| рН | pH Units | | INORG-001 | [NT] | 198030-1 | 7.1 7.1 RPD:0 | LCS-1 | 101% |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 198030-1 | 840 840 RPD:0 | LCS-1 | 99% |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 198030-1 | 510 500 RPD:2 | [NR] | [NR] |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 198030-1 | <5 [N/T] | LCS-1 | 110% |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 198030-1 | 0.3 0.3 RPD:0 | [NR] | [NR] |
| Nitrate as NO ₃ | mg/L | 0.5 | INORG-081 | <0.5 | 198030-1 | <0.5 <0.5 | [NR] | [NR] |
| Nitrite as NO2 | mg/L | 0.5 | INORG-081 | <0.5 | 198030-1 | <0.5 <0.5 | [NR] | [NR] |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 198030-1 | 0.007 [N/T] | LCS-1 | 99% |
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Ionic Balance | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 13/07/ 2017 | 198030-1 | 13/07/2017 13/07/2017 | LCS-1 | 13/07/2017 |
| Date analysed | - | | | 13/07/ 2017 | 198030-1 | 13/07/2017 13/07/2017 | LCS-1 | 13/07/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198030-1 | 61 [N/T] | LCS-1 | 103% |
| Potassium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198030-1 | 1.6 [N/T] | LCS-1 | 97% |
| Magnesium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198030-1 | 31 [N/T] | LCS-1 | 99% |
| Sodium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198030-1 | 66 [N/T] | LCS-1 | 102% |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 198030-1 | 330 330 RPD:0 | LCS-1 | 99% |
| Carbonate CO3 ² - as CaCO 3 | mg/L | 5 | INORG-006 | <5 | 198030-1 | <5 <5 | LCS-1 | 99% |
| Total Alkalinity as CaCO3 | mg/L | 5 | INORG-006 | <5 | 198030-1 | 330 330 RPD:0 | LCS-1 | 99% |
| Chloride | mg/L | 1 | INORG-081 | <1 | 198030-1 | 71 71 RPD: 0 | [NR] | [NR] |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 198030-1 | 42 42 RPD:0 | [NR] | [NR] |
| Hardness as CaCO ₃ | mg/L | 3 | METALS- 008 | <3 | 198030-1 | 280 [N/T] | [NR] | [NR] |

| Client Reference: Corunna Downs | | | | | | | | | |
|---------------------------------|-------|-------------|----------------|----------------|---------------|---------------------------|-----------|---------------------|--|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery | |
| Dissolved Metals in Water | | | | | | Base II Duplicate II %RPD | | Recovery | |
| Date prepared | - | | | 17/07/ 2017 | 198030-1 | 17/07/2017 17/07/2017 | LCS-1 | 17/07/2017 | |
| Date analysed | - | | | 17/07/ 2017 | 198030-1 | 17/07/2017 17/07/2017 | LCS-1 | 17/07/2017 | |
| Silica* | mg/L | 0.2 | METALS- 020 | <0.2 | 198030-1 | 41 [N/T] | LCS-1 | 110% | |
| Aluminium-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 198030-1 | <0.01 <0.01 | LCS-1 | 95% | |
| Antimony-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.002 0.002 RPD:0 | LCS-1 | 80% | |
| Arsenic-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.003 0.003 RPD:0 | LCS-1 | 98% | |
| Barium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.050 0.050 RPD:0 | LCS-1 | 97% | |
| Boron-Dissolved | mg/L | 0.02 | METALS- 022 | <0.02 | 198030-1 | 0.22 0.22 RPD:0 | LCS-1 | 103% | |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS- 022 | <0.000 | 198030-1 | <0.0001 <0.0001 | LCS-1 | 94% | |
| Chromium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 90% | |
| Cobalt-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 97% | |
| Copper-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.001 0.001 RPD: 0 | LCS-1 | 92% | |
| Iron-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 198030-1 | <0.01 0.01 | LCS-1 | 101% | |
| Lead-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 98% | |
| Manganese- Dissolved | mg/L | 0.005 | METALS- 022 | <0.005 | 198030-1 | 0.21 0.20 RPD: 5 | LCS-1 | 89% | |
| Mercury-Dissolved | mg/L | 0.0000 5 | METALS- 021 | <0.000 05 | 198030-1 | <0.00005 <0.00005 | LCS-1 | 112% | |
| Molybdenum- Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 93% | |
| Nickel-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.017 0.016 RPD:6 | LCS-1 | 89% | |
| Selenium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 99% | |
| Strontium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.32 0.31 RPD:3 | LCS-1 | 89% | |
| Tin-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | <0.001 <0.001 | LCS-1 | 94% | |
| Zinc-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198030-1 | 0.016 0.016 RPD:0 | LCS-1 | 99% | |

Client Reference: Corunna Downs QUALITYCONTROL UNITS Dup. Sm# **Duplicate** Spike Sm# Spike % Recovery Miscellaneous Inorganics Base + Duplicate + %RPD Date prepared [NT] [NT] 198030-2 12/07/2017 Date analysed [NT] [NT] 198030-2 12/07/2017 рΗ pH Units [NT] [NT] [NR] [NR] Electrical Conductivity (EC) μS/cm [NT] [NT] [NR] [NR] Total Dissolved Solids [NT] [NR] mg/L [NT] [NR] (grav) Total Suspended Solids mg/L [NT] [NT] [NR] [NR] Fluoride mg/L [NT] [NT] 198030-2 93% mg/L [NT] [NT] 198030-2 100% Nitrate as NO₃ Nitrite as NO2 mg/L [NT] [NT] 198030-2 101% NOx as N mg/L [NT] [NT] [NR] [NR] QUALITYCONTROL UNITS Dup. Sm# Duplicate Spike Sm# Spike % Recovery Base + Duplicate + %RPD Ionic Balance Date prepared [NT] [NT] 198030-2 13/07/2017 [NT] 198030-2 Date analysed [NT] 13/07/2017 [NR] Calcium - Dissolved [NT] [NT] [NR] mg/L Potassium - Dissolved [NT] [NT] [NR] [NR] mg/L Magnesium - Dissolved mg/L [NT] [NT] [NR] [NR] Sodium - Dissolved mg/L [NT] [NT] [NR] [NR] Bicarbonate HCO3 as mg/L [NT] [NT] [NR] [NR] CaCO₃ Carbonate CO3²⁻ as mg/L [NT] [NT] [NR] [NR] CaCO₃ Total Alkalinity as CaCO3 mg/L [NT] [NT] [NR] [NR]

[NT]

[NT]

[NT]

198030-2

198030-2

[NR]

99%

107%

[NR]

MPL Reference: 198030 Revision No: R 00

Chloride

Sulphate

Hardness as CaCO3

mg/L

mg/L

mg/L

[NT]

[NT]

[NT]

Client Reference: Corunna Downs QUALITYCONTROL UNITS Dup. Sm# **Duplicate** Spike Sm# Spike % Recovery Dissolved Metals in Water Base + Duplicate + %RPD Date prepared [NT] [NT] 198030-2 17/07/2017 Date analysed [NT] [NT] 198030-2 17/07/2017 Silica* mg/L [NT] [NT] [NR] [NR] Aluminium-Dissolved [NT] [NT] 198030-2 86% mg/L Antimony-Dissolved [NT] 198030-2 mg/L [NT] 79% Arsenic-Dissolved mg/L [NT] [NT] 198030-2 103% Barium-Dissolved mg/L [NT] [NT] 198030-2 105% Boron-Dissolved mg/L [NT] [NT] 198030-2 # Cadmium-Dissolved mg/L [NT] [NT] 198030-2 99% Chromium-Dissolved mg/L [NT] [NT] 198030-2 99% Cobalt-Dissolved mg/L [NT] [NT] 198030-2 94% Copper-Dissolved mg/L [NT] [NT] 198030-2 86% 198030-2 Iron-Dissolved mg/L [NT] [NT] 96% Lead-Dissolved [NT] [NT] 198030-2 93% mg/L [NT] 198030-2 Manganese-Dissolved mg/L [NT] 84% Mercury-Dissolved mg/L [NT] [NT] 198030-2 106% Molybdenum-Dissolved mg/L [NT] [NT] 198030-2 101% Nickel-Dissolved mg/L [NT] [NT] 198030-2 84%

[NT]

[NT]

[NT]

[NT]

198030-2

198030-2

198030-2

198030-2

106%

82%

95%

94%

[NT]

[NT]

[NT]

[NT]

mg/L

mg/L

mg/L

mg/L

MPL Reference: 198030 Revision No: R 00

Selenium-Dissolved

Strontium-Dissolved

Tin-Dissolved

Zinc-Dissolved

Report Comments:

Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

Definitions:

NT: Not tested NA: Test not required INS: Insufficient sample for this test PQL: Practical Quantitation Limit <: Less than >: Greater than RPD: Relative Percent Difference LCS: Laboratory Control Sample NS: Not Specified NEPM: National Environmental Protection Measure NR: Not Reported

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011

Quality Control Definitions

Blank: This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.

Duplicate: This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.

Matrix Spike: A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory Control Sample): This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike: Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.



16-18 Hayden Court, Myaree, Western Australia 6154 PO Box 4023 Myaree BC, Western Australia 6960 tel: +61 8 9317 2505

> email: lab@mpl.com.au envirolab.com.au

Envirolab Services (WA) Pty Ltd trading as MPL Laboratories | ABN 53 140 099 207

CERTIFICATE OF ANALYSIS 198330

Client:

Atlas Iron Limited Level 18, 300 Murray Street PERTH WA 6000

Attention: David Nyquest

Sample log in details:

Your Reference: Corunna Downs

No. of samples: 3 Water

Date/Time samples received: 17/08/2017 / 09:45

Date completed instructions received: 18/07/2017

Location:

Analysis Details:

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last pages of this report for any comments relating to the results.

Report Details:

Date results requested by: 24/07/17

Date of Preliminary Report: Not issued Issue Date: 24/07/17

NATA accreditation number 2901. This document shall not be reproduced except in full.

Accredited for compliance with ISO/IEC 17025 - Testing

Tests not covered by NATA are denoted with *.

Results Approved By:

Joshua Lim Operations Manager



| Miscellaneous Inorganics | | | | |
|-------------------------------|----------|---------------------|---------------------|---------------------|
| Our Reference: | UNITS | 198330-1 | 198330-2 | 198330-3 |
| Your Reference | | CRD0026 | CRD0062 | CRD0062 |
| Inviron ID | | 1831016 | 1831019 | 1831020 |
| Date Sampled Type of sample | | 09/07/2017 Water | 12/07/2017 Water | 15/07/2017 Water |
| Time Sampled | | 07:30 | 08:40 | 08:25 |
| Date prepared | - | 18/07/2017 | 18/07/2017 | 18/07/2017 |
| Date analysed | - | 18/07/2017 | 18/07/2017 | 18/07/2017 |
| рН | pH Units | 7.0 | 7.2 | 7.2 |
| Electrical Conductivity (EC) | μS/cm | 770 | 1,300 | 1,500 |
| Total Dissolved Solids (grav) | mg/L | 460 | 800 | 930 |
| Total Suspended Solids | mg/L | <5 | <5 | <5 |
| Fluoride | mg/L | 0.4 | 0.3 | 0.4 |
| Nitrate as N | mg/L | 0.82 | 1.4 | 1.7 |
| Nitrite as N | mg/L | 0.017 | 0.019 | 0.008 |
| NOx as N | mg/L | 0.83 | 1.4 | 1.8 |

| Ionic Balance | | | | |
|--------------------------------------|-------|------------|------------|------------|
| Our Reference: | UNITS | 198330-1 | 198330-2 | 198330-3 |
| Your Reference | | CRD0026 | CRD0062 | CRD0062 |
| Inviron ID | | 1831016 | 1831019 | 1831020 |
| Date Sampled | | 09/07/2017 | 12/07/2017 | 15/07/2017 |
| Type of sample | | Water | Water | Water |
| Time Sampled | | 07:30 | 08:40 | 08:25 |
| Date prepared | - | 18/07/2017 | 18/07/2017 | 18/07/2017 |
| Date analysed | - | 18/07/2017 | 18/07/2017 | 18/07/2017 |
| Calcium - Dissolved | mg/L | 88 | 89 | 97 |
| Potassium - Dissolved | mg/L | <0.5 | 1.2 | 1.1 |
| Magnesium - Dissolved | mg/L | 22 | 52 | 57 |
| Sodium - Dissolved | mg/L | 61 | 130 | 160 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 350 | 350 | 360 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | <5 | <5 | <5 |
| Total Alkalinity as CaCO₃ | mg/L | 350 | 350 | 360 |
| Chloride | mg/L | 42 | 190 | 220 |
| Sulphate | mg/L | 22 | 91 | 120 |
| Ionic Balance | % | 1.1 | 1.5 | 1.4 |
| Sum of Anions | meq/L | 7.42 | 12.9 | 14.6 |
| Sum of Cations | meq/L | 8.88 | 14.5 | 16.3 |
| Hardness as CaCO ₃ | mg/L | 310 | 440 | 480 |

| Dissolved Metals in Water | | | | |
|-----------------------------|-------|----------------|----------------|----------------|
| Our Reference: | UNITS | 198330-1 | 198330-2 | 198330-3 |
| Your Reference | | CRD0026 | CRD0062 | CRD0062 |
| Inviron ID | | 1831016 | 1831019 | 1831020 |
| Date Sampled | | 09/07/2017 | 12/07/2017 | 15/07/2017 |
| Type of sample Time Sampled | | Water 07:30 | Water 08:40 | Water 08:25 |
| | | | | |
| Date prepared | - | 20/07/2017 | 20/07/2017 | 20/07/2017 |
| Date analysed | - | 20/07/2017 | 20/07/2017 | 20/07/2017 |
| Silica* | mg/L | 31 | 41 | 43 |
| Aluminium-Dissolved | mg/L | <0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | <0.001 | 0.002 | 0.001 |
| Boron-Dissolved | mg/L | 0.2 | 0.24 | 0.29 |
| Barium-Dissolved | mg/L | 0.004 | 0.069 | 0.054 |
| Cadmium-Dissolved | mg/L | <0.0001 | <0.0001 | <0.0001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.05 | 0.03 | <0.01 |
| Lead-Dissolved | mg/L | <0.001 | 0.002 | 0.001 |
| Manganese-Dissolved | mg/L | 0.008 | 0.19 | 0.11 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | <0.001 | 0.002 | 0.002 |
| Nickel-Dissolved | mg/L | 0.014 | 0.41 | 0.006 |
| Selenium-Dissolved | mg/L | <0.001 | 0.002 | 0.002 |
| Strontium-Dissolved | mg/L | 0.44 | 0.62 | 0.69 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.034 | 0.13 | 0.012 |

| MethodID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110 -B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| INORG-055 | Nitrate - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | Nitrite - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-022 | Determination of various metals by ICP-MS. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |

| | Client Reference: | | | Corunna Downs | | | | |
|--|-------------------|-------|----------------|----------------|---------------|----------------------------|-----------|---------------------|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Miscellaneous Inorganics | | | | | | Base II Duplicate II %RPD | | , |
| Date prepared | - | | | 18/07/ 2017 | 198330-1 | 18/07/2017 18/07/2017 | LCS-1 | 18/07/2017 |
| Date analysed | - | | | 18/07/ 2017 | 198330-1 | 18/07/2017 18/07/2017 | LCS-1 | 18/07/2017 |
| рН | pH Units | | INORG-001 | [NT] | 198330-1 | 7.0 [N/T] | LCS-1 | 101% |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 198330-1 | 770 [N/T] | LCS-1 | 99% |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 198330-1 | 460 [N/T] | LCS-1 | 104% |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 198330-1 | <5 <5 | LCS-1 | 106% |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 198330-1 | 0.4 0.4 RPD:0 | LCS-1 | 93% |
| Nitrate as N | mg/L | 0.005 | INORG-055 | <0.005 | 198330-1 | 0.82 0.82 RPD:0 | LCS-1 | 104% |
| Nitrite as N | mg/L | 0.005 | INORG-055 | <0.005 | 198330-1 | 0.017 0.017 RPD:0 | LCS-1 | 104% |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 198330-1 | 0.83 0.84 RPD: 1 | LCS-1 | 104% |
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Ionic Balance | | | | | | Base II Duplicate II % RPD | | |
| Date prepared | - | | | 18/07/ 2017 | 198330-1 | 18/07/2017 18/07/2017 | LCS-1 | 18/07/2017 |
| Date analysed | - | | | 18/07/ 2017 | 198330-1 | 18/07/2017 18/07/2017 | LCS-1 | 18/07/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198330-1 | 88 [N/T] | LCS-1 | 105% |
| Potassium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198330-1 | <0.5 [N/T] | LCS-1 | 105% |
| Magnesium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198330-1 | 22 [N/T] | LCS-1 | 103% |
| Sodium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 198330-1 | 61 [N/T] | LCS-1 | 112% |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 198330-1 | 350 [N/T] | LCS-1 | 106% |
| Carbonate CO3 ² - as CaCO 3 | mg/L | 5 | INORG-006 | <5 | 198330-1 | <5 [N/T] | LCS-1 | 106% |
| Total Alkalinity as CaCO3 | mg/L | 5 | INORG-006 | <5 | 198330-1 | 350 [N/T] | LCS-1 | 106% |
| Chloride | mg/L | 1 | INORG-081 | <1 | 198330-1 | 42 42 RPD:0 | LCS-1 | 95% |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 198330-1 | 22 22 RPD:0 | LCS-1 | 96% |
| Hardness as CaCO ₃ | mg/L | 3 | METALS- 008 | <3 | 198330-1 | 310 [N/T] | [NR] | [NR] |

| Client Reference: Corunna Downs | | | | | | | | |
|---------------------------------|-------|-------------|----------------|----------------|---------------|---------------------------|-----------|---------------------|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Dissolved Metals in Water | | | | | | Base II Duplicate II %RPD | | Receivery |
| Date prepared | - | | | 20/07/ 2017 | 198330-1 | 20/07/2017 20/07/2017 | LCS-1 | 20/07/2017 |
| Date analysed | - | | | 20/07/ 2017 | 198330-1 | 20/07/2017 20/07/2017 | LCS-1 | 20/07/2017 |
| Silica* | mg/L | 0.2 | METALS- 020 | <0.2 | 198330-1 | 31 [N/T] | LCS-1 | 110% |
| Aluminium-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 198330-1 | <0.01 <0.01 | LCS-1 | 83% |
| Antimony-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 109% |
| Arsenic-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 93% |
| Boron-Dissolved | mg/L | 0.02 | METALS- 022 | <0.02 | 198330-1 | 0.2 0.2 RPD:0 | LCS-1 | 99% |
| Barium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | 0.004 0.004 RPD:0 | LCS-1 | 98% |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS- 022 | <0.000 | 198330-1 | <0.0001 <0.0001 | LCS-1 | 94% |
| Cobalt-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 96% |
| Chromium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 96% |
| Copper-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 93% |
| Iron-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 198330-1 | 0.05 0.05 RPD:0 | LCS-1 | 95% |
| Lead-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 97% |
| Manganese- Dissolved | mg/L | 0.005 | METALS- 022 | <0.005 | 198330-1 | 0.008 0.008 RPD:0 | LCS-1 | 88% |
| Mercury-Dissolved | mg/L | 0.0000 5 | METALS- 021 | <0.000 05 | 198330-1 | <0.00005 [N/T] | LCS-1 | 98% |
| Molybdenum- Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 91% |
| Nickel-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | 0.014 0.014 RPD:0 | LCS-1 | 91% |
| Selenium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 106% |
| Strontium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | 0.44 0.45 RPD:2 | LCS-1 | 89% |
| Tin-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | <0.001 <0.001 | LCS-1 | 98% |
| Zinc-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 198330-1 | 0.034 0.037 RPD:8 | LCS-1 | 94% |

Report Comments:

Definitions:

NT: Not tested NA: Test not required INS: Insufficient sample for this test PQL: Practical Quantitation Limit

<: Less than >: Greater than RPD: Relative Percent Difference LCS: Laboratory Control Sample

NS: Not Specified NEPM: National Environmental Protection Measure NR: Not Reported

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011

Quality Control Definitions

Blank: This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.

Duplicate: This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.

Matrix Spike: A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory Control Sample): This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike: Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.





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> email: lab@mpl.com.au envirolab.com.au

Envirolab Services (WA) Pty Ltd trading as MPL Laboratories | ABN 53 140 099 207

CERTIFICATE OF ANALYSIS 199108

Client:

Atlas Iron Limited Level 18, 300 Murray Street PERTH WA 6000

Attention: D Nyquest

Sample log in details:

Your Reference: Corunna Downs

No. of samples: 6 Water

Date/Time samples received: 04/08/2017 / 14:00

Date completed instructions received: 07/08/2017

Location:

Analysis Details:

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last pages of this report for any comments relating to the results.

Report Details:

Date results requested by: 11/08/17
Date of Preliminary Report: Not issued Issue Date: 10/08/17

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Accredited for compliance with ISO/IEC 17025 - Testing

Tests not covered by NATA are denoted with *.

Results Approved By:

Joshua Lim Operations Manager



| Miscellaneous Inorganics | | | | | | |
|-------------------------------|----------|------------|------------|------------|------------|------------|
| Our Reference: | UNITS | 199108-1 | 199108-2 | 199108-3 | 199108-4 | 199108-5 |
| Your Reference | | CRD00064 | CRD00064 | CRD00058 | CRD00058 | CRD00045 |
| Inviron ID | | 1831040 | 1831041 | 1831042 | 1831043 | 1831044 |
| Date Sampled | | 17/07/2017 | 20/07/2017 | 24/07/2017 | 27/07/2017 | 29/07/2017 |
| Time Sampled | | 14:10 | 13:50 | 09:00 | 08:30 | 10:10 |
| Type of sample | | GW | GW | GW | GW | GW |
| Date prepared | - | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 |
| Date analysed | - | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 |
| рН | pH Units | 7.2 | 7.2 | 7.5 | 7.5 | 7.2 |
| Electrical Conductivity (EC) | μS/cm | 1,400 | 1,400 | 2,900 | 3,000 | 1,100 |
| Total Dissolved Solids (grav) | mg/L | 820 | 830 | 1,700 | 1,800 | 650 |
| Total Suspended Solids | mg/L | <5 | <5 | <5 | <5 | <5 |
| Fluoride | mg/L | 0.6 | 0.6 | 1.6 | 1.6 | 0.6 |
| Nitrate as N | mg/L | 1.1 | 1.1 | 1.1 | 1.4 | 1.3 |
| Nitrite as N | mg/L | <0.005 | <0.005 | 0.022 | <0.005 | <0.005 |
| NOx as N | mg/L | 1.1 | 1.1 | 1.1 | 1.4 | 1.3 |

| | I | |
|-------------------------------|----------|------------|
| Miscellaneous Inorganics | | |
| Our Reference: | UNITS | 199108-6 |
| Your Reference | | CRD00045 |
| Inviron ID | | 1831045 |
| Date Sampled | | 01/08/2017 |
| Time Sampled | | 09:50 |
| Type of sample | | GW |
| Date prepared | - | 07/08/2017 |
| Date analysed | - | 07/08/2017 |
| рН | pH Units | 7.3 |
| Electrical Conductivity (EC) | μS/cm | 1,100 |
| Total Dissolved Solids (grav) | mg/L | 650 |
| Total Suspended Solids | mg/L | <5 |
| Fluoride | mg/L | 0.6 |
| Nitrate as N | mg/L | 1.2 |
| Nitrite as N | mg/L | <0.005 |
| NOx as N | mg/L | 1.2 |

| | | 1 | 1 | | | |
|--|---------|---------------------|---------------------|---------------------|---------------------|---------------------|
| Ionic Balance | LINITTO | 400400.4 | 400400.0 | 400400.0 | 100100 1 | 400400 5 |
| Our Reference: | UNITS | 199108-1 | 199108-2 | 199108-3 | 199108-4 | 199108-5 |
| Your Reference | | CRD00064 | CRD00064 | CRD00058 | CRD00058 | CRD00045 |
| Inviron ID | | 1831040 | 1831041 | 1831042 | 1831043 | 1831044 |
| Date Sampled | | 17/07/2017 14:10 | 20/07/2017 13:50 | 24/07/2017 09:00 | 27/07/2017 08:30 | 29/07/2017 10:10 |
| Time Sampled Type of sample | | GW | 13.50 GW | GW | 06.30 GW | GW |
| турс от заттрю | | CVV | GVV | OW | | OVV |
| Date prepared | - | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 |
| Date analysed | - | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 | 07/08/2017 |
| Calcium - Dissolved | mg/L | 61 | 62 | 22 | 22 | 64 |
| Potassium - Dissolved | mg/L | 2.5 | 2.6 | 1.4 | 1.3 | <0.5 |
| Magnesium - Dissolved | mg/L | 47 | 47 | 35 | 35 | 35 |
| Sodium - Dissolved | mg/L | 200 | 190 | 630 | 630 | 120 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 460 | 460 | 690 | 700 | 440 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 | <5 | <5 | <5 | <5 |
| Hydroxide OH ⁻ as CaCO ₃ | mg/L | <5 | <5 | <5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 460 | 460 | 690 | 700 | 440 |
| Chloride | mg/L | 180 | 180 | 480 | 500 | 84 |
| Sulphate | mg/L | 51 | 49 | 130 | 130 | 25 |
| Ionic Balance | % | 1.2 | 0.41 | 2.1 | 1.2 | -0.64 |
| Sum of Anions | meq/L | 13.7 | 13.6 | 27.6 | 28.2 | 10.1 |
| Sum of Cations | meq/L | 15.7 | 15.4 | 31.3 | 31.5 | 11.5 |
| Hardness as CaCO ₃ | mg/L | 350 | 350 | 200 | 200 | 310 |

| Ionic Balance | | |
|---------------------------------------|-------|------------|
| Our Reference: | UNITS | 199108-6 |
| Your Reference | | CRD00045 |
| Inviron ID | | 1831045 |
| Date Sampled | | 01/08/2017 |
| Time Sampled | | 09:50 |
| Type of sample | | GW |
| Date prepared | - | 07/08/2017 |
| Date analysed | - | 07/08/2017 |
| Calcium - Dissolved | mg/L | 67 |
| Potassium - Dissolved | mg/L | <0.5 |
| Magnesium - Dissolved | mg/L | 37 |
| Sodium - Dissolved | mg/L | 120 |
| Bicarbonate HCO3 as CaCO3 | mg/L | 440 |
| Carbonate CO3 ²⁻ as CaCO3 | mg/L | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 440 |
| Chloride | mg/L | 84 |
| Sulphate | mg/L | 24 |
| Ionic Balance | % | 0.089 |
| Sum of Anions | meq/L | 10.1 |
| Sum of Cations | meq/L | 11.8 |
| Hardness as CaCO ₃ | mg/L | 320 |

| Dissolved Metals in Water | | | | | | |
|-----------------------------|-------|-------------|-------------|-------------|-------------|-------------|
| Our Reference: | UNITS | 199108-1 | 199108-2 | 199108-3 | 199108-4 | 199108-5 |
| Your Reference | | CRD00064 | CRD00064 | CRD00058 | CRD00058 | CRD00045 |
| Inviron ID | | 1831040 | 1831041 | 1831042 | 1831043 | 1831044 |
| Date Sampled | | 17/07/2017 | 20/07/2017 | 24/07/2017 | 27/07/2017 | 29/07/2017 |
| Time Sampled Type of sample | | 14:10 GW | 13:50 GW | 09:00 GW | 08:30 GW | 10:10 GW |
| 71 1 | | | | _ | _ | |
| Date prepared | - | 10/08/2017 | 10/08/2017 | 10/08/2017 | 10/08/2017 | 10/08/2017 |
| Date analysed | - | 10/08/2017 | 10/08/2017 | 10/08/2017 | 10/08/2017 | 10/08/2017 |
| Silica* | mg/L | 44 | 44 | 48 | 51 | 44 |
| Aluminium-Dissolved | mg/L | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.003 | 0.002 | 0.012 | 0.014 | 0.002 |
| Barium-Dissolved | mg/L | 0.016 | 0.009 | 0.054 | 0.035 | 0.011 |
| Boron-Dissolved | mg/L | 0.29 | 0.30 | 0.84 | 0.82 | 0.25 |
| Cadmium-Dissolved | mg/L | <0.0001 | 0.0004 | 0.0004 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | <0.001 | <0.001 | 0.001 | 0.001 | <0.001 |
| Iron-Dissolved | mg/L | <0.01 | <0.01 | 0.01 | <0.01 | <0.01 |
| Lead-Dissolved | mg/L | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.007 | <0.005 | 0.086 | <0.005 | <0.005 |
| Mercury-Dissolved | mg/L | <0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.005 | 0.005 | 0.024 | 0.025 | 0.002 |
| Nickel-Dissolved | mg/L | 0.009 | 0.005 | 0.016 | 0.014 | <0.001 |
| Selenium-Dissolved | mg/L | <0.001 | <0.001 | 0.003 | 0.003 | <0.001 |
| Strontium-Dissolved | mg/L | 0.46 | 0.47 | 0.35 | 0.35 | 0.59 |
| Tin-Dissolved | mg/L | <0.001 | <0.001 | 0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.010 | 0.008 | 0.077 | 0.014 | 0.007 |

| Dissolved Metals in Water | | |
|---------------------------|-------|-----------------------|
| Our Reference: | UNITS | 199108-6 |
| Your Reference | | CRD00045 |
| Inviron ID | | 1831045 01/08/2017 |
| Date Sampled Time Sampled | | 01/06/2017 |
| Type of sample | | GW |
| Date prepared | - | 10/08/2017 |
| Date analysed | _ | 10/08/2017 |
| Silica* | mg/L | 44 |
| Aluminium-Dissolved | • | |
| | mg/L | <0.01 |
| Antimony-Dissolved | mg/L | <0.001 |
| Arsenic-Dissolved | mg/L | 0.002 |
| Barium-Dissolved | mg/L | 0.007 |
| Boron-Dissolved | mg/L | 0.25 |
| Cadmium-Dissolved | mg/L | <0.0001 |
| Chromium-Dissolved | mg/L | <0.001 |
| Cobalt-Dissolved | mg/L | <0.001 |
| Copper-Dissolved | mg/L | 0.002 |
| Iron-Dissolved | mg/L | <0.01 |
| Lead-Dissolved | mg/L | <0.001 |
| Manganese-Dissolved | mg/L | <0.005 |
| Mercury-Dissolved | mg/L | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.002 |
| Nickel-Dissolved | mg/L | 0.003 |
| Selenium-Dissolved | mg/L | <0.001 |
| Strontium-Dissolved | mg/L | 0.60 |
| Tin-Dissolved | mg/L | <0.001 |
| Zinc-Dissolved | mg/L | 0.020 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110 -B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| INORG-055 | Nitrate - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | Nitrite - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-022 | Determination of various metals by ICP-MS. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |

| Client Reference: Corunna Downs | | | | | | | | |
|--|----------|-------|----------------|----------------|---------------|---------------------------|-----------|---------------------|
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Miscellaneous Inorganics | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 07/08/ 2017 | 199108-1 | 07/08/2017 07/08/2017 | LCS-1 | 07/08/2017 |
| Date analysed | - | | | 07/08/ 2017 | 199108-1 | 07/08/2017 07/08/2017 | LCS-1 | 07/08/2017 |
| pН | pH Units | | INORG-001 | [NT] | 199108-1 | 7.2 [N/T] | LCS-1 | 101% |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 199108-1 | 1400 [N/T] | LCS-1 | 99% |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 199108-1 | 820 820 RPD: 0 | LCS-1 | 101% |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 199108-1 | <5 <5 | LCS-1 | 97% |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 199108-1 | 0.6 0.6 RPD:0 | LCS-1 | 101% |
| Nitrate as N | mg/L | 0.005 | INORG-055 | <0.005 | 199108-1 | 1.1 1.1 RPD: 0 | LCS-1 | 100% |
| Nitrite as N | mg/L | 0.005 | INORG-055 | <0.005 | 199108-1 | <0.005 <0.005 | LCS-1 | 107% |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 199108-1 | 1.1 1.1 RPD: 0 | LCS-1 | 100% |
| QUALITYCONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Ionic Balance | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 07/08/ 2017 | 199108-1 | 07/08/2017 07/08/2017 | LCS-1 | 07/08/2017 |
| Date analysed | - | | | 07/08/ 2017 | 199108-1 | 07/08/2017 07/08/2017 | LCS-1 | 07/08/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 199108-1 | 61 [N/T] | LCS-1 | 106% |
| Potassium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 199108-1 | 2.5 [N/T] | LCS-1 | 103% |
| Magnesium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 199108-1 | 47 [N/T] | LCS-1 | 104% |
| Sodium - Dissolved | mg/L | 0.5 | METALS- 020 | <0.5 | 199108-1 | 200 [N/T] | LCS-1 | 104% |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 199108-1 | 460 [N/T] | LCS-1 | 98% |
| Carbonate CO3 ² - as CaCO 3 | mg/L | 5 | INORG-006 | <5 | 199108-1 | <5 [N/T] | LCS-1 | 98% |
| Total Alkalinity as CaCO3 | mg/L | 5 | INORG-006 | <5 | 199108-1 | 460 [N/T] | LCS-1 | 98% |
| Chloride | mg/L | 1 | INORG-081 | <1 | 199108-1 | 180 180 RPD:0 | LCS-1 | 99% |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 199108-1 | 51 50 RPD:2 | LCS-1 | 101% |
| Hardness as CaCO3 | mg/L | 3 | METALS- 008 | <3 | 199108-1 | 350 [N/T] | [NR] | [NR] |

| | | C | lient Refere | nce: | Corunna Do | wns | | |
|---------------------------|-------|-------------|----------------|----------------|---------------|---------------------------|-----------|---------------------|
| QUALITY CONTROL | UNITS | PQL | METHOD | Blank | Duplicate Sm# | Duplicate results | Spike Sm# | Spike % Recovery |
| Dissolved Metals in Water | | | | | | Base II Duplicate II %RPD | | |
| Date prepared | - | | | 10/08/ 2017 | 199108-1 | 10/08/2017 10/08/2017 | LCS-1 | 10/08/2017 |
| Date analysed | - | | | 10/08/ 2017 | 199108-1 | 10/08/2017 10/08/2017 | LCS-1 | 10/08/2017 |
| Silica* | mg/L | 0.2 | METALS- 020 | <0.2 | 199108-1 | 44 [N/T] | LCS-1 | 106% |
| Aluminium-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 199108-1 | <0.01 <0.01 | LCS-1 | 94% |
| Antimony-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 80% |
| Arsenic-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.003 0.003 RPD:0 | LCS-1 | 96% |
| Barium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.016 0.016 RPD:0 | LCS-1 | 96% |
| Boron-Dissolved | mg/L | 0.02 | METALS- 022 | <0.02 | 199108-1 | 0.29 0.29 RPD:0 | LCS-1 | 90% |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS- 022 | <0.000 | 199108-1 | <0.0001 <0.0001 | LCS-1 | 97% |
| Chromium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 88% |
| Cobalt-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 97% |
| Copper-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 90% |
| Iron-Dissolved | mg/L | 0.01 | METALS- 022 | <0.01 | 199108-1 | <0.01 <0.01 | LCS-1 | 100% |
| Lead-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 103% |
| Manganese- Dissolved | mg/L | 0.005 | METALS- 022 | <0.005 | 199108-1 | 0.007 0.007 RPD:0 | LCS-1 | 93% |
| Mercury-Dissolved | mg/L | 0.0000 5 | METALS- 021 | <0.000 05 | 199108-1 | <0.00005 [N/T] | LCS-1 | 96% |
| Molybdenum- Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.005 0.006 RPD: 18 | LCS-1 | 95% |
| Nickel-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.009 0.009 RPD:0 | LCS-1 | 92% |
| Selenium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 94% |
| Strontium-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.46 0.47 RPD:2 | LCS-1 | 96% |
| Tin-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | <0.001 <0.001 | LCS-1 | 99% |
| Zinc-Dissolved | mg/L | 0.001 | METALS- 022 | <0.001 | 199108-1 | 0.010 0.010 RPD:0 | LCS-1 | 94% |

Client Reference: Corunna Downs QUALITYCONTROL UNITS Dup. Sm# **Duplicate** Spike Sm# Spike % Recovery Miscellaneous Inorganics Base + Duplicate + % RPD Date prepared [NT] [NT] 199108-2 07/08/2017 [NT] [NT] 199108-2 07/08/2017 Date analysed рΗ pH Units [NT] [NT] [NR] [NR] Electrical Conductivity (EC) [NT] [NT] [NR] [NR] µS/cm Total Dissolved Solids [NR] mg/L [NT] [NT] [NR] (grav) Total Suspended Solids mg/L [NT] [NT] [NR] [NR] Fluoride mg/L [NT] [NT] [NR] [NR] Nitrate as N [NT] [NT] 199108-2 105% mg/L Nitrite as N mg/L [NT] [NT] 199108-2 105% NO_x as N mg/L [NT] [NT] 199108-2 105% QUALITYCONTROL UNITS Dup. Sm# Duplicate Spike Sm# Spike % Recovery Dissolved Metals in Water Base + Duplicate + %RPD Date prepared [NT] [NT] 199108-2 08/08/2017 Date analysed [NT] [NT] 199108-2 08/08/2017 Silica* [NT] [NR] [NR] mg/L [NT] Aluminium-Dissolved [NT] 94% [NT] 199108-2 mg/L Antimony-Dissolved [NT] [NT] 199108-2 78% mg/L Arsenic-Dissolved mg/L [NT] [NT] 199108-2 106% Barium-Dissolved [NT] [NT] 199108-2 98% mg/L Boron-Dissolved mg/L [NT] [NT] 199108-2 # Cadmium-Dissolved mg/L [NT] [NT] 199108-2 108% Chromium-Dissolved [NT] 199108-2 89% mg/L [NT] Cobalt-Dissolved mg/L [NT] [NT] 199108-2 94% Copper-Dissolved mg/L [NT] [NT] 199108-2 85% Iron-Dissolved [NT] [NT] 199108-2 mg/L 99% Lead-Dissolved mg/L [NT] [NT] 199108-2 98% Manganese-Dissolved [NT] 199108-2 93% mg/L [NT] Mercury-Dissolved mg/L [NT] [NT] [NR] [NR] Molybdenum-Dissolved mg/L [NT] [NT] 199108-2 109% Nickel-Dissolved 199108-2 mg/L [NT] [NT] 86% Selenium-Dissolved mg/L [NT] [NT] 199108-2 104%

[NT]

[NT]

[NT]

MPL Reference: 199108 Revision No: R 00

mg/L

mg/L

mg/L

[NT]

[NT]

[NT]

Strontium-Dissolved

Tin-Dissolved

Zinc-Dissolved

111%

105%

93%

199108-2

199108-2

199108-2

Report Comments:

Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

Definitions:

NT: Not tested NA: Test not required INS: Insufficient sample for this test PQL: Practical Quantitation Limit <: Less than >: Greater than RPD: Relative Percent Difference LCS: Laboratory Control Sample NS: Not Specified NEPM: National Environmental Protection Measure NR: Not Reported

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011

MPL Reference: 199108
Revision No: R 00

Page 10 of 11

Quality Control Definitions

Blank: This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.

Duplicate: This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.

Matrix Spike: A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory Control Sample): This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike: Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.



Envirolab Services (WA) Pty Ltd trading as MPL Laboratories

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CERTIFICATE OF ANALYSIS 203451

| Client Details | |
|----------------|--|
| Client | Atlas Iron Limited |
| Attention | David Nyquest |
| Address | Level 18, 300 Murray Street, PERTH, WA, 6000 |

| Sample Details | |
|--------------------------------------|-----------------------|
| Your Reference | Atlas / Corunna Downs |
| Number of Samples | 6 Water |
| Date samples received | 20/11/2017 |
| Date completed instructions received | 20/11/2017 |

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last page of this report for any comments relating to the results.

| Report Details | | | | |
|---|---|--|--|--|
| Date results requested by | 27/11/2017 | | | |
| Date of Issue | 24/11/2017 | | | |
| NATA Accreditation Number 2901. This document shall not be reproduced except in full. | | | | |
| Accredited for compliance with ISO/IEO | C 17025 - Testing. Tests not covered by NATA are denoted with * | | | |

Results Approved By

Joshua Lim, Operations Manager

Authorised By

J.Lw

Todd Lee, Laboratory Manager

| Miscellaneous Inorganics | | | | | | | |
|-------------------------------|----------|-------|------------|------------|------------|------------|------------|
| Our Reference | | | 203451-1 | 203451-2 | 203451-3 | 203451-4 | 203451-5 |
| Your Reference | UNITS | PQL | CRD0043 | CRD0039 | CRD0056 | CRD0040 | CRD0051 |
| Date Sampled | | | 04/11/2017 | 06/11/2017 | 07/11/2017 | 10/11/2017 | 11/11/2017 |
| Type of sample | | | Water | Water | Water | Water | Water |
| Inviron ID | | | 1831056 | 1831057 | 1831058 | 1831059 | 1831060 |
| Date prepared | - | | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 |
| Date analysed | - | | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 |
| рН | pH Units | | 7.5 | 7.6 | 7.5 | 8.1 | 8.1 |
| Electrical Conductivity (EC) | μS/cm | 1 | 820 | 800 | 860 | 1,600 | 1,500 |
| Total Dissolved Solids (grav) | mg/L | 5 | 490 | 480 | 520 | 970 | 890 |
| Total Suspended Solids | mg/L | 5 | 140 | 310 | 440 | 110 | 21 |
| Fluoride | mg/L | 0.1 | 0.5 | 0.4 | 0.5 | 1.2 | 1.2 |
| Nitrate as NO ₃ | mg/L | 0.5 | 6.0 | 6.3 | 7.4 | 5.1 | 4.6 |
| Nitrite as NO ₂ | mg/L | 0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| NOx as N | mg/L | 0.005 | 1.5 | 1.7 | 1.9 | 1.4 | 1.3 |

| Miscellaneous Inorganics | | | |
|-------------------------------|----------|-------|------------|
| Our Reference | | | 203451-6 |
| Your Reference | UNITS | PQL | CRD0081 |
| Date Sampled | | | 12/11/2017 |
| Type of sample | | | Water |
| Inviron ID | | | 1831061 |
| Date prepared | - | | 20/11/2017 |
| Date analysed | - | | 20/11/2017 |
| pH | pH Units | | 7.9 |
| Electrical Conductivity (EC) | μS/cm | 1 | 980 |
| Total Dissolved Solids (grav) | mg/L | 5 | 590 |
| Total Suspended Solids | mg/L | 5 | 1,400 |
| Fluoride | mg/L | 0.1 | 0.7 |
| Nitrate as NO ₃ | mg/L | 0.5 | 8.1 |
| Nitrite as NO ₂ | mg/L | 0.5 | <0.5 |
| NOx as N | mg/L | 0.005 | 2.2 |

| Ionic Balance | | | | | | | |
|--|-------|-----|------------|------------|------------|------------|------------|
| Our Reference | | | 203451-1 | 203451-2 | 203451-3 | 203451-4 | 203451-5 |
| Your Reference | UNITS | PQL | CRD0043 | CRD0039 | CRD0056 | CRD0040 | CRD0051 |
| Date Sampled | | | 04/11/2017 | 06/11/2017 | 07/11/2017 | 10/11/2017 | 11/11/2017 |
| Type of sample | | | Water | Water | Water | Water | Water |
| Inviron ID | | | 1831056 | 1831057 | 1831058 | 1831059 | 1831060 |
| Date prepared | - | | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 |
| Date analysed | - | | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 | 20/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | 88 | 88 | 81 | 62 | 39 |
| Potassium - Dissolved | mg/L | 0.5 | <0.5 | <0.5 | <0.5 | <0.5 | 1.1 |
| Magnesium - Dissolved | mg/L | 0.5 | 26 | 30 | 25 | 67 | 61 |
| Sodium - Dissolved | mg/L | 0.5 | 75 | 72 | 82 | 190 | 190 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | 360 | 360 | 400 | 450 | 420 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 | <5 | <5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 | <5 | <5 | <5 | <5 |
| Total Alkalinity as CaCO₃ | mg/L | 5 | 360 | 360 | 400 | 450 | 420 |
| Chloride | mg/L | 1 | 66 | 56 | 75 | 240 | 200 |
| Sulphate | mg/L | 1 | 26 | 33 | 20 | 66 | 58 |
| Ionic Balance | % | | 0.99 | 2.6 | -4.4 | -0.75 | -0.47 |
| Hardness as CaCO₃ | mg/L | 3 | 330 | 340 | 300 | 430 | 350 |
| Sum of Anions | meq/L | 0 | 8.33 | 8.22 | 9.09 | 15.6 | 13.9 |
| Sum of Cations | meq/L | 0 | 9.84 | 10.0 | 9.64 | 17.0 | 15.3 |

| Ionic Balance | | | |
|--|-------|-----|------------|
| Our Reference | | | 203451-6 |
| Your Reference | UNITS | PQL | CRD0081 |
| Date Sampled | | | 12/11/2017 |
| Type of sample | | | Water |
| Inviron ID | | | 1831061 |
| Date prepared | - | | 20/11/2017 |
| Date analysed | - | | 20/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | 65 |
| Potassium - Dissolved | mg/L | 0.5 | <0.5 |
| Magnesium - Dissolved | mg/L | 0.5 | 45 |
| Sodium - Dissolved | mg/L | 0.5 | 92 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | 430 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 |
| Total Alkalinity as CaCO₃ | mg/L | 5 | 430 |
| Chloride | mg/L | 1 | 92 |
| Sulphate | mg/L | 1 | 36 |
| Ionic Balance | % | | -3.9 |
| Hardness as CaCO₃ | mg/L | 3 | 350 |
| Sum of Anions | meq/L | 0 | 10.4 |
| Sum of Cations | meq/L | 0 | 11.0 |

| Dissolved Metals in Water | | | | | | | |
|---------------------------|-------|---------|------------|------------|------------|------------|------------|
| Our Reference | | | 203451-1 | 203451-2 | 203451-3 | 203451-4 | 203451-5 |
| Your Reference | UNITS | PQL | CRD0043 | CRD0039 | CRD0056 | CRD0040 | CRD0051 |
| Date Sampled | | | 04/11/2017 | 06/11/2017 | 07/11/2017 | 10/11/2017 | 11/11/2017 |
| Type of sample | | | Water | Water | Water | Water | Water |
| Inviron ID | | | 1831056 | 1831057 | 1831058 | 1831059 | 1831060 |
| Date prepared | - | | 21/11/2017 | 21/11/2017 | 21/11/2017 | 21/11/2017 | 21/11/2017 |
| Date analysed | - | | 21/11/2017 | 21/11/2017 | 21/11/2017 | 21/11/2017 | 21/11/2017 |
| Silica | mg/L | 0.2 | 31 | 33 | 30 | 64 | 53 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 | 0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.001 | <0.001 | 0.001 | <0.001 | 0.01 | 0.006 |
| Barium-Dissolved | mg/L | 0.001 | 0.007 | 0.016 | 0.002 | 0.11 | 0.040 |
| Boron-Dissolved | mg/L | 0.02 | 0.20 | 0.2 | 0.21 | 0.39 | 0.36 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 | <0.0001 | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | 0.002 | 0.006 | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.01 | <0.01 | <0.01 | <0.01 | 0.06 | 0.02 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | 0.017 | 0.033 | 0.022 | 0.033 | 0.030 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | 0.006 | 0.007 |
| Nickel-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | 0.002 | 0.003 |
| Selenium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | 0.002 | 0.002 |
| Strontium-Dissolved | mg/L | 0.001 | 0.67 | 0.64 | 0.63 | 0.91 | 0.52 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.013 | <0.001 | 0.032 | 0.012 | <0.001 |

| Dissolved Metals in Water | | | |
|---------------------------|-------|---------|------------|
| Our Reference | | | 203451-6 |
| Your Reference | UNITS | PQL | CRD0081 |
| Date Sampled | | | 12/11/2017 |
| Type of sample | | | Water |
| Inviron ID | | | 1831061 |
| Date prepared | - | | 21/11/2017 |
| Date analysed | - | | 21/11/2017 |
| Silica | mg/L | 0.2 | 45 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.001 | 0.001 |
| Barium-Dissolved | mg/L | 0.001 | 0.029 |
| Boron-Dissolved | mg/L | 0.02 | 0.20 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.01 | <0.01 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | 0.078 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.001 | 0.006 |
| Nickel-Dissolved | mg/L | 0.001 | 0.003 |
| Selenium-Dissolved | mg/L | 0.001 | 0.001 |
| Strontium-Dissolved | mg/L | 0.001 | 0.49 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.002 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110-B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |
| METALS-022 | Determination of various metals by ICP-MS. |

MPL Reference: 203451 Page | **7 of 13**

Revision No: R00

| QUALITY COI | Duplicate | | | | Spike Recovery % | | | | | |
|-------------------------------|-----------|-------|-----------|------------|------------------|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203451-2 |
| Date prepared | - | | | 20/11/2017 | 1 | 20/11/2017 | 20/11/2017 | | 20/11/2017 | 20/11/2017 |
| Date analysed | - | | | 20/11/2017 | 1 | 20/11/2017 | 20/11/2017 | | 20/11/2017 | 20/11/2017 |
| рН | pH Units | | INORG-001 | [NT] | 1 | 7.5 | 7.5 | 0 | 101 | [NT] |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 1 | 820 | 810 | 1 | 101 | [NT] |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 1 | 490 | 480 | 2 | 102 | [NT] |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 1 | 140 | [NT] | | 99 | [NT] |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 1 | 0.5 | 0.5 | 0 | 87 | 84 |
| Nitrate as NO ₃ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | 6.0 | 6.0 | 0 | 100 | 96 |
| Nitrite as NO ₂ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | <0.5 | <0.5 | 0 | 99 | 98 |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | 1.5 | [NT] | | 113 | [NT] |

| QUALIT | | | Du | | Spike Recovery % | | | | | |
|--|-------|-----|------------|------------|------------------|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203451-2 |
| Date prepared | - | | | 20/11/2017 | 1 | 20/11/2017 | 20/11/2017 | | 20/11/2017 | 20/11/2017 |
| Date analysed | - | | | 20/11/2017 | 1 | 20/11/2017 | 20/11/2017 | | 20/11/2017 | 20/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 88 | 88 | 0 | 101 | 75 |
| Potassium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | <0.5 | <0.5 | 0 | 99 | 99 |
| Magnesium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 26 | 26 | 0 | 104 | 98 |
| Sodium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 75 | 74 | 1 | 99 | 88 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 360 | 370 | 3 | 100 | [NT] |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | <5 | <5 | 0 | 100 | [NT] |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 360 | 370 | 3 | 100 | [NT] |
| Chloride | mg/L | 1 | INORG-081 | <1 | 1 | 66 | 66 | 0 | 99 | 99 |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 1 | 26 | 26 | 0 | 99 | 100 |
| Hardness as CaCO ₃ | mg/L | 3 | METALS-008 | <3 | 1 | 330 | 330 | 0 | [NT] | [NT] |

| QUALITY CON | ALITY CONTROL: Dissolved Metals in Water Duplicate | | | | plicate | Spike Recovery % | | | | |
|----------------------|--|---------|------------|------------|---------|------------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203451-2 |
| Date prepared | - | | | 21/11/2017 | 1 | 21/11/2017 | 21/11/2017 | | 21/11/2017 | 21/11/2017 |
| Date analysed | - | | | 21/11/2017 | 1 | 21/11/2017 | 21/11/2017 | | 21/11/2017 | 21/11/2017 |
| Silica | mg/L | 0.2 | METALS-020 | <0.2 | 1 | 31 | 30 | 3 | 102 | 107 |
| Aluminium-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | <0.01 | 0 | 94 | 97 |
| Antimony-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 89 | 95 |
| Arsenic-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 95 | 107 |
| Barium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.007 | 0.007 | 0 | 87 | 93 |
| Boron-Dissolved | mg/L | 0.02 | METALS-022 | <0.02 | 1 | 0.20 | 0.2 | 0 | 96 | 106 |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS-022 | <0.0001 | 1 | <0.0001 | <0.0001 | 0 | 97 | 109 |
| Chromium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 93 | 99 |
| Cobalt-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.002 | 0.002 | 0 | 88 | 89 |
| Copper-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 92 | 90 |
| Iron-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | <0.01 | 0 | 95 | 98 |
| Lead-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 94 | 96 |
| Manganese-Dissolved | mg/L | 0.005 | METALS-022 | <0.005 | 1 | 0.017 | 0.017 | 0 | 97 | 97 |
| Mercury-Dissolved | mg/L | 0.00005 | METALS-021 | <0.00005 | 1 | <0.00005 | <0.00005 | 0 | 95 | 94 |
| Molybdenum-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 93 | 103 |
| Nickel-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 92 | 92 |
| Selenium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 91 | 116 |
| Strontium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.67 | 0.65 | 3 | 102 | # |
| Tin-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 93 | 97 |
| Zinc-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.013 | 0.012 | 8 | 95 | 97 |

| Result Definitions | | | | | | | | |
|--------------------|---|--|--|--|--|--|--|--|
| NT | Not tested | | | | | | | |
| NA | Test not required | | | | | | | |
| INS | Insufficient sample for this test | | | | | | | |
| PQL | Practical Quantitation Limit | | | | | | | |
| < | Less than | | | | | | | |
| > | Greater than | | | | | | | |
| RPD | Relative Percent Difference | | | | | | | |
| LCS | Laboratory Control Sample | | | | | | | |
| NS | Not specified | | | | | | | |
| NEPM | National Environmental Protection Measure | | | | | | | |
| NR | Not Reported | | | | | | | |

| Q | uality Contro | ol Definitions |
|---|--------------------------------|--|
| | Blank | This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples. |
| | Duplicate | This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable. |
| | Matrix Spike | A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist. |
| | CS (Laboratory Control Sample) | This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample. |
| | Surrogate Spike | Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples. |
| | | |

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

MPL Reference: 203451 Page | **12 of 13**Revision No: R00

Report Comments

Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

 MPL Reference:
 203451
 Page | 13 of 13

 Revision No:
 R00



Envirolab Services (WA) Pty Ltd trading as MPL Laboratories

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CERTIFICATE OF ANALYSIS 203775

| Client Details | |
|----------------|--|
| Client | Atlas Iron Limited |
| Attention | David Nyquest |
| Address | Level 18, 300 Murray Street, PERTH, WA, 6000 |

| Sample Details | |
|--------------------------------------|-------------------------------------|
| Your Reference | Atlas / Corunna Downs / Groundwater |
| Number of Samples | 2 Water |
| Date samples received | 27/11/2017 |
| Date completed instructions received | 27/11/2017 |

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last page of this report for any comments relating to the results.

| Report Details | | | | | |
|--|------------|--|--|--|--|
| Date results requested by | 04/12/2017 | | | | |
| Date of Issue | 04/12/2017 | | | | |
| NATA Accreditation Number 2901. This document shall not be reproduced except in full. | | | | | |
| Accredited for compliance with ISO/IEC 17025 - Testing. Tests not covered by NATA are denoted with * | | | | | |

Results Approved By

Joshua Lim, Operations Manager

Authorised By

J.Lw

Todd Lee, Laboratory Manager



| Miscellaneous Inorganics | | | | |
|-------------------------------|----------|-------|------------|------------|
| Our Reference | | | 203775-1 | 203775-2 |
| Your Reference | UNITS | PQL | CRD0088 | CRD0088 |
| Inviron ID | | | 1831072 | 1831074 |
| Date Sampled | | | 19/11/2017 | 22/11/2017 |
| Type of sample | | | Water | Water |
| Time Sampled | | | 04:30 PM | 04:10 PM |
| Date prepared | - | | 27/11/2017 | 27/11/2017 |
| Date analysed | - | | 27/11/2017 | 27/11/2017 |
| рН | pH Units | | 7.1 | 7.0 |
| Electrical Conductivity (EC) | μS/cm | 1 | 960 | 940 |
| Total Dissolved Solids (grav) | mg/L | 5 | 570 | 570 |
| Total Suspended Solids | mg/L | 5 | 13 | 5 |
| Fluoride | mg/L | 0.1 | 0.4 | 0.4 |
| Nitrate as NO ₃ | mg/L | 0.5 | 7.3 | 7.0 |
| Nitrite as NO ₂ | mg/L | 0.5 | <0.5 | <0.5 |
| NOx as N | mg/L | 0.005 | 1.9 | 1.9 |

| Ionic Balance | | | | |
|--|-------|-----|------------|------------|
| Our Reference | | | 203775-1 | 203775-2 |
| Your Reference | UNITS | PQL | CRD0088 | CRD0088 |
| Inviron ID | | | 1831072 | 1831074 |
| Date Sampled | | | 19/11/2017 | 22/11/2017 |
| Type of sample | | | Water | Water |
| Time Sampled | | | 04:30 PM | 04:10 PM |
| Date prepared | - | | 27/11/2017 | 27/11/2017 |
| Date analysed | - | | 27/11/2017 | 27/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | 93 | 93 |
| Potassium - Dissolved | mg/L | 0.5 | <0.5 | <0.5 |
| Magnesium - Dissolved | mg/L | 0.5 | 30 | 29 |
| Sodium - Dissolved | mg/L | 0.5 | 71 | 72 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | 380 | 380 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | 380 | 380 |
| Chloride | mg/L | 1 | 56 | 57 |
| Sulphate | mg/L | 1 | 35 | 34 |
| Ionic Balance | % | | 1.5 | 1.7 |
| Hardness as CaCO₃ | mg/L | 3 | 360 | 350 |
| Sum of Anions | meq/L | 0 | 8.51 | 8.48 |
| Sum of Cations | meq/L | 0 | 10.2 | 10.2 |

| Dissolved Metals in Water | | | | |
|---------------------------|-------|---------|------------|------------|
| Our Reference | | | 203775-1 | 203775-2 |
| Your Reference | UNITS | PQL | CRD0088 | CRD0088 |
| Inviron ID | | | 1831072 | 1831074 |
| Date Sampled | | | 19/11/2017 | 22/11/2017 |
| Type of sample | | | Water | Water |
| Time Sampled | | | 04:30 PM | 04:10 PM |
| Date prepared | - | | 30/11/2017 | 30/11/2017 |
| Date analysed | - | | 30/11/2017 | 30/11/2017 |
| Silica | mg/L | 0.2 | 32 | 32 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.001 | 0.002 | 0.001 |
| Barium-Dissolved | mg/L | 0.001 | 0.017 | 0.011 |
| Boron-Dissolved | mg/L | 0.02 | 0.2 | 0.2 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | 0.009 | 0.008 |
| Copper-Dissolved | mg/L | 0.001 | 0.014 | 0.004 |
| Iron-Dissolved | mg/L | 0.01 | <0.01 | <0.01 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | 0.027 | 0.023 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Nickel-Dissolved | mg/L | 0.001 | 0.015 | 0.008 |
| Selenium-Dissolved | mg/L | 0.001 | 0.001 | 0.001 |
| Strontium-Dissolved | mg/L | 0.001 | 0.69 | 0.71 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.049 | 0.015 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110-B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |
| METALS-022 | Determination of various metals by ICP-MS. |

 MPL Reference:
 203775
 Page | 5 of 11

 Revision No:
 R00

| QUALITY COI | QUALITY CONTROL: Miscellaneous Inorganics | | | | | | | | Spike Re | covery % |
|-------------------------------|---|-------|-----------|------------|---|------------|------------|-----|------------|----------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | [NT] |
| Date prepared | - | | | 27/11/2017 | 1 | 27/11/2017 | 27/11/2017 | | 27/11/2017 | |
| Date analysed | - | | | 27/11/2017 | 1 | 27/11/2017 | 27/11/2017 | | 27/11/2017 | |
| pH | pH Units | | INORG-001 | [NT] | 1 | 7.1 | 7.1 | 0 | 101 | |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 1 | 960 | 940 | 2 | 103 | |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 1 | 570 | 560 | 2 | 98 | |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 1 | 13 | [NT] | | [NT] | |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 1 | 0.4 | [NT] | | 81 | |
| Nitrate as NO ₃ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | 7.3 | [NT] | | 98 | |
| Nitrite as NO ₂ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | <0.5 | [NT] | | 99 | |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | 1.9 | [NT] | | 112 | [NT] |

| QUALIT | QUALITY CONTROL: Ionic Balance | | | | | | Duplicate | | | Spike Recovery % | |
|--|--------------------------------|-----|------------|------------|---|------------|------------|-----|------------|------------------|--|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203775-2 | |
| Date prepared | - | | | 27/11/2017 | 1 | 27/11/2017 | 27/11/2017 | | 27/11/2017 | 27/11/2017 | |
| Date analysed | - | | | 27/11/2017 | 1 | 27/11/2017 | 27/11/2017 | | 27/11/2017 | 27/11/2017 | |
| Calcium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 93 | 94 | 1 | 104 | 86 | |
| Potassium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | <0.5 | <0.5 | 0 | 104 | 104 | |
| Magnesium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 30 | 31 | 3 | 108 | 105 | |
| Sodium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 71 | 71 | 0 | 102 | 92 | |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 380 | 380 | 0 | 96 | [NT] | |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | <5 | <5 | 0 | 96 | [NT] | |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 380 | 380 | 0 | 96 | [NT] | |
| Chloride | mg/L | 1 | INORG-081 | <1 | 1 | 56 | [NT] | | 98 | [NT] | |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 1 | 35 | [NT] | | 98 | [NT] | |
| Hardness as CaCO ₃ | mg/L | 3 | METALS-008 | <3 | 1 | 360 | 360 | 0 | [NT] | [NT] | |

| QUALITY COI | NTROL: Diss | solved Me | tals in Water | | | Du | plicate | | Spike Re | covery % |
|----------------------|-------------|-----------|---------------|------------|---|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203775-2 |
| Date prepared | - | | | 30/11/2017 | 1 | 30/11/2017 | 29/11/2017 | | 30/11/2017 | 29/11/2017 |
| Date analysed | - | | | 30/11/2017 | 1 | 30/11/2017 | 29/11/2017 | | 30/11/2017 | 29/11/2017 |
| Silica | mg/L | 0.2 | METALS-020 | <0.2 | 1 | 32 | 33 | 3 | 107 | # |
| Aluminium-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | [NT] | | 92 | [NT] |
| Antimony-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 98 | [NT] |
| Arsenic-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.002 | [NT] | | 100 | [NT] |
| Barium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.017 | [NT] | | 109 | [NT] |
| Boron-Dissolved | mg/L | 0.02 | METALS-022 | <0.02 | 1 | 0.2 | [NT] | | 102 | [NT] |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS-022 | <0.0001 | 1 | <0.0001 | [NT] | | 99 | [NT] |
| Chromium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 103 | [NT] |
| Cobalt-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.009 | [NT] | | 105 | [NT] |
| Copper-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.014 | [NT] | | 108 | [NT] |
| Iron-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | [NT] | | 102 | [NT] |
| Lead-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 106 | [NT] |
| Manganese-Dissolved | mg/L | 0.005 | METALS-022 | <0.005 | 1 | 0.027 | [NT] | | 100 | [NT] |
| Mercury-Dissolved | mg/L | 0.00005 | METALS-021 | <0.00005 | 1 | <0.00005 | [NT] | | 94 | [NT] |
| Molybdenum-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 96 | [NT] |
| Nickel-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.015 | [NT] | | 106 | [NT] |
| Selenium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.001 | [NT] | | 111 | [NT] |
| Strontium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.69 | [NT] | | 97 | [NT] |
| Tin-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 100 | [NT] |
| Zinc-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.049 | [NT] | | 104 | [NT] |

| Result Definiti | Result Definitions | | | | | | | | |
|-----------------|---|--|--|--|--|--|--|--|--|
| NT | Not tested | | | | | | | | |
| NA | Test not required | | | | | | | | |
| INS | Insufficient sample for this test | | | | | | | | |
| PQL | Practical Quantitation Limit | | | | | | | | |
| < | Less than | | | | | | | | |
| > | Greater than | | | | | | | | |
| RPD | Relative Percent Difference | | | | | | | | |
| LCS | Laboratory Control Sample | | | | | | | | |
| NS | Not specified | | | | | | | | |
| NEPM | National Environmental Protection Measure | | | | | | | | |
| NR | Not Reported | | | | | | | | |

| Quality Contro | ol Definitions |
|------------------------------------|--|
| Blank | This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples. |
| Duplicate | This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable. |
| Matrix Spike | A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist. |
| LCS (Laboratory Control Sample) | This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample. |
| Surrogate Spike | Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples. |
| | |

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

MPL Reference: 203775 Page | **10 of 11**Revision No: R00

Report Comments

Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

MPL Reference: 203775 Page | 11 of 11 Revision No: R00



Envirolab Services (WA) Pty Ltd trading as MPL Laboratories

ABN 53 140 099 207 16-18 Hayden Court Myaree WA 6154 ph 08 9317 2505 fax 08 9317 4163 lab@mpl.com.au www.mpl.com.au

CERTIFICATE OF ANALYSIS 203908

| Client Details | |
|----------------|--|
| Client | Atlas Iron Limited |
| Attention | David Nyquest |
| Address | Level 18, 300 Murray Street, PERTH, WA, 6000 |

| Sample Details | |
|--------------------------------------|-------------------------------------|
| Your Reference | Atlas / Corunna Downs / Groundwater |
| Number of Samples | 2 Water |
| Date samples received | 29/11/2017 |
| Date completed instructions received | 29/11/2017 |

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

| Report Details | | | | |
|--|------------|--|--|--|
| Date results requested by | 06/12/2017 | | | |
| Date of Issue | 06/12/2017 | | | |
| NATA Accreditation Number 2901. This document shall not be reproduced except in full. | | | | |
| Accredited for compliance with ISO/IEC 17025 - Testing. Tests not covered by NATA are denoted with * | | | | |

Results Approved By

Joshua Lim, Operations Manager

Authorised By

Q.Lw

Todd Lee, Laboratory Manager



| Miscellaneous Inorganics | | | | |
|-------------------------------|----------|-------|------------|------------|
| Our Reference | | | 203908-1 | 203908-2 |
| Your Reference | UNITS | PQL | CRD0089 | CRD0089 |
| Inviron ID | | | 1831078 | 1831079 |
| Date Sampled | | | 24/11/2017 | 27/11/2017 |
| Type of sample | | | Water | Water |
| Date prepared | - | | 29/11/2017 | 29/11/2017 |
| Date analysed | - | | 29/11/2017 | 29/11/2017 |
| рН | pH Units | | 7.0 | 7.0 |
| Electrical Conductivity (EC) | μS/cm | 1 | 1,000 | 1,000 |
| Total Dissolved Solids (grav) | mg/L | 5 | 570 | 550 |
| Total Suspended Solids | mg/L | 5 | <5 | <5 |
| Fluoride | mg/L | 0.1 | 0.7 | 0.7 |
| Nitrate as NO ₃ | mg/L | 0.5 | 7.9 | 7.7 |
| Nitrite as NO ₂ | mg/L | 0.5 | <0.5 | <0.5 |
| NOx as N | mg/L | 0.005 | 1.8 | 1.7 |

| Ionic Balance | | | | |
|--|-------|-----|------------|------------|
| Our Reference | | | 203908-1 | 203908-2 |
| Your Reference | UNITS | PQL | CRD0089 | CRD0089 |
| Inviron ID | | | 1831078 | 1831079 |
| Date Sampled | | | 24/11/2017 | 27/11/2017 |
| Type of sample | | | Water | Water |
| Date prepared | - | | 29/11/2017 | 29/11/2017 |
| Date analysed | - | | 29/11/2017 | 29/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | 97 | 94 |
| Potassium - Dissolved | mg/L | 0.5 | <0.5 | <0.5 |
| Magnesium - Dissolved | mg/L | 0.5 | 25 | 25 |
| Sodium - Dissolved | mg/L | 0.5 | 83 | 81 |
| Bicarbonate HCO₃ as CaCO₃ | mg/L | 5 | 400 | 400 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | 400 | 400 |
| Chloride | mg/L | 1 | 77 | 76 |
| Sulphate | mg/L | 1 | 21 | 20 |
| Ionic Balance | % | | -0.43 | -0.92 |
| Hardness as CaCO₃ | mg/L | 3 | 350 | 340 |
| Sum of Anions | meq/L | 0 | 9.20 | 9.04 |
| Sum of Cations | meq/L | 0 | 10.6 | 10.3 |

| Dissolved Metals in Water | | | | |
|---------------------------|-------|---------|------------|------------|
| Our Reference | | | 203908-1 | 203908-2 |
| Your Reference | UNITS | PQL | CRD0089 | CRD0089 |
| Inviron ID | | | 1831078 | 1831079 |
| Date Sampled | | | 24/11/2017 | 27/11/2017 |
| Type of sample | | | Water | Water |
| Date prepared | - | | 04/12/2017 | 04/12/2017 |
| Date analysed | - | | 04/12/2017 | 04/12/2017 |
| Silica | mg/L | 0.2 | 31 | 30 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Barium-Dissolved | mg/L | 0.001 | 0.003 | 0.003 |
| Boron-Dissolved | mg/L | 0.02 | 0.20 | 0.20 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | 0.002 | 0.004 |
| Iron-Dissolved | mg/L | 0.01 | <0.01 | <0.01 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | 0.012 | 0.014 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Nickel-Dissolved | mg/L | 0.001 | <0.001 | 0.003 |
| Selenium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.001 | 0.66 | 0.63 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.006 | 0.008 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110-B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |
| METALS-022 | Determination of various metals by ICP-MS. |

 MPL Reference:
 203908
 Page | 5 of 10

 Revision No:
 R00

| QUALITY CONTROL: Miscellaneous Inorganics | | | | | | Duplicate Spike Re | | | | covery % |
|---|----------|-------|-----------|------------|---|--------------------|------------|-----|------------|----------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | [NT] |
| Date prepared | - | | | 29/11/2017 | 1 | 29/11/2017 | 29/11/2017 | | 29/11/2017 | |
| Date analysed | - | | | 29/11/2017 | 1 | 29/11/2017 | 29/11/2017 | | 29/11/2017 | |
| pH | pH Units | | INORG-001 | [NT] | 1 | 7.0 | 7.0 | 0 | 101 | |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 1 | 1000 | 1000 | 0 | 103 | |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 1 | 570 | [NT] | | 101 | |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 1 | <5 | [NT] | | 97 | |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 1 | 0.7 | [NT] | | 101 | |
| Nitrate as NO ₃ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | 7.9 | [NT] | | 100 | |
| Nitrite as NO ₂ | mg/L | 0.5 | INORG-081 | <0.5 | 1 | <0.5 | [NT] | | 104 | |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | 1.8 | [NT] | | 112 | [NT] |

| QUALITY CONTROL: Ionic Balance | | | | | | Du | plicate | | Spike Re | covery % |
|--|-------|-----|------------|------------|---|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203908-2 |
| Date prepared | - | | | 29/11/2017 | 1 | 29/11/2017 | 29/11/2017 | | 29/11/2017 | 29/11/2017 |
| Date analysed | - | | | 29/11/2017 | 1 | 29/11/2017 | 29/11/2017 | | 29/11/2017 | 29/11/2017 |
| Calcium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 97 | 97 | 0 | 110 | 78 |
| Potassium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | <0.5 | <0.5 | 0 | 107 | 103 |
| Magnesium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 25 | 26 | 4 | 110 | 104 |
| Sodium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 83 | 83 | 0 | 106 | [NT] |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 400 | 400 | 0 | 110 | [NT] |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | <5 | <5 | 0 | 110 | [NT] |
| Total Alkalinity as CaCO₃ | mg/L | 5 | INORG-006 | <5 | 1 | 400 | 400 | 0 | 110 | [NT] |
| Chloride | mg/L | 1 | INORG-081 | <1 | 1 | 77 | [NT] | | 99 | [NT] |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 1 | 21 | [NT] | | 97 | [NT] |
| Hardness as CaCO ₃ | mg/L | 3 | METALS-008 | <3 | 1 | 350 | 350 | 0 | [NT] | [NT] |

| QUALITY CONTROL: Dissolved Metals in Water | | | | | | Du | plicate | | Spike Re | covery % |
|--|-------|---------|------------|------------|---|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 203908-2 |
| Date prepared | - | | | 04/12/2017 | 1 | 04/12/2017 | 01/12/2017 | | 04/12/2017 | 01/12/2017 |
| Date analysed | - | | | 04/12/2017 | 1 | 04/12/2017 | 01/12/2017 | | 04/12/2017 | 01/12/2017 |
| Silica | mg/L | 0.2 | METALS-020 | <0.2 | 1 | 31 | 32 | 3 | 111 | 116 |
| Aluminium-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | [NT] | | 89 | [NT] |
| Antimony-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 96 | [NT] |
| Arsenic-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 98 | [NT] |
| Barium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.003 | [NT] | | 99 | [NT] |
| Boron-Dissolved | mg/L | 0.02 | METALS-022 | <0.02 | 1 | 0.20 | [NT] | | 99 | [NT] |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS-022 | <0.0001 | 1 | <0.0001 | [NT] | | 102 | [NT] |
| Chromium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 91 | [NT] |
| Cobalt-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 93 | [NT] |
| Copper-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.002 | [NT] | | 92 | [NT] |
| Iron-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | [NT] | | 92 | [NT] |
| Lead-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 99 | [NT] |
| Manganese-Dissolved | mg/L | 0.005 | METALS-022 | <0.005 | 1 | 0.012 | [NT] | | 94 | [NT] |
| Mercury-Dissolved | mg/L | 0.00005 | METALS-021 | <0.00005 | 1 | <0.00005 | [NT] | | 94 | [NT] |
| Molybdenum-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 99 | [NT] |
| Nickel-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 93 | [NT] |
| Selenium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 100 | [NT] |
| Strontium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.66 | [NT] | | 100 | [NT] |
| Tin-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | [NT] | | 101 | [NT] |
| Zinc-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.006 | [NT] | | 94 | [NT] |

| Result Definiti | ons |
|-----------------|---|
| NT | Not tested |
| NA | Test not required |
| INS | Insufficient sample for this test |
| PQL | Practical Quantitation Limit |
| < | Less than |
| > | Greater than |
| RPD | Relative Percent Difference |
| LCS | Laboratory Control Sample |
| NS | Not specified |
| NEPM | National Environmental Protection Measure |
| NR | Not Reported |

| Quality Control | ol Definitions |
|------------------------------------|--|
| Blank | This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples. |
| Duplicate | This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable. |
| Matrix Spike | A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist. |
| LCS (Laboratory Control Sample) | This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample. |
| Surrogate Spike | Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples. |
| | |

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

MPL Reference: 203908 Page | **10 of 10**Revision No: R00



Envirolab Services (WA) Pty Ltd trading as MPL Laboratories

ABN 53 140 099 207 16-18 Hayden Court Myaree WA 6154 ph 08 9317 2505 fax 08 9317 4163 lab@mpl.com.au www.mpl.com.au

CERTIFICATE OF ANALYSIS 206060

| Client Details | |
|----------------|--|
| Client | Atlas Iron Limited |
| Attention | Esme Wink |
| Address | Level 18, 300 Murray Street, PERTH, WA, 6000 |

| Sample Details | |
|--------------------------------------|-------------------------------------|
| Your Reference | Corunna Downs / 53276 / Groundwater |
| Number of Samples | 8 Water |
| Date samples received | 29/01/2018 |
| Date completed instructions received | 29/01/2018 |

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

| Report Details | |
|---------------------------------------|--|
| Date results requested by | 05/02/2018 |
| Date of Issue | 05/02/2018 |
| NATA Accreditation Number 2901. Th | nis document shall not be reproduced except in full. |
| Accredited for compliance with ISO/IE | EC 17025 - Testing. Tests not covered by NATA are denoted with * |

Results Approved By

Todd Lee, Laboratory Manager, Perth

Authorised By

Q.Lw

Todd Lee, Laboratory Manager



| Miscellaneous Inorganics | | | | | | | |
|-------------------------------|----------|-------|-------------|-------------|-------------|-------------|-------------------------------------|
| Our Reference | | | 206060-1 | 206060-2 | 206060-3 | 206060-4 | 206060-5 |
| Your Reference | UNITS | PQL | CRD0071 | CRD0083 | CRD0082 | CRD0027 | CRD0004 (CDWB0001- Camp Bore) |
| Inviron ID | | | 1831102 | 1831103 | 1831104 | 1831105 | 1831106 |
| Date Sampled | | | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 10:45 AM | 11:05 AM | 11:30 AM | 12:30 PM | 02:20 PM |
| Date prepared | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Date analysed | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| рН | pH Units | | 6.9 | 7.4 | 7.2 | 6.2 | 7.7 |
| Electrical Conductivity (EC) | μS/cm | 1 | 820 | 790 | 850 | 48 | 1,400 |
| Total Dissolved Solids (grav) | mg/L | 5 | 490 | 480 | 510 | 29 | 780 |
| Total Suspended Solids | mg/L | 5 | <5 | <5 | <5 | 50 | <5 |
| Fluoride | mg/L | 0.1 | 0.3 | 0.2 | 0.1 | <0.1 | 0.3 |
| Nitrate as N | mg/L | 0.005 | 0.006 | <0.005 | 0.025 | 1.1 | 0.29 |
| Nitrite as N | mg/L | 0.005 | <0.005 | <0.005 | <0.005 | 0.027 | 1.9 |
| NOx as N | mg/L | 0.005 | 0.006 | <0.005 | 0.026 | 1.1 | 2.2 |

| Miscellaneous Inorganics | | | | | |
|-------------------------------|----------|-------|------------------------------------|-----------------------|-------------|
| Our Reference | | | 206060-6 | 206060-7 | 206060-8 |
| Your Reference | UNITS | PQL | CRD0005 (CDWB0002- Kasabian) | CRD0003 (CDRC0014) | CRD0024 |
| Inviron ID | | | 1831107 | 1831108 | 1831109 |
| Date Sampled | | | 23/01/2018 | 24/01/2018 | 24/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 02:45 PM | 11:00 AM | 12:20 PM |
| Date prepared | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Date analysed | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| рН | pH Units | | 7.2 | 6.6 | 5.6 |
| Electrical Conductivity (EC) | μS/cm | 1 | 1,100 | 570 | 93 |
| Total Dissolved Solids (grav) | mg/L | 5 | 610 | 340 | 56 |
| Total Suspended Solids | mg/L | 5 | 35 | 120 | 19 |
| Fluoride | mg/L | 0.1 | 0.2 | 0.2 | <0.1 |
| Nitrate as N | mg/L | 0.005 | 1.6 | <0.005 | 1.1 |
| Nitrite as N | mg/L | 0.005 | <0.005 | <0.005 | <0.005 |
| NOx as N | mg/L | 0.005 | 1.6 | <0.005 | 1.1 |

| Ionic Balance | | | | | | | |
|--|-------|-----|-------------|-------------|-------------|-------------|-------------------------------------|
| Our Reference | | | 206060-1 | 206060-2 | 206060-3 | 206060-4 | 206060-5 |
| Your Reference | UNITS | PQL | CRD0071 | CRD0083 | CRD0082 | CRD0027 | CRD0004 (CDWB0001- Camp Bore) |
| Inviron ID | | | 1831102 | 1831103 | 1831104 | 1831105 | 1831106 |
| Date Sampled | | | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 10:45 AM | 11:05 AM | 11:30 AM | 12:30 PM | 02:20 PM |
| Date prepared | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Date analysed | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Calcium - Dissolved | mg/L | 0.5 | 61 | 76 | 62 | 2.7 | 47 |
| Potassium - Dissolved | mg/L | 0.5 | 1.3 | 1.9 | 2.6 | 0.5 | 5.5 |
| Magnesium - Dissolved | mg/L | 0.5 | 30 | 24 | 32 | 1.2 | 51 |
| Sodium - Dissolved | mg/L | 0.5 | 60 | 66 | 62 | 3.5 | 94 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | 320 | 320 | 340 | 12 | 510 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 | <5 | <5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 | <5 | <5 | <5 | <5 |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | 320 | 320 | 340 | 12 | 510 |
| Chloride | mg/L | 1 | 47 | 41 | 46 | 3 | 120 |
| Sulphate | mg/L | 1 | 39 | 27 | 39 | 2 | 14 |
| Sum of Anions | meq/L | 0 | 7.29 | 6.98 | 7.69 | 0.304 | 12.0 |
| Sum of Cations | meq/L | 0 | 8.20 | 8.69 | 8.51 | 0.396 | 10.8 |
| Ionic Balance | % | | -1.4 | 3.3 | -2.3 | 6.6 | -12 |
| Hardness as CaCO₃ | mg/L | 3 | 280 | 290 | 290 | 12 | 330 |

| Ionic Balance | | | | | |
|--|-------|-----|------------------------------------|-----------------------|-------------|
| Our Reference | | | 206060-6 | 206060-7 | 206060-8 |
| Your Reference | UNITS | PQL | CRD0005 (CDWB0002- Kasabian) | CRD0003 (CDRC0014) | CRD0024 |
| Inviron ID | | | 1831107 | 1831108 | 1831109 |
| Date Sampled | | | 23/01/2018 | 24/01/2018 | 24/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 02:45 PM | 11:00 AM | 12:20 PM |
| Date prepared | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Date analysed | - | | 29/01/2018 | 29/01/2018 | 29/01/2018 |
| Calcium - Dissolved | mg/L | 0.5 | 76 | 20 | 1.8 |
| Potassium - Dissolved | mg/L | 0.5 | 1.6 | 3.0 | 0.8 |
| Magnesium - Dissolved | mg/L | 0.5 | 56 | 31 | 3.4 |
| Sodium - Dissolved | mg/L | 0.5 | 59 | 35 | 7.9 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | 450 | 100 | 16 |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | <5 | <5 | <5 |
| Hydroxide OH⁻ as CaCO₃ | mg/L | 5 | <5 | <5 | <5 |
| Total Alkalinity as CaCO₃ | mg/L | 5 | 450 | 100 | 16 |
| Chloride | mg/L | 1 | 64 | 60 | 11 |
| Sulphate | mg/L | 1 | 18 | 74 | 1 |
| Sum of Anions | meq/L | 0 | 9.49 | 4.93 | 0.591 |
| Sum of Cations | meq/L | 0 | 11.0 | 5.14 | 0.732 |
| Ionic Balance | % | | -0.33 | -1.6 | 6.1 |
| Hardness as CaCO₃ | mg/L | 3 | 420 | 180 | 18 |

| Dissolved Metals in Water | | | | | | | |
|---------------------------|-------|---------|-------------|-------------|-------------|-------------|-------------------------------------|
| Our Reference | | | 206060-1 | 206060-2 | 206060-3 | 206060-4 | 206060-5 |
| Your Reference | UNITS | PQL | CRD0071 | CRD0083 | CRD0082 | CRD0027 | CRD0004 (CDWB0001- Camp Bore) |
| Inviron ID | | | 1831102 | 1831103 | 1831104 | 1831105 | 1831106 |
| Date Sampled | | | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 | 23/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 10:45 AM | 11:05 AM | 11:30 AM | 12:30 PM | 02:20 PM |
| Date prepared | - | | 31/01/2018 | 31/01/2018 | 31/01/2018 | 31/01/2018 | 31/01/2018 |
| Date analysed | - | | 31/01/2018 | 31/01/2018 | 31/01/2018 | 31/01/2018 | 31/01/2018 |
| Silica | mg/L | 0.2 | 28 | 29 | 48 | 3.3 | 39 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 | <0.01 | 0.06 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | 0.004 | <0.001 | 0.002 |
| Arsenic-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | 0.006 | <0.001 | 0.002 |
| Barium-Dissolved | mg/L | 0.001 | 0.10 | 0.088 | 0.070 | 0.004 | 0.084 |
| Boron-Dissolved | mg/L | 0.02 | 0.2 | 0.2 | 0.25 | <0.02 | 0.25 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 | <0.0001 | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | 0.002 | <0.001 | <0.001 | 0.001 | 0.002 |
| Iron-Dissolved | mg/L | 0.01 | 0.30 | <0.01 | <0.01 | 0.05 | 0.07 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | 0.33 | 0.012 | 0.20 | 0.027 | 0.13 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 | <0.00005 |
| Molybdenum-Dissolved | mg/L | 0.001 | <0.001 | 0.002 | <0.001 | <0.001 | 0.001 |
| Nickel-Dissolved | mg/L | 0.001 | 0.001 | <0.001 | <0.001 | <0.001 | 0.002 |
| Selenium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.001 | 0.28 | 0.51 | 0.28 | 0.015 | 0.28 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.014 | 0.007 | 0.009 | 0.005 | 0.009 |

| Dissolved Metals in Water | | | | | |
|---------------------------|-------|---------|------------------------------------|-----------------------|-------------|
| Our Reference | | | 206060-6 | 206060-7 | 206060-8 |
| Your Reference | UNITS | PQL | CRD0005 (CDWB0002- Kasabian) | CRD0003 (CDRC0014) | CRD0024 |
| Inviron ID | | | 1831107 | 1831108 | 1831109 |
| Date Sampled | | | 23/01/2018 | 24/01/2018 | 24/01/2018 |
| Type of sample | | | Groundwater | Groundwater | Groundwater |
| Time Sampled | | | 02:45 PM | 11:00 AM | 12:20 PM |
| Date prepared | - | | 31/01/2018 | 31/01/2018 | 31/01/2018 |
| Date analysed | - | | 31/01/2018 | 31/01/2018 | 31/01/2018 |
| Silica | mg/L | 0.2 | 39 | 18 | 17 |
| Aluminium-Dissolved | mg/L | 0.01 | <0.01 | <0.01 | <0.01 |
| Antimony-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Arsenic-Dissolved | mg/L | 0.001 | 0.002 | <0.001 | <0.001 |
| Barium-Dissolved | mg/L | 0.001 | 0.073 | 0.015 | 0.007 |
| Boron-Dissolved | mg/L | 0.02 | 0.23 | 0.1 | 0.05 |
| Cadmium-Dissolved | mg/L | 0.0001 | <0.0001 | <0.0001 | <0.0001 |
| Chromium-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Cobalt-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Copper-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Iron-Dissolved | mg/L | 0.01 | <0.01 | 0.04 | <0.01 |
| Lead-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Manganese-Dissolved | mg/L | 0.005 | <0.005 | 0.45 | 0.016 |
| Mercury-Dissolved | mg/L | 0.00005 | <0.00005 | <0.00005 | 0.00008 |
| Molybdenum-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Nickel-Dissolved | mg/L | 0.001 | <0.001 | 0.001 | 0.003 |
| Selenium-Dissolved | mg/L | 0.001 | 0.002 | <0.001 | <0.001 |
| Strontium-Dissolved | mg/L | 0.001 | 0.20 | 0.095 | 0.023 |
| Tin-Dissolved | mg/L | 0.001 | <0.001 | <0.001 | <0.001 |
| Zinc-Dissolved | mg/L | 0.001 | 0.007 | 0.005 | 0.008 |

| Method ID | Methodology Summary |
|------------|---|
| INORG-001 | pH - Measured using pH meter and electrode base on APHA latest edition, Method 4500-H+. Please note that the results for water analyses may be indicative only, as analysis can be completed outside of the APHA recommended holding times. Soils are reported from a 1:5 water extract unless otherwise specified. |
| INORG-002 | Conductivity and Salinity - measured using a conductivity cell at 25°C based on APHA latest edition Method 2510. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-006 | Alkalinity - determined titrimetrically based on APHA latest edition, Method 2320-B. Soils reported from a 1:5 water extract unless otherwise specified. |
| INORG-018 | Total Dissolved Solids - determined gravimetrically. The solids are dried at 180±5°C |
| INORG-019 | Suspended Solids - determined gravimetrically by filtration of the sample. The samples are dried at 104+/-5oC. |
| INORG-040 | Ion Balance Calculation: Cations in water by ICP-OES; Anions in water by IC; Alkalinity in water by Titration using APHA methods. |
| INORG-055 | Nitrite - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | Nitrate - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-055 | NOx - determined colourimetrically. Soils are analysed from a water extract. |
| INORG-081 | Anions - a range of anions are determined by Ion Chromatography based on APHA latest edition Method 4110-B. Soils and other sample types reported from a water extract unless otherwise specified (standard soil extract ratio 1:5). |
| METALS-008 | Hardness calculated from Calcium and Magnesium as per APHA latest edition 2340B. |
| METALS-020 | Metals in soil and water by ICP-OES. |
| METALS-021 | Determination of Mercury by Cold Vapour AAS. |
| METALS-022 | Determination of various metals by ICP-MS. |

 MPL Reference:
 206060
 Page | 7 of 13

 Revision No:
 R00

| QUALITY CONTROL: Miscellaneous Inorganics | | | | | | Du | | Spike Recovery % | | |
|---|----------|-------|-----------|------------|---|------------|------------|------------------|------------|------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | [NT] |
| Date prepared | - | | | 29/01/2018 | 1 | 29/01/2018 | 29/01/2018 | | 29/01/2018 | |
| Date analysed | - | | | 29/01/2018 | 1 | 29/01/2018 | 29/01/2018 | | 29/01/2018 | |
| рН | pH Units | | INORG-001 | [NT] | 1 | 6.9 | 6.9 | 0 | 101 | |
| Electrical Conductivity (EC) | μS/cm | 1 | INORG-002 | <1 | 1 | 820 | 820 | 0 | 109 | |
| Total Dissolved Solids (grav) | mg/L | 5 | INORG-018 | <5 | 1 | 490 | 490 | 0 | 105 | |
| Total Suspended Solids | mg/L | 5 | INORG-019 | <5 | 1 | <5 | [NT] | | 105 | |
| Fluoride | mg/L | 0.1 | INORG-081 | <0.1 | 1 | 0.3 | 0.3 | 0 | 95 | |
| Nitrate as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | 0.006 | 0.006 | 0 | 94 | |
| Nitrite as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | <0.005 | <0.005 | 0 | 119 | |
| NOx as N | mg/L | 0.005 | INORG-055 | <0.005 | 1 | 0.006 | 0.006 | 0 | 103 | [NT] |

| QUALITY CONTROL: Ionic Balance | | | | | | Du | Spike Recovery % | | | |
|--|-------|-----|------------|------------|---|------------|------------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 206060-2 |
| Date prepared | - | | | 29/01/2018 | 1 | 29/01/2018 | 29/01/2018 | | 29/01/2018 | 29/01/2018 |
| Date analysed | - | | | 29/01/2018 | 1 | 29/01/2018 | 29/01/2018 | | 29/01/2018 | 29/01/2018 |
| Calcium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 61 | 61 | 0 | 98 | [NT] |
| Potassium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 1.3 | 1.3 | 0 | 100 | 98 |
| Magnesium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 30 | 30 | 0 | 99 | 90 |
| Sodium - Dissolved | mg/L | 0.5 | METALS-020 | <0.5 | 1 | 60 | 60 | 0 | 98 | 91 |
| Bicarbonate HCO ₃ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 320 | 310 | 3 | 102 | [NT] |
| Carbonate CO ₃ ²⁻ as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | <5 | <5 | 0 | 102 | [NT] |
| Total Alkalinity as CaCO ₃ | mg/L | 5 | INORG-006 | <5 | 1 | 320 | 310 | 3 | 102 | [NT] |
| Chloride | mg/L | 1 | INORG-081 | <1 | 1 | 47 | 47 | 0 | 99 | [NT] |
| Sulphate | mg/L | 1 | INORG-081 | <1 | 1 | 39 | 39 | 0 | 108 | [NT] |
| Hardness as CaCO ₃ | mg/L | 3 | METALS-008 | <3 | 1 | 280 | 280 | 0 | [NT] | [NT] |

| QUALITY CON | NTROL: Diss | solved Me | tals in Water | | | Du | plicate | | Spike Re | covery % |
|----------------------|-------------|-----------|---------------|------------|---|------------|------------|-----|------------|------------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | LCS-1 | 206060-2 |
| Date prepared | - | | | 31/01/2018 | 1 | 31/01/2018 | 31/01/2018 | | 31/01/2018 | 31/01/2018 |
| Date analysed | - | | | 31/01/2018 | 1 | 31/01/2018 | 31/01/2018 | | 31/01/2018 | 31/01/2018 |
| Silica | mg/L | 0.2 | METALS-020 | <0.2 | 1 | 28 | 28 | 0 | 106 | 89 |
| Aluminium-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | <0.01 | <0.01 | 0 | 103 | [NT] |
| Antimony-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 99 | [NT] |
| Arsenic-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 102 | [NT] |
| Barium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.10 | 0.10 | 0 | 99 | [NT] |
| Boron-Dissolved | mg/L | 0.02 | METALS-022 | <0.02 | 1 | 0.2 | 0.2 | 0 | 108 | [NT] |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS-022 | <0.0001 | 1 | <0.0001 | <0.0001 | 0 | 102 | [NT] |
| Chromium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 100 | [NT] |
| Cobalt-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 99 | [NT] |
| Copper-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.002 | 0.002 | 0 | 104 | [NT] |
| Iron-Dissolved | mg/L | 0.01 | METALS-022 | <0.01 | 1 | 0.30 | 0.31 | 3 | 103 | [NT] |
| Lead-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 106 | [NT] |
| Manganese-Dissolved | mg/L | 0.005 | METALS-022 | <0.005 | 1 | 0.33 | 0.34 | 3 | 104 | [NT] |
| Mercury-Dissolved | mg/L | 0.00005 | METALS-021 | <0.00005 | 1 | <0.00005 | [NT] | | 110 | [NT] |
| Molybdenum-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 103 | [NT] |
| Nickel-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.001 | 0.001 | 0 | 103 | [NT] |
| Selenium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 103 | [NT] |
| Strontium-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.28 | 0.28 | 0 | 103 | [NT] |
| Tin-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | <0.001 | <0.001 | 0 | 103 | [NT] |
| Zinc-Dissolved | mg/L | 0.001 | METALS-022 | <0.001 | 1 | 0.014 | 0.014 | 0 | 102 | [NT] |

| QUALITY CONTROL: Dissolved Metals in Water | | | | Duplicate | | | Spike Recovery % | | | |
|--|-------|---------|------------|-----------|---|------------|------------------|-----|------|------|
| Test Description | Units | PQL | Method | Blank | # | Base | Dup. | RPD | [NT] | [NT] |
| Date prepared | - | | | [NT] | 4 | 31/01/2018 | 01/02/2018 | | | [NT] |
| Date analysed | - | | | [NT] | 4 | 31/01/2018 | 01/02/2018 | | | [NT] |
| Silica | mg/L | 0.2 | METALS-020 | [NT] | 4 | 3.3 | [NT] | | | [NT] |
| Aluminium-Dissolved | mg/L | 0.01 | METALS-022 | [NT] | 4 | 0.06 | [NT] | | | [NT] |
| Antimony-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Arsenic-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Barium-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | 0.004 | [NT] | | | [NT] |
| Boron-Dissolved | mg/L | 0.02 | METALS-022 | [NT] | 4 | <0.02 | [NT] | | | [NT] |
| Cadmium-Dissolved | mg/L | 0.0001 | METALS-022 | [NT] | 4 | <0.0001 | [NT] | | | [NT] |
| Chromium-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Cobalt-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Copper-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | 0.001 | [NT] | | | [NT] |
| Iron-Dissolved | mg/L | 0.01 | METALS-022 | [NT] | 4 | 0.05 | [NT] | | | [NT] |
| Lead-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Manganese-Dissolved | mg/L | 0.005 | METALS-022 | [NT] | 4 | 0.027 | [NT] | | | [NT] |
| Mercury-Dissolved | mg/L | 0.00005 | METALS-021 | [NT] | 4 | <0.00005 | <0.00005 | 0 | | [NT] |
| Molybdenum-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Nickel-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Selenium-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Strontium-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | 0.015 | [NT] | | | [NT] |
| Tin-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | <0.001 | [NT] | | | [NT] |
| Zinc-Dissolved | mg/L | 0.001 | METALS-022 | [NT] | 4 | 0.005 | [NT] | | | [NT] |

| Result Definiti | Result Definitions | | | | | | |
|-----------------|---|--|--|--|--|--|--|
| NT | Not tested | | | | | | |
| NA | Test not required | | | | | | |
| INS | Insufficient sample for this test | | | | | | |
| PQL | Practical Quantitation Limit | | | | | | |
| < | Less than | | | | | | |
| > | Greater than | | | | | | |
| RPD | Relative Percent Difference | | | | | | |
| LCS | Laboratory Control Sample | | | | | | |
| NS | Not specified | | | | | | |
| NEPM | National Environmental Protection Measure | | | | | | |
| NR | Not Reported | | | | | | |

| | Quality Contro | ol Definitions |
|-----|------------------------------------|--|
| | Blank | This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples. |
| | Duplicate | This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable. |
| | Matrix Spike | A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist. |
| | LCS (Laboratory Control Sample) | This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample. |
| | Surrogate Spike | Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples. |
| - 1 | | |

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

MPL Reference: 206060 Page | 13 of 13 Revision No: R00

Appendix G Numerical Model Summary

Model Setup

Modelling Software and Interface

The numerical groundwater modelling code MODFLOW-2005 using the Upstream Weighting Package (UPW) was used to develop the groundwater flow model for Corunna Downs. The Groundwater Vistas graphical user interface (Version 6.96) was used to develop the model input files and process the model output.

Model Extent and Grid

The model domain has dimensions of 39km (north to south) by 25.4km (east to west), with corner coordinates specified in Table 1

Table 1: Model Extent - Corner Coordinates

| Model Corner | Easting(m) | Northing(m) |
|--------------|------------|-------------|
| North-East | 790138 | 7656963 |
| North-West | 764738 | 7656963 |
| South-West | 764738 | 7617963 |
| South-East | 790138 | 7617963 |

The model grid consists of 3 layers, and 254 columns and has a uniform cell size of 100 by 100m. The model and all associated data have been plotted using the GDA 1994 MGA zone 50 coordinate system.

Model Layer Geometry

The elevation of the top of the uppermost layer, Layer 1, is equal to the ground surface elevation. A summary of model layers is presented in Table 2

Table 2: Model Layer Description

| Model Layer | Thickness (m) | Description |
|-------------|---------------|------------------------|
| 1 | 2 - 220 | Top is ground surface |
| 2 | 3 | Constant 3m thickness |
| 3 | 80 - 211 | Average thickness 113m |

Groundwater Inflow and Outflow

Groundwater Throughflow

The general direction of groundwater flow in the model is from south to north. Groundwater throughflow occurs through three boundaries. Groundwater flows into the model through a constant head boundary in Layer 3 on the southern boundary of the model, representing inflow from fractured bedrock. Groundwater inflow also occurs through a general head boundary along the southeastern boundary in Layer 1 of the model, representing inflow from the alluvium of the Coongan River. Groundwater outflow occurs through a drain boundary on the northern model boundary in Layer 2.

Rainfall Recharge

Apart from groundwater inflow from upstream catchments, all other inflow to the groundwater model is from rainfall recharge. There are two zones of recharge in the model: one covering the area of the Cleaverville Formation and the other covering the remaining model area. Recharge to the Cleaverville

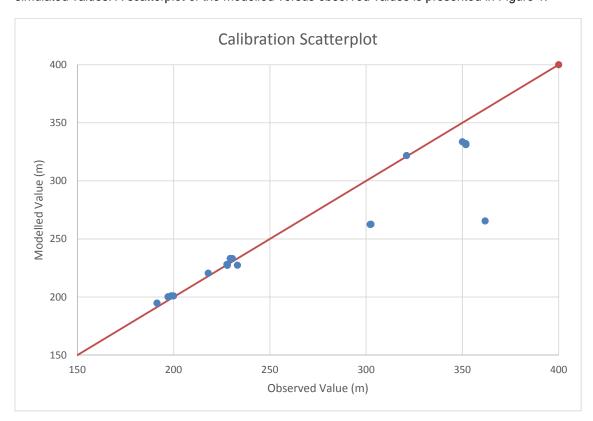
Formation is 9.86x10⁻⁵ m/d and recharge to the rest of the model area is 4.93x10⁻⁵ m/d. The recharge rate is constant throughout the entire simulation period.

Evapotranspiration

Evapotranspiration (ET) is simulated everywhere in the model with a maximum ET rate of 0.005 m/d and an extinction depth of 5m. The ET surface is set equal to the ground surface. The ET setup is the same for the entire simulation period.

Model Calibration

A steady state approach to model calibration was adopted due to a lack of long-term water level monitoring data. The steady state calibration provides a distribution of water levels that reflects the groundwater system prior to any development. The model was calibrated manually, by adjusting the hydraulic conductivity and storage parameters to find a best match between the observed and simulated values. A scatterplot of the modelled versus observed values is presented in Figure 1.



The scaled root mean square (SRMS) is 15.4% and the residual mean is 12.2m.

The calibrated steady state water levels were used as the initial conditions for the prediction model.

Calibrated aquifer parameters are presented in Table 3.

Table 3:Calibrated Aquifer Parameters

| Zone | Kh (m/d) | Kz (m/d) | Ss | Sy | |
|------|----------|----------|---------|-----|--|
| 1 | 1 | 0.01 | 0.00001 | .02 | |
| 2 | 1 | 0.0001 | 0.00001 | .02 | |
| 3 | 1 | 0.01 | 0.00001 | .02 | |
| 4 | 0.0001 | 0.00005 | 0.00001 | .02 | |

| 5 | | 0.01 | 0.001 | 0.00001 | .02 |
|---|--|------|-------|---------|-----|
|---|--|------|-------|---------|-----|

Water Balance

The calibrated steady state water balance is presented in Table 4. The water balance indicates that inflows and outflows are dominated by recharge and evapotranspiration. Evapotranspiration accounts for more than 99% of the outflows from groundwater and recharge for more than 99% of the inflows.

Table 4: Calibrated Steady State Water Balance

| Water Balance Component | Groundwater Inflow (kL/d) | Groundwater Outflow (kL/d) |
|-------------------------|---------------------------|----------------------------|
| General Head Boundary | 290 | 0 |
| Drain | 0 | 142 |
| Constant Head Boundary | 10 | 0 |
| Recharge | 39,502 | 0 |
| Evapotranspiration | 0 | 39,659 |

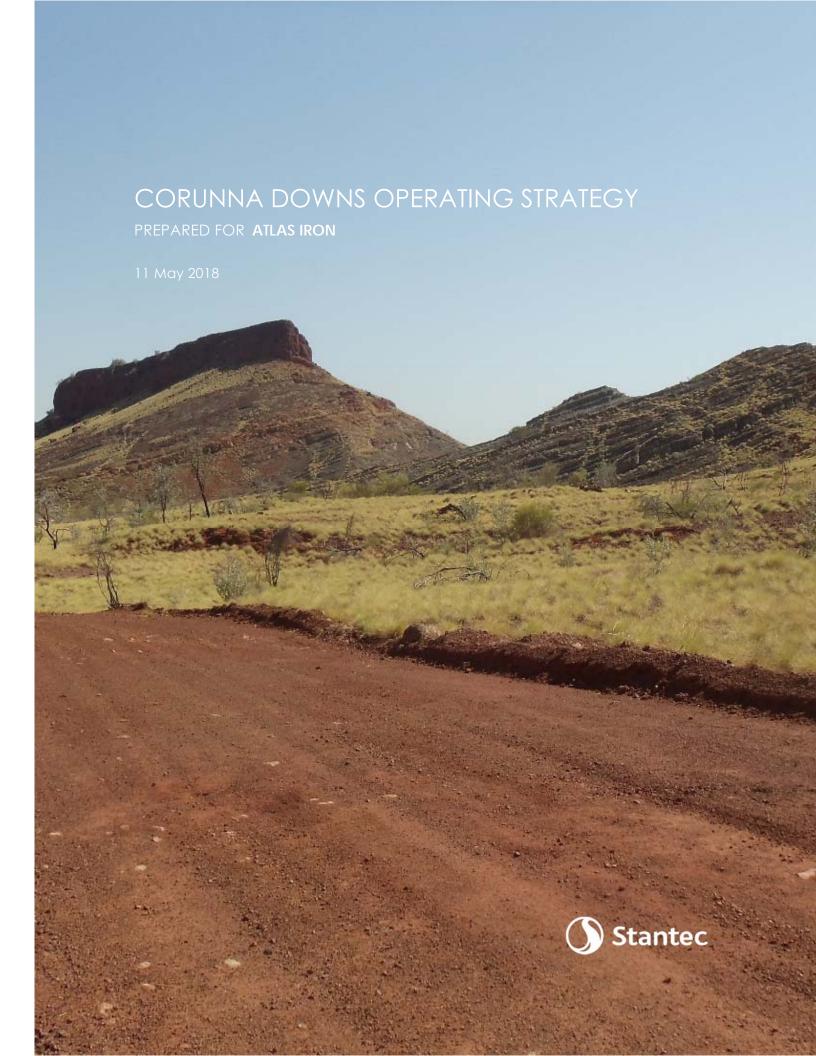
Pumping Prediction

The LOM pumping prediction was implemented using the MNW1 (Multi-Node Well) package. A minimum pumping water level constraint was applied to the pumped wells. If the modelled water level in the casing of a pumped well reaches the minimum level, the pumping rate will be reduced so that the water does not drop below that level. Pumping rates for the LOM prediction are presented in Table 5.

Table 5: Pumping Rates for Life of Mine

| Pumping Bore | Specified Rate | | Modelled Rate | | |
|---------------|----------------|------------|---------------|------------|--|
| | (m³/d) | litres/sec | (m³/d) | litres/sec | |
| CRD71 | 691.2 | 8.0 | 691.2 | 8.0 | |
| CRD74 | 432 | 5.0 | 432 | 5.0 | |
| CRD82 | 432 | 5.0 | 432 | 5.0 | |
| CRD83 | 561.6 | 6.5 | 562 | 6.5 | |
| CRD84 | 259.2 | 3.0 | 259 | 3.0 | |
| CRD85 | 259.2 | 3.0 | 259 | 3.0 | |
| CRD71 | 691.2 | 8.0 | 691.2 | 8.0 | |
| Total Pumping | 2635.2 | 30.5 | 2635.2 | 30.5 | |

Appendix H Operating Strategy



Atlas Iron

Corunna Downs Operating Strategy

CONTENTS

| 1. | INTRODUCTION | 1 |
|--------|--|----|
| 2. | ADMINISTRATIVE REQUIREMENTS | 2 |
| 3. | WATER SOURCE DESCRIPTION | 3 |
| 4. | Water Sources | 3 |
| 4.1 | Groundwater Bores | 3 |
| 4.2 | Proposed Water Distribution Network | 3 |
| 5. | IDENTIFYING AND MANAGING IMPACTS | 5 |
| 5.1 | Other Users | 5 |
| 5.2 | Groundwater Dependent Ecosystems (GDEs) | 5 |
| 6. | OPERATING RULES | 6 |
| 6.1 | Groundwater Production Bores | 6 |
| 7. | MONITORING AND REPORTING | 7 |
| 7.1 | Purpose | 7 |
| 7.2 | Water Use Measurement | 7 |
| 7.3 | Water Level Monitoring | 8 |
| 7.4 | Water Quality Monitoring | 9 |
| 8. | ENVIRONMENTAL IMPACT MONITORING | 9 |
| 9. | CONTINGENCY PROGRAMME | 10 |
| 10. | WATER USE EFFICIENCY | 10 |
| 11. | SUMMARY LIST OF COMMITMENTS | 12 |
| 12. | References | 13 |
| TZI | OF TABLES | |
| | | 2 |
| | 4-1: Summary of Production Bores and Maximum Pumping Rates | |
| | 5-1: Summary of surface water feature details. | |
| | 5-2: Main issues requiring ongoing management | |
| | 5-1: Production Bores Abstraction Details | |
| | 7-1: Water Use Monitoring | |
| | 7-2: Water level monitoring locations and schedule | |
| | 7-3: Water quality monitoring schedule | |
| | P-1: Contingency Plan | |
| able 1 | 1-1: Summary Of Commitments | 12 |

LIST OF FIGURES

| Figure 4-1: Proposed Haul Road Construction Turkeys Nests | |
|---|--|
| Figure 4-2: Proposed Mine Water Circuits | |

APPENDICES

Appendix A Groundwater Licences

1. INTRODUCTION

Atlas Iron Limited (Atlas) are currently undertaking a mining study for their Corunna Downs Project located approximately 237 km by road, southeast of Port Hedland and 33 km south southwest from Marble Bar.

Groundwater abstraction is currently authorised under two 5C licences to take water, GWL184565(1) for 100,000 kL/annum for road construction purposes, and GWL176960(4) for 100,000 kL/annum construction, campsite and potable water supply purposes (Appendix 1). On 21 March 2017, Atlas applied to amend GWL176960, seeking 1,100,000 kL/annum for all mining purposes on the Corunna mining leases. The Department of Water and Environmental Protection (DWER) specified that additional information was required before they could assess the application:

- i. H2 basic hydrogeological assessment including drilling and test pumping
- ii. Groundwater Operating Strategy

This Groundwater Operating Strategy report has been prepared by Stantec on behalf of Atlas, in accordance with the guidelines provided in Operational Policy 5.08¹, and constitutes Item ii of the DWERs request for additional information.

Name of water licence applicant/licensee: Atlas Iron Limited

Name of Development project or purpose: Corunna Downs Project

Legal description and address of land where (a) water is taken, and (b) water is used (if different):

L45/408, G45/339, L45/418, E45/4639, L45/407, M45/1257, L45/410

"I understand that the commitments given in the attached operating strategy will be a condition of an associated water licence if approved and that a breach of a commitment or any licence condition may be an infringement of the Rights in Water and Irrigation Act 1914".

Signatures

| Person legally responsible for water licence | .Date |
|---|-------|
| Printed name: | |
| Approved by delegated authority Department of Water | Date |
| Printed name: | |

¹ Operational policy 5.08 - Use of operating strategies in the water licensing process. Government of Western Australia. Department of Water. June 2011.

2. ADMINISTRATIVE REQUIREMENTS

| Number | Requirement |
|--------|---|
| 1.1 | List any other water licences already issued that are relevant to this operating strategy: |
| | GWL184565(1) for 100,000 kL/annum for road construction purposes, and GWL176960(4) construction, campsite and potable water supply purposes. |
| 1.2 | Does the water licence involve a staged development? |
| | No staged development. Average monthly water demand is anticipated to be consistent upon commencement of ore processing. |
| 1.3 | Has there been any investigation and reporting on the water source and/or environment involving the development?: - YES |
| | Stantec 2018a: Corunna Downs Project Hydrogeological Investigation. Unpublished Report prepared for Atlas Iron. |
| | Stantec 2018b: Corunna Downs Project H2 Basic Hydrogeological Assessment. Unpublished Report prepared for Atlas Iron |
| | WEC, (2018a) Corunna Downs Project – Assessment of Groundwater Drawdown Impacts to Vegetation. Unpublished report prepared for Atlas Iron Limited. May, 2018 |
| 1.4 | Is the development within an area covered by a DoW water resource management/allocation plan? |
| | No. |
| 1.5 | Person responsible for implementing the Operating Strategy: |
| | Corunna Registered Manager |
| | Telephone: 08 6228 8000, 300 Murry Street, PERTH WA 6000 |
| | PO Box 7071, Cloisters Square PO, WA 6850 |
| 1.6 | Reporting dates: |
| | Water use metering data - by 30 September every year. Operating strategy compliance report - by 30 September every year. |
| | The "Water Year" is defined as the 12 month period commencing from the last day of the month in which the water license was issued. For the previous GWL the Water Year was from 29 May to 28 May [sic] |
| 1.7 | Date of major review of the Operating Strategy - three months prior to the expiry date on the water license. |

WATER SOURCE DESCRIPTION

Water demand for the Project is proposed to be sourced from groundwater production bores drawing water from the fractured rock aquifer comprised predominantly within weathered to fresh basalt.

Groundwater quality at Corunna is classified as fresh to brackish (TDS <2 000 mg/L) according to Department of Water Operational Policy 5.08.

4. Water Sources

4.1 Groundwater Bores

The existing groundwater supply wells at Corunna are listed in Table 4-1. Potable water supplies for the camp are likely to be sourced from some of these bores.

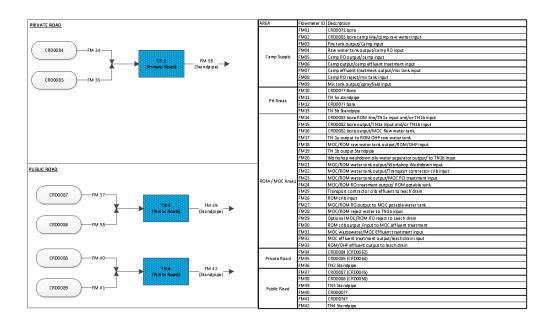
Table 4-1: Summary of Production Bores and Maximum Pumping Rates

| Bore ID | Easting | Northing | Drilled Depth (m) | Screen (mbgl) | CRT Pumping Rate (L/s) | Proposed Maximum Pumping Rate (L/s) |
|---------|---------|----------|-------------------------|------------------|---------------------------------|--|
| CRD0007 | TBA | TBA | | | | |
| CRD0071 | 778429 | 7633394 | 96 | 10 - 96 | 24.0 | 8.0 |
| CRD0074 | TBA | TBA | | | | 5.0 |
| CRD0082 | 778953 | 7631289 | 88 | 10 to 88 | 25.0 | 8.0 |
| CRD0083 | 778579 | 7632984 | 82 | 6 to 78 | 20.0 | 8.0 |
| CRD0084 | 778981 | 7641952 | 64 | 6 to 60 | 6.0 | 5.0 |
| CRD0085 | 780809 | 7642040 | 64 | 6 to 64 | 5.0 | 4.0 |
| CRD0086 | 782443 | 7644390 | 70 | 4 to 70 | 4.0 | 3.0 |
| CRD0087 | 781895 | 7645717 | 64 | 4 to 64 | 15.0 | 8.0 |
| CRD0088 | 782285 | 7652335 | 102 | 9 to 99 | 12.0 | 8.0 |
| CRD0089 | 782719 | 7652280 | 100 | 12 to 96 | 12.0 | 8.0 |

4.2 Proposed Water Distribution Network

The proposed water distribution network comprises the utilisation of a series Turkeys Nests (TN) located as follows:

- TN's associated with haul road construction, two located along the along the public road section of the haul road alignment (Section 91 Licence area), with water sourced from production bores CRD0086 and CRD0087 supplying TN3, and CRD0088 and CRD0089 supplying TN4 (Figure 4-1);
- One TN (TN2) supplied by CRD0084 and CRD0085 (Figure 4-1);
- Two TNs (TN's 5a and 5b) located in the pit areas source production bores yet to be identified (Figure 4-2); and
- Two TNs (TN's 1a and 1b) located in the ROM/MOC area, sourced from CRD0083 and CRD0084 (Figure 4-2).



02/05/2018

Figure 4-1: Proposed Haul Road Construction Turkeys Nests

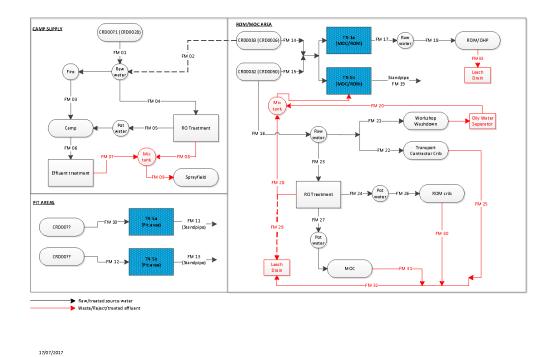


Figure 4-2: Proposed Mine Water Circuits

5. IDENTIFYING AND MANAGING IMPACTS

There are two water supply components, water supply for haul road construction, and water supply for the mining operations.

5.1 Other Users

No other groundwater users are likely to be affected by abstraction activities at Corunna.

5.2 Groundwater Dependent Ecosystems (GDEs)

Eleven (11) small permanent or ephemeral pools have been identified in the upper (southern) reaches of the catchment, in the vicinity of the proposed mining areas (Table 5-1). Four of the features have been identified as likely to be supported to some extent by groundwater contributions.

Abstraction for road construction activities is unlikely to impact upon the pools, however operational abstraction for the mining operations will likely impact upon the pools and they will require monitoring for the duration of abstraction.

The operational raw water requirements have been numerically modelled for the life of mine (LOM). The maximum drawdowns indicated by the modelling are shown on Table 5-1 results at specified time steps for each of the key environmental features. Four of the pools CO-WS's 3, 5, 8, and 13 were identified as having drawdowns of over 1 m after a year of abstraction at 30.5 L/s. By the end of mining the model indicated that these same features had been impacted between 2.3 and 3.73 m.

Table 5-1: Summary of surface water feature details.

| Location ID | Easting | Northing | Elevation (mAHD) | TDS (mg/L) | Groundwater Source | Modelled Drawdown at LOM (m) |
|-------------|----------|----------|---------------------|------------|-----------------------|------------------------------------|
| CO-WS-01 | 778586 | 7630030 | 255.627 | 210 | Likely | 0.02 |
| CO-WS-02 | 776034 | 7620690 | 371.100 | No sample | Unlikely | 0.56 |
| CO-WS-03 | 778506 | 7633950 | 227.531 | 180 | Unlikely (dry) | 2.30 |
| CO-WS-05 | 773504 | 7623870 | 313.184 | 690 | Likely | 3.52 |
| CO-WS-08 | 774961 | 7625570 | 321.721 | 510 | Unlikely | 3.31 |
| CO-WS-09 | 776568 | 7622980 | 344.725 | 2800 | Unlikely (dry) | 0.11 |
| CO-WS-10 | 777461 | 7629400 | 297.225 | No sample | Unlikely | 0.02 |
| CO-WS-11 | 777517 | 7626870 | 398.728 | 33 | Unlikely | 0.29 |
| CO-WS-12 | 777092.2 | 7629040 | 373.970 | 100 | Likely | 0.05 |
| CO-WS-13 | 777092 | 7629040 | 327.170 | 550 | Unlikely | 3.73 |
| CO-WS-14 | 774623 | 7623940 | 320.990 | 190-210 | Likely | 0.10 |

Notes: Coordinates are GDA94

The main issues identified as requiring ongoing management are summarised in Table 5-2.

Table 5-2: Main issues requiring ongoing management

| Issue | Management Objective | Measurement | Management Response |
|---|--|---|---|
| Groundwater Levels – Surface Water Features and Groundwater Dependant Vegetation (GDV). | Ensuring that the lowering of groundwater levels does not impact vegetation communities. | Monitor standing water levels monthly to ensure that water level does not drop significantly (>0.25 m) over life of mine. | If a significant change in water level is identified, review abstraction rates and use. Consider alternative water supply sources and increase in frequency of monitoring. |
| Groundwater Levels – Underestimation of drawdown on the local aquifer. | Ensuring that the lowering of groundwater levels does not impact upon bore yield. | Monitor standing water levels monthly to ensure that water level does not drop below primary aquifer zone/3 m above pump placement between monitoring events. | Do not exceed maximum pumping rates for individual bores. If water levels drop to within 3 m of pump placement, review abstraction rates and use. Consider resting individual bore and/or use of alternative sources. |
| Reliable water supply - Reduced bore yields. | Ensure water use does not exceed annual allocation. | Water meters installed and recorded monthly. | Review process and investigate options to reduce demand. Review licence abstraction limits and amend licence if required. |
| Groundwater salinity at production bores - Degradation of groundwater quality. | Maintain salinity (TDS) concentrations below 5 000 mg/L. | Monthly field pH and EC test. Ensuring results do not exceed 5 000 mg/L. | Review results and if bores are indicating an increase over a period of time, investigate options to reduce demand at a single bore and bring alternative bores online. |
| Reliable water supply - Mine footprint limits further water exploration. | Ensure water use does not exceed annual allocation. | Abstraction impact monitoring, all monitoring criteria. | Identify alternative supply options. |

6. OPERATING RULES

6.1 Groundwater Production Bores

Existing groundwater supply production bores at Corunna are listed in Table 6-1. Additional production bores may be drilled in the pit areas when operations commence, and the Operating Strategy will then be updated to reflect these additions.

Table 6-1: Production Bores Abstraction Details

| Bore ID | Proposed Maximum Abstraction Rate (L/s) | Estimated Annual Abstraction (kL/year) | Operating Protocol | Abstraction Strategy |
|---------|--|--|-----------------------|-------------------------|
| CRD0007 | tba | | Backup Bore | Demand basis |
| CRD0071 | 8.0 | 252,300 | Primary Bore | Demand basis |

| Bore ID | Proposed Maximum Abstraction Rate (L/s) | Estimated Annual Abstraction (kL/year) | Operating Protocol | Abstraction Strategy |
|---------|--|--|-----------------------|-------------------------|
| CRD0074 | 5.0 | 157,700 | Primary Bore | Demand basis |
| CRD0082 | 8.0 | 157,700 | Primary Bore | Demand basis |
| CRD0083 | 8.0 | 205,000 | Primary Bore | Demand basis |
| CRD0084 | 5.0 | 94600 | Primary Bore | Demand basis |
| CRD0085 | 4.0 | 94600 | Primary Bore | Demand basis |
| CRD0086 | 3.0 | 21000 | | |
| CRD0087 | 8.0 | 21000 | Road construction | n water supply bores |
| CRD0088 | 8.0 | 21000 | only | |
| CRD0089 | 8.0 | 21000 | | |

MONITORING AND REPORTING

7.1 Purpose

The purpose of the monitoring programme is to obtain regular measurements of water use and basic groundwater chemistry parameters in order to provide comparison with baseline data, to assess whether the allocation has been exceeded, and to ensure that water use conforms to licensed conditions.

The "Water Year" is considered to be the period 1 July to 30 June for each year of operation.

One hard copy and one electronic copy of the 'annual groundwater monitoring summary' (in accordance with Operational Policy 5.12) will be submitted to DoW by 30 September for each year of operation.

All data will be supplied in graphical and tabular form (raw data).

A groundwater monitoring review is due every 3 years, the first one being 30 September 2021.

7.2 Water Use Measurement

Mechanical flow meters will be used to measure the water use for the project. Flow meters are proposed for installation at the locations shown on Figure 4-1 and Figure 4-2. Meter details will be provided to DWER in the annual groundwater monitoring summary, in the format presented in Table 7-1. Instantaneous flow rates and cumulative volumes will be recorded.

Table 7-1: Water Use Monitoring

| Draw Point | Site Meter Number | Meter type/Serial No. | Meter Maintenance Calibration Schedule | Frequency of Recording Meter Data |
|------------|-------------------|--------------------------|--|---|
| CRD0007 | | | | |
| CRD0071 | | | | Daily while |
| CRD0074 | | | | operational, |
| CRD0082 | | | | otherwise |
| CRD0083 | | | | weekly. |
| CRD0084 | | | | |

| Draw Point | Site Meter Number | Meter type/Serial No. | Meter Maintenance Calibration Schedule | Frequency of Recording Meter Data |
|------------|-------------------|--------------------------|--|---|
| CRD0085 | | | | |
| CRD0086 | | | | |
| CRD0087 | | | | |
| CRD0088 | | | | |
| CRD0089 | | | | |

Note: *Flowmeter serial numbers, calibration certificates and initial reading will be provided in the first annual monitoring report. If and when additional draw points are added to the water distribution system, this table will be updated.

7.3 Water Level Monitoring

Water level monitoring will be carried out according to the schedule shown in Table 7-2. Where automatic water level recorders with data loggers have been installed, they will be monitored quarterly.

Table 7-2: Water level monitoring locations and schedule

| Location ID | Location Type | Easting | Northing | Monitoring Frequency |
|-------------|-----------------|---------|----------|-------------------------|
| CRD0007 | Production bore | TBA | TBA | Weekly |
| CRD0071 | Production bore | 778429 | 7633394 | Weekly |
| CRD0074 | Production bore | TBA | TBA | Weekly |
| CRD0082 | Production bore | 778953 | 7631289 | Weekly |
| CRD0083 | Production bore | 778579 | 7632984 | Weekly |
| CRD0084 | Production bore | 778981 | 7641952 | Weekly |
| CRD0085 | Production bore | 780809 | 7642040 | Weekly |
| CRD0086 | Production bore | 782443 | 7644390 | Weekly |
| CRD0087 | Production bore | 781895 | 7645717 | Weekly |
| CRD0088 | Production bore | 782285 | 7652335 | Weekly |
| CRD0089 | Production bore | 782719 | 7652280 | Weekly |
| CRD0001 | Monitoring bore | 776154 | 7623040 | Monthly |
| CRD0003 | Monitoring bore | 776206 | 7623203 | Monthly |
| CRD0016 | Monitoring bore | 773188 | 7624729 | Monthly |
| CRD0017 | Monitoring bore | 777072 | 7627229 | Monthly |
| CRD0018 | Monitoring bore | 777239 | 7627895 | Monthly |
| CRD0021 | Monitoring bore | 776799 | 7625367 | Monthly |
| CRD0022 | Monitoring bore | 776585 | 7626361 | Monthly |
| CRD0023 | Monitoring bore | 777193 | 7626328 | Monthly |
| CRD0026 | Monitoring bore | 778568 | 7632991 | Monthly |
| CRD0027 | Monitoring bore | 779018 | 7634054 | Monthly |
| CRD0028 | Monitoring bore | 778440 | 7633400 | Monthly |
| CRD0031 | Monitoring bore | 776754 | 7625643 | Monthly |
| CRD0033 | Monitoring bore | 776182 | 7623126 | Monthly |
| CRD0039 | Monitoring bore | 782368 | 7652870 | Monthly |
| CRD0043 | Monitoring bore | 782275 | 7652340 | Monthly |

| Location ID | Location Type | Easting | Northing | Monitoring Frequency |
|-------------|-----------------|---------|----------|-------------------------|
| CRD0044 | Monitoring bore | 782273 | 7645380 | Monthly |
| CRD0045 | Monitoring bore | 781895 | 7645717 | Monthly |
| CRD0050 | Monitoring bore | 778959 | 7631281 | Monthly |
| CRD0056 | Monitoring bore | 782732 | 7652279 | Monthly |
| CRD0058 | Monitoring bore | 782443 | 7644390 | Monthly |
| CRD0062 | Monitoring bore | 778987 | 7641946 | Monthly |
| CRD0064 | Monitoring bore | 780813 | 7642048 | Monthly |
| CRD0075 | Monitoring bore | 778427 | 7633388 | Monthly |
| CO-WS-01 | Surface Pond | 778586 | 7630030 | Monthly |
| CO-WS-05 | Surface Pond | 773504 | 7623870 | Monthly |
| CO-WS-08 | Surface Pond | 774961 | 7625570 | Monthly |
| CO-WS-10 | Surface Pond | 777461 | 7629400 | Monthly |
| CO-WS-12 | Surface Pond | 777092 | 7629040 | Monthly |
| CO-WS-13 | Surface Pond | 777092 | 7629040 | Monthly |
| CO-WS-14 | Surface Pond | 774623 | 7623940 | Monthly |

7.4 Water Quality Monitoring

The water quality monitoring schedule is presented on Table 7-3.

Table 7-3: Water quality monitoring schedule

| Location | Frequency | Type of monitoring | Parameters |
|------------------|-----------|---------------------|---|
| Production bores | Weekly | Field measurements | Water LevelsSalinitypHTemperature |
| | Quarterly | Laboratory testing* | Major ionsMetalsTotal Petroleum HydrocarbonsTotal Suspended Solids |
| Monitoring Bores | Monthly | Field measurements | As for production bores |
| | Annually | Laboratory testing | As for production bores |
| Surface water | Monthly | Field measurements | As for production bores |
| values | | Laboratory testing | As for production bores (excluding hydrocarbons for surface water sites) |

Notes: *Laboratory tested of the Comprehensive Analytical Suite (Operational policy no. 5.12, ApendixC4)

8. ENVIRONMENTAL IMPACT MONITORING

Proposed environmental impact monitoring methodology is presented for assessment within the Mining Proposal submission to the Department of Mines, Industry Regulation and Safety. Within this submission,

Atlas has proposed a number of monitoring schedules and performance criteria (triggers) for groundwater monitoring for the GDE's and groundwater dependant vegetation (Atlas, 2018).

Atlas will comply with the groundwater abstraction licence conditions (RIWI Act 1914) and ensure that adequate mitigation measures are employed to demonstrate achievement of the final environmental outcomes and performance criteria outlined within the Mining Proposal, assessed under delegation of the Environmental Protection Act 1986 and approved in accordance with the Mining Act 1978. (

CONTINGENCY PROGRAMME

The project risks identified in Table 5-2 have been assessed in the context of contingency measures to ameliorate the risks. These measures are summarised in Table 10-1.

10. WATER USE EFFICIENCY

It will be to Atlas's benefit that an efficient water use practice is set up and maintained during the project, as environmental effects can be minimised and potential cost savings can be realised. In this regard, Atlas will implement inspection and maintenance systems aimed at ensuring that water use on-site is monitored, and issues identified that may result in more efficient water use.

Table 10-1: Contingency Plan

| Risk Consideration | Reasoning | Contingency Measure |
|--|--|---|
| Groundwater Levels – Surface Water Features and GDV. | Fractured rock aquifer performance is extremely difficult to characterise without long term operational monitoring data. Episodic climatic factors (rainfall) have a significant influence upon the extent of drawdown impacts on surface water features and GDV. | If a significant change in water level is identified, review abstraction rates and use, and cease abstraction from proximal water supply bores and use alternative bores. Consider increasing frequency of monitoring |
| Groundwater Levels – Underestimation of drawdown on the local aquifer | Fractured rock aquifer performance is extremely difficult to characterise without long term operational monitoring data. | Prior to finalising Site Water Operating Plan review drawdown assessment in consideration of completed drilling and testing program. Alternative/additional supply bores may need to be constructed |
| Reliable water supply - Reduced bore yields | | and reticulated to meet demand should dewatering reduce the local aquifer viability, degrade groundwater quality or adversely |
| Groundwater salinity at production bores - Degradation of groundwater quality. | | impact surface water values. Target areas will be identified for future potential water exploration within the mine approvals footprint. |
| Reliable water supply - Mine footprint limits further water exploration. | | |
| Water meter failure. Monitoring and reporting commitments cannot be met. | Mechanical failure is common. | Keep at least one spare, calibrated water meter on site at all times. Inspect meters monthly. Inform DoW if a meter failure occurs and if a reporting commitment cannot be met. |
| | Groundwater Levels – Surface Water Features and GDV. Groundwater Levels – Underestimation of drawdown on the local aquifer Reliable water supply - Reduced bore yields Groundwater salinity at production bores - Degradation of groundwater quality. Reliable water supply - Mine footprint limits further water exploration. Water meter failure. Monitoring and reporting commitments | Groundwater Levels – Surface Water Features and GDV. Fractured rock aquifer performance is extremely difficult to characterise without long term operational monitoring data. Episodic climatic factors (rainfall) have a significant influence upon the extent of drawdown impacts on surface water features and GDV. Groundwater Levels – Underestimation of drawdown on the local aquifer Reliable water supply - Reduced bore yields Groundwater salinity at production bores - Degradation of groundwater quality. Reliable water supply - Mine footprint limits further water exploration. Water meter failure. Monitoring and reporting commitments Fractured rock aquifer performance is extremely difficult to characterise without long term operational monitoring data. Mechanical failure is common. |

11. SUMMARY LIST OF COMMITMENTS

The licensee will comply with this operating strategy as a condition of the Licence to Take Water, Instrument No. **GWL176960** for the taking of water from the Pilbara Water Region, at the Corunna Project.

The licensee will carry out and report to the department on the monitoring programme summarised in Table 11-1

Table 11-1: Summary Of Commitments

| Location | Frequency | Type of monitoring | Parameters |
|------------------|-----------|---------------------|--|
| Production bores | Weekly | Field measurements | Water LevelsSalinitypHTemperature |
| | Quarterly | Laboratory testing* | Major ions Metals Total Petroleum Hydrocarbons Total Suspended Solids |
| Flow meters | Daily | Reading | Volume (kL) instantaneous and cumulative |
| Monitoring Bores | Monthly | Field measurements | As for production bores |
| | Annually | Laboratory testing | As for production bores |
| Surface water | Monthly | Field measurements | As for production bores |
| values | | Laboratory testing | As for production bores (excluding hydrocarbons for surface water sites) |

Notes: *Laboratory tested of the Comprehensive Analytical Suite (Operational policy no. 5.12, ApendixC4)

New bore details, locations and meter information will be supplied in the annual compliance report each year.

The licensee shall inform the DWER of any likely breach in the commitment of this operating strategy within 14 days of the licensee being aware of the possible breach. This also includes the implementation of a contingency response.

An annual water use (metering) report and the compliance (monitoring) report will be submitted by 30 September each year, respectively, in formats described in DoW (2009).

12. References

The following references were used during preparation of the Operating Strategy:

Atlas, 2018: Corunna Downs Hydrogeological Summary (pre-print)

DoW, 2009: Strategic policy 5.03: Metering the taking of water. June 2009. Government of Western Australia. Department of Water.

DoW, 2011: Operational policy 5.08 - Use of operating strategies in the water licensing process. Government of Western Australia, Department of Water. June 2011.

DoW 2009: Operational policy 5.12: Hydrogeological reporting associated with a groundwater well licence.

Golder Associates, 2010: *Corunna Downs Field Survey Report*. Unpublished report (087641274-004-R-Rev3), prepared for Gondwana Resources Ltd, February 2010.

Stantec 2018a: Corunna Downs Project, Hydrogeological Investigation, prepared for Atlas Iron

WEC, (2018a) Corunna Downs Project – Assessment of Groundwater Drawdown Impacts to Vegetation. Unpublished report prepared for Atlas Iron Limited. May, 2018.

WEC, (2018b). Corunna Downs Project, Investigation of Relationships Between Vegetation and Hydrology – "Soak" Area. Unpublished report prepared for Atlas Iron Limited, Perth, WA.



Appendix A Groundwater Licences



Your Ref: App13211
Our ref: RF10954; wrd352780
Enq@iries@ncStephanie*Phamia's water future
(08) 6364 6874

Corunna Downs

David Nyquest Atlas Iron PO Box 7071 Cloisters Square WA 6850

Dear David,

Re: Issue of a licence under the Rights in Water and Irrigation Act 1914

Property: L45/408, G45/339, L45/418, E45/4639, L45/407, M45/1257, L45/410 - Corunna Downs Project

Please find enclosed your licence to take groundwater - GWL176960(4).

Please take time to read this document as it contains important information about your rights and responsibilities.

In addition, please note the following:

There are Clearing Regulations Schedule 1 Areas within the tenements. Please be advised that if you wish to undertake any clearing of vegetation within these areas you will need to do so in consultation with the Department of Environment Regulation (DER). Please contact the DER on (08) 6467 5000 for further information.

If you have any queries about this matter please contact Stephanie Pham on (08) 6364 6874.

Yours sincerely,

Kevin Hopkinson

Program Manager - Pilbara District

North West Region Department of Water

Kein Herboron

29 May 2017

Page 1 of 1
Instrument No. GWL176960(4)

LICENCE TO TAKE WATER

Granted by the Minister under section 5C of the Rights in Water and Irrigation Act 1914

| Licensee(s) | Atlas Iron Limited | | | |
|----------------------------------|--|---|-----------------|--|
| Description of Water Resource | Pilbara Pilbara - Fractured Rock | Annual Water 100000 kL Entitlement | | |
| Location of Water Source | L45/408, G45/339, L45/418, L45 | L45/408, G45/339, L45/418, L45/410, L45/407, M45/1257, E45/4639 | | |
| Authorised Activities | Taking of water for | Taking of water for Location of Activity | | |
| | Dust suppression for earthworks and construction purposes Exploratory drilling operations General campsite purposes Potable Water Supply purposes Road construction purposes Road maintenance purposes | L45/408, G45/339, L45/418, L M45/1257, E45/4639 | 45/410, L45/407 | |
| Duration of Licence | From 29 May 2017 to 28 May 2027 | | | |



Your Ref: App13998
Our ref: RF10954; wrd358426
Enquiries: Stephanie Phan
(08) 6364 6874
Securing Western Australia's water future

David Nyquest Atlas Iron PO Box 7071 Cloisters Square WA 6850

Dear David,

Re: Issue of a licence under the Rights in Water and Irrigation Act 1914

Property: Section 91 Lic 869-2016_A6435862 - Corunna Downs Project

Please find enclosed your licence to take groundwater – GWL184565.

Please take time to read this document as it contains important information about your rights and responsibilities.

In addition, please note the following:

There are registered sites of Aboriginal Heritage Significance within the project area. Please be advised that it is your responsibility to ensure appropriate consultation with any affected Traditional Owners and adequate referral to the Department of Aboriginal Affairs (DAA) is made, to ensure full compliance with the *Aboriginal Heritage Act 1972*.

Clearing Regulations Schedule 1 Areas are within your project area. Please be advised that if you wish to undertake any clearing of vegetation within these areas you will need to do so in consultation with the Department of Environment Regulation (DER). Please contact the DER on (08) 6467 5000 for further information.

Contaminated site ID1335 near Halse Road/Limestone Marble Bar Road has been identified as near or within your project area. The site is listed as "possibly contaminated – investigation required" under the Department of Environment Regulation (DER) contaminated sites classification system. Please consult the DER for additional information and advice and/or any relevant approvals. The DER Contaminated Sites hotline number is 1300 762 982.

Priority fauna are located within the project area. If you have any queries, please contact the Department of Parks and Wildlife's Species and Communities Branch on (08) 9219 9511 for further information.

The Marble Bar Water Reserve was proclaimed in 1972 under the Country Areas Water Supply Act 1947 (CAWS).

A Drinking Water Source Protection Plan was prepared for the Marble Bar Water Reserve in 2000, and updated in 2010. Groundwater is drawn from the Coongan well-field 2-3km west of the town and adjacent to the Coongan River. The Coongan wellfield draws from fractured volcanic rock on the Coongan Rivers eastern bank. Significant recharge occurs during high rainfall events and the direction of groundwater flow is closely related to surface drainage, in a north to north westerly direction.

Given the unconfined nature of the aquifer, it is vulnerable to contamination. Land and water based uses and activities within the catchment can directly affect water quality and treatment. It should be noted that protecting a drinking water supply to provide a safe drinking water source is a cheaper option than both treatment and remediation; furthermore treatment is not 100% reliable.

It is therefore important to ensure any bores are appropriately located to avoid drawdown and constructed to prevent contamination of the public drinking water source. All bores should be constructed in accordance with *Minimum construction requirements for water bores in Australia* (National Minimum Bore Specifications Committee 2003).

Existing and future mining proposals within the water reserve are compatible with conditions, and should adhere to the Department of Water's *Water Quality Protection Guidelines for Mining and Mineral Processing 1-11* and other relevant Water Quality Protection Notes published by the Department of Water

If you have any queries about this matter please contact Stephanie Pham on (08) 6364 6874.

Yours sincerely,

Kevin Hopkinson

Program Manager – Pilbara District

North West Region Department of Water

Kein Heron

30 May 2017



Page 1 of 1
Instrument No. GWL184565(1)

LICENCE TO TAKE WATER

Granted by the Minister under section 5C of the Rights in Water and Irrigation Act 1914

| Licensee(s) | Atlas Iron Limited | | | | |
|----------------------------------|--|--|--|--|--|
| Description of Water Resource | Pilbara Annual Water Pilbara - Fractured Rock Entitlement 100000 kL | | | | |
| Location of Water Source | f Water Source Section 91 of the LAA Lic 00869-2016_A6435862 | | | | |
| Authorised Activities | Taking of water for | st suppression for earthworks d construction purposes ploratory drilling operations ad construction purposes | | | |
| | Dust suppression for earthworks and construction purposes Exploratory drilling operations Road construction purposes Road maintenance purposes | | | | |
| Duration of Licence | From 31 May 2017 to 31 January | 2019 | | | |

This Licence is granted subject to the Rights in Water and Irrigation Regulations 2000

Perth

41 Bishop Street, JOLIMONT, WA 6014 Tel +61 (08) 9388 8799

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