

## Appendix E Noise Studies

Appendix E1 Acoustical Assessment Roe Highway Stage 7 South Street to Kwinana Freeway-

Herring Storer Acoustics

Appendix E2 Roe Hwy – Stage 7 Traffic Noise – Barrier Design – Vipac

Rochdale Holdings Pty Ltd A B N 85 009 049 067 trading as:

## **HERRING STORER ACOUSTICS**

Suite 34, 11 Preston Street, Como, W.A. 6152 P.O. Box 219, Como, W.A. 6952

Telephone: (08) 9367 6200 Facsimile: (08) 9474 2579

Email: hsa@hsacoustics.com.au



The transfer of the

## **ACOUSTICAL ASSESSMENT**

# ROE HIGHWAY STAGE 7 SOUTH STREET TO KWINANA FREEWAY

BY

HERRING STORER ACOUSTICS

**AUGUST 2003** 

OUR REF: 1763-2-03107-1-2





#### **CONTENTS**

- 1.0 INTRODUCTION
- 2.0 SUMMARY
- 3.0 METHODOLOGY
- 4.0 CRITERIA
- 5.0 RESULTS

#### **APPENDICES**

- A General Locality Map
- B Noise Monitoring Results
- C Predicted Noise Levels to Residences Single Point Calculations
- D Predicted 2031 Noise Levels to Surrounding Areas Noise Level Contour Plots: Existing Fences
- E Minimum Recommended Noise Walls
- F Predicted 2031 Noise Levels to Surrounding Areas Noise Level Contour Plots: Recommended Noise Walls
- G Predicted 2031 Noise Levels to Surrounding Areas Noise Level Contour Plots: 4 Metre High Noise Walls
- H Traffic Flow Information

#### 1.0 INTRODUCTION

Herring Storer Acoustics (HSA) was commissioned by Gutteridge Haskins & Davey (GHD) to undertake an acoustic assessment for the proposed Roe Highway Stage 7, between South Street and the Kwinana Freeway. Preliminary work was previously undertaken by ERM Mitchell McCotter Pty Ltd (Roe Highway Project Stage 7, Noise Impact Assessment Report; June 1999, Ref: 28024), which measured the existing noise levels at residences adjacent the route and nominated suitable noise control in the form of noise barrier walls, in order to satisfy the nominated criteria. Since this time, the predicted traffic volumes have changed as well as the assessment criteria. As such, the work undertaken in the ERM report is no longer relevant, hence the purpose of this assessment.

#### The study involved the following:

- 1. A review of the ERM report, particularly the noise data logging, as these may still be relevant. However, the future predicted noise levels would be irrelevant due to new information.
- 2. Where necessary, repeat the noise monitoring at residences and/or measure the noise levels at other relevant locations. Note that the noise monitoring is required so as to obtain baseline noise levels and hence, establish the appropriate criteria, since this dependent upon the existing noise levels.
- 3. Construction of a digital model of the route for incorporation into the computer modelling programme SoundPlan 5.6 (Main Roads Western Australia (MRWA) supplied the proposed road design, existing ground contours and cadastral data).
- 4. Calculation of the noise propagation for the relative lines of traffic for the Years 2011 and 2031 as per the existing situation (proposed design, existing fences etc). This included both noise contour plots and single point calculations to specific residences.
- 5. Where exceedances to the criteria are apparent, determine suitable noise control to satisfy the criteria.
- 6. Recalculation of the noise propagation for the relative lines of traffic for the Years 2011 and 2031 based on the recommended noise walls.
- 7. Calculate the noise levels based on 4 metre high walls (considered by MRWA to be the maximum practicable height) for the length of the road.

A plan of the area of interest is contained within Appendix A. Residences of concern are located on the northern side of the Highway only, in the suburb of Leeming, with industrial, airport and park land being to the south of the road.

#### 2.0 <u>SUMMARY</u>

The criteria to be satisfied at residences are:

63 dB(A) L<sub>10(18hour)</sub><sup>1</sup> and 55 dB(A) L<sub>eq(8hour)</sub><sup>2</sup> where the existing noise level is less than 60 dB(A) L<sub>10(18hour)</sub> and 52 dB(A) L<sub>eq(8hour)</sub> or;

 The existing noise level + 3 dB(A) where the existing noise level is more than 60 dB(A) L<sub>10(18hour)</sub> and 52 dB(A) L<sub>eq(8hour)</sub>.

These criteria apply at 1 metre from a dwelling and to the ground floor only, due to the impracticality of controlling noise at upper floors.

All residences in this area have been determined to have an existing  $L_{10(18hour)}$  that is less than 60 dB(A) and/or an existing  $L_{eq(8hour)}$  that is less than 52 dB(A), such that the criteria to be met from Roe Highway is 63 dB(A)  $L_{10(18hour)}$  and 55 dB(A)  $L_{eq(8hour)}$ .

Data including traffic volumes, percentage heavy vehicles, speed, road surface etc were incorporated into the computer programme SoundPlan 5.6. This programme enables the user to select a number of algorithms to predict the noise level propagation. In accordance with MRWA requirements, the *Calculation of Road Traffic Noise* (CoRTN) algorithms were selected.

From the information provided, it was calculated that the  $L_{10(18hour)}$  noise levels would be the more critical. This is because the  $L_{eq(8hour)}$  was calculated to be 8.5 dB(A) less than the  $L_{10(18hour)}$  whereas the difference in the criteria is only 8.0 dB(A). For example, if the predicted  $L_{10(18hour)}$  is 63 dB(A), the  $L_{eq(8hour)}$  would be 54.5 dB(A). Hence, it is the former parameter that determines the noise control requirements.

Noise levels were predicted at each residence immediately adjacent the Highway for the Years 2011 and 2031 based on the residences existing fences. A summary of these calculations is shown in Appendices C & D as single point and noise contour calculations respectively. In 2011, the highest predicted level is 67.3 dB(A)  $L_{10(18hour)}$  (4.3 dB(A) exceedance) and in 2031, the highest predicted level is 69.1 dB(A)  $L_{10(18hour)}$  (6.1 dB(A) exceedance). The 63 dB(A)  $L_{10(18hour)}$  criterion in 2031 is predicted to be exceeded at the majority of residences between Green Croft Gardens to Merrifield Circle, east of the Kwinana Freeway and between Stone Court and Tetlow Place, southwest of the Kwinana Freeway.

As exceedances were determined, noise controls were considered. The recommended noise control is shown in Appendix E with the resultant noise levels shown in Appendices C & F. Furthermore, as requested by MRWA, consideration was also given to constructing 4-metre high noise walls for the length of the project to reduce the noise levels as far as practicable. The results of this design are shown in Appendices C (single point calculations) and G (noise level contours). Table 2.1 below compares the total surface areas of the minimum recommended barriers and the 4 metre high barriers.

 $L_{10(18hour)}$  is the arithmetic average of the  $L_{10}$  values between 0600 hours and midnight, where  $L_{10}$  is the noise level exceeded for 10% of the time.

<sup>2</sup> L<sub>eq(8hour)</sub> is the logarithmic average of the Leq values between 2200 hours and 0600 hours, where the L<sub>eq</sub> is the equivalent (average) noise level for the measurement period.

TABLE 2.1 - TOTAL SURFACE AREA OF NOISE WALLS

Option	Wall Surface Area (m²)		
Minimum Recommended	8,980		
4m High Barriers for Length	15,660		

#### 3.0 METHODOLOGY

The existing acoustic environment was quantified by utilising three (3) automatic noise data loggers at selected residences adjacent the route. Reference was also made to the locations used in the *Roe Highway Project Stage 7, Noise Impact Assessment Report*; June 1999, Ref: 28024 by ERM Mitchell McCotter Pty Ltd, where noise monitoring was also undertaken.

Measurements were undertaken generally in accordance with Australian Standard 2702-1984 *Acoustics – Methods for the Measurement of Road Traffic Noise.* The noise loggers were set-up to record the A-weighted noise level at 1-hour intervals, with the following parameters reported:

$L_1$	The noise level exceeded for 1% of the time (9 seconds).
$L_{10}$	The noise level exceeded for 10% of the time (1 ½ minutes).
$L_{90}$	The noise level exceed for 90% of the time (ambient noise).
$L_{eq}$	The continuous equivalent noise level (average).

From the recorded noise levels, the  $L_{10(18hour)}$ ,  $L_{eq(8hour)}$  and  $L_{eq(24hour)}$  were calculated, defined as:

L <sub>10(18hour)</sub>	The arithmetic average of the recorded L <sub>10</sub> values between 0600 hours
-------------------------	--

and midnight.

 $L_{\text{eq(8hour)}}$  The logarithmic average of the recorded  $L_{\text{eq}}$  values between 2200 hours

and 0600 hours on the same day.

L<sub>eq(24hour)</sub> The logarithmic average of the recorded L<sub>eq</sub> values for a complete 24-

hour period.

The noise logging undertaken by HSA in 2003 were situated at the following residences:

Location H1 36 Merrifield Circle, Leeming
Location H2 17 Heatherlea Parkway, Leeming
Location H3 13 Evergreen Court, Leeming

The noise logging undertaken by ERM in 1998 were situated at the following residences:

Location E1 41 Merrifield Circle, Leeming
Location E3 15 Sellen Court, Leeming
Location E4 20 Noreatt Place, Leeming
Location E4 30 Fern Leaf Court, Leeming
Location E5 13 Evergreen Court, Leeming

Traffic flow information was obtained from GHD and is attached in Appendix H. Other data used in the model is shown below in Table 3.1.

**TABLE 3.1 – TNOISE INPUT DATA** 

Parameter	Roe Highway	Off Ramps & Side Roads
18 Hour Traffic Flow	95% of 24 hour	95% of 24 hour
8 Hour Traffic Flow	7% of 24 hour	7% of 24 hour
% Heavy Vehicles – 18 hour	14	5
% Heavy Vehicles – 8 hour	28	10
Vehicle Speed (km/hr)	100	70
Receiver Height Above Ground (m)	1.5	1.5
Façade Correction (dB(A))	2.5	2.5
Road Surface	OGA	DGA – Off Ramps OGA – Side Roads

Note: Open graded asphalt (2.5 dB(A) quieter than DGA).

The noise levels were predicted using both single point calculations and noise level contours. Single point calculations (SPC) show the noise level at a specific residence whilst noise contours show the noise levels over the surrounding areas. As the noise contour plot is dependent upon the calculation resolution and the amount of interpolation, the single point calculations are always more accurate. Where discrepancies occur between the two calculation types, it is the single point calculations that take priority. The scenarios calculated were:

- 1. Year 2011 Road Traffic & Existing Situation (i.e. no noise walls) SPC only
- 2. Year 2031 Road Traffic & Existing Situation (i.e. no noise walls)
- 3. Year 2011 Road Traffic & Recommended Noise Walls SPC only
- 4. Year 2031 Road Traffic & Recommended Noise Walls
- 5. Year 2011 Road Traffic & 4m High Noise Walls SPC only
- 6. Year 2031 Road Traffic & 4m High Noise Walls

Note that where the residences have a higher relative level (RL) than the road, the noise wall was placed at the boundary of the residences. Where the residences RL is lower than the road, the noise wall has been placed at the edge of the road (2 metres from the edge of the nearest carriageway), however the practicalities of such barriers would require further investigation.

Calculations were made to the first row of houses. Compliance at this location will result in compliance at houses further away due to the attenuation provided by the first row dwellings. However, these dwellings have not been placed in the model and hence this attenuation is not evident in the noise contours.

#### 4.0 CRITERIA

The criteria used in this project are the Main Roads Noise Level Objectives as defined below:

"Objectives are specified upper limits of traffic noise which it is intended, should not be exceeded. Objectives apply outside residential buildings, and outside public buildings such as hospitals, schools and libraries. In the case of public buildings there is a scope to relax the objectives if affected rooms are airconditioned, and therefore normally used with windows closed.

Noise L	_evel Objectives
Base Objective	Objective for High Ambient Areas
63 dB(A) L <sub>10(18hour)</sub>	Ambient + 3 dB(A)
55 dB(A) L <sub>eg(8hour)</sub>	Ambient + 3 dB(A)

#### Notes

- (1) Noise levels are L<sub>10 (18hour)</sub> values, from 6am to midnight, and L<sub>eq(8hour)</sub> values from 10 p.m. to 6 a.m.
- (2) Ambient noise is the level of noise before the road project commences
- (3) A high ambient area is where ambient noise is more than 60 dB(A) L<sub>10(18hour)</sub>, or 52 dB(A) L<sub>eq(8hour)</sub>.
- (4) Due to the impracticality of controlling noise at the upper floors of multi-storey buildings, noise assessment is restricted to the ground floor level.
- (5) Noise is assessed 1 metre from a building, and 1.2 to 1.5 metres above the ground floor level.
- (6) The objectives apply to the expected 15 to 20 years after opening of the road project, using available traffic forecasts.
- (7) Noise level objectives relate to the total traffic noise expected at a building facade, i.e. noise from the new road and any other roads.

#### 5.0 RESULTS

The results of the noise monitoring are contained in Appendix B. Tables 5.1 and 5.2 show the calculated weekday  $L_{10(18hour)}$ ,  $L_{eq(8hour)}$  and  $L_{eq(24hour)}$  of the HSA and ERM monitoring respectively.

TABLE 5.1 - HSA MEASURED L<sub>10(18hour)</sub>, L<sub>eq(8hour)</sub> AND L<sub>eq(24hour)</sub>

Location	L <sub>10(18hour)</sub>	L <sub>eq(8hour)</sub>	L <sub>eq(24hour)</sub>
H1. 36 Merrifield Circle, Leeming	60	53	58
H2. 17 Heatherlea Parkway, Leeming	52	45	51
H3. 13 Evergreen Court, Leeming	51	43	49

TABLE 5.2 - ERM MEASURED L<sub>10(18hour)</sub>, L<sub>eq(8hour)</sub> AND L<sub>eq(24hour)</sub>

Location	L <sub>10(18hour)</sub>	Leg(8hour)	L <sub>eq(24hour)</sub>
E1. 41 Merrifield Circle, Leeming	55	53	51
E2. 15 Sellen Court, Leeming	50	50	48
E3. 20 Noreatt Place, Leeming	49	50	49
E4. 30 Fern Leaf Court, Leeming	50	52	53
E5. 13 Evergreen Court, Leeming	53	55	56

The monitoring undertaken by ERM shows some relatively high  $L_{eq(8hour)}$  values in comparison to the  $L_{10(18hour)}$  values. No explanation is provided in the report to justify this anomaly. For the two HSA locations that were in similar locations (H1 & H3), the relationship between the two parameters is considered more typical. Nevertheless, the monitoring does indicate that all locations have  $L_{10(18hour)}$  values of less than 60 dB(A) and therefore the applicable criteria is 63 dB(A)  $L_{10(18hour)}$ . The  $L_{eq(8hour)}$  values are somewhat sporadic, considered mainly due to the ERM anomalies. Thus, it is considered that the acceptable  $L_{eq(8hour)}$  value is also the base level of 55 dB(A).

It has been calculated that the  $L_{eq(8hour)}$  would be 8.5 dB(A) less than the  $L_{10(18hour)}$ . As such it is the  $L_{10(18hour)}$  criteria that determines the amount of noise control required as compliance with this, will result in compliance with the  $L_{eq(8hour)}$  criteria. For instance, if the  $L_{10(18hour)}$  predicted noise level is 63 dB(A), the  $L_{eq(8hour)}$  noise level will be 54.5 dB(A), hence compliance with both criteria.

Noise levels in the Years 2011 and 2031 were predicted based on the existing standard residential fences. Noise levels were predicted to be up to 67.3 dB(A)  $L_{10(18hour)}$  (4.3 dB(A) exceedance) in 2011 and 69.1 dB(A)  $L_{10(18hour)}$  (6.1 dB(A) exceedance) in 2031. The results of these calculations can be seen in Appendix C as single point calculations. Noise contour plots are also contained in Appendix D for the Year 2031. The 63 dB(A)  $L_{10(18hour)}$  criterion in 2031 is predicted to be exceeded at the majority of residences between Green Croft Gardens to Merrifield Circle, east of the Kwinana Freeway and between Stone Court and Tetlow Place, southwest of the Kwinana Freeway.

As exceedances were calculated, noise control is required to satisfy the MRWA criteria. A number of options are available to minimise road traffic noise and in this instance, noise barriers are considered the most practicable. Where the relative level (RL) of the road is higher than that at the residences, the barriers have been placed adjacent the road (2 metres from the edge of the nearest carriageway). Where the RL of the road is lower than that of the residences, the barrier has been placed at the boundary of the residences. The practicalities of either option, particularly a barrier on the road reserve, have not been explored at this stage.

The minimum length and height of the noise walls are given in Appendix E. Both the height of the barrier and top RL of the barriers are shown on the drawings. The barriers are required to be at the specified height (or higher) for the length of the wall until the next height is nominated, reading from left to right. Remembering that these are the minimum heights, it may be more aesthetic to construct barriers of a more consistent height. Note that the barriers are required to have a surface mass of more than  $10 \text{kg/m}^2$  and not contain any gaps.

Appendix C contains the single point calculations to each of the residences for the Years 2011 and 2031 with the minimum recommended noise walls. Noise contour plots are contained in Appendix F for the 2031 scenario.

It is considered that a 4 metre high noise wall is the maximum practicable height of barrier that would be constructed. Contained in Appendices C and G are the predicted noise levels if such walls were constructed for the length of the road.

A comparison of the surface areas of the minimum recommended barriers and the 4 metre high barriers is shown below in Table 5.3.

TABLE 5.3 - TOTAL SURFACE AREA OF NOISE WALLS

Option	W 110 c		
Option	Wall Surface Area (m²)		
Minimum Recommended	8,980		
4m High Barriers for Length	15,660		

For: HERRING STORER ACOUSTICS

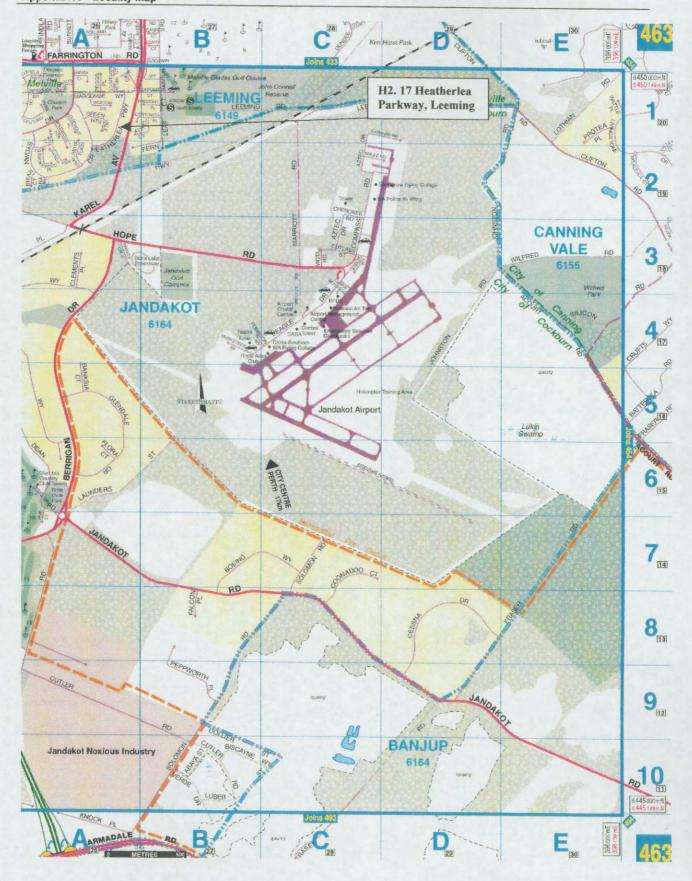
Terry George

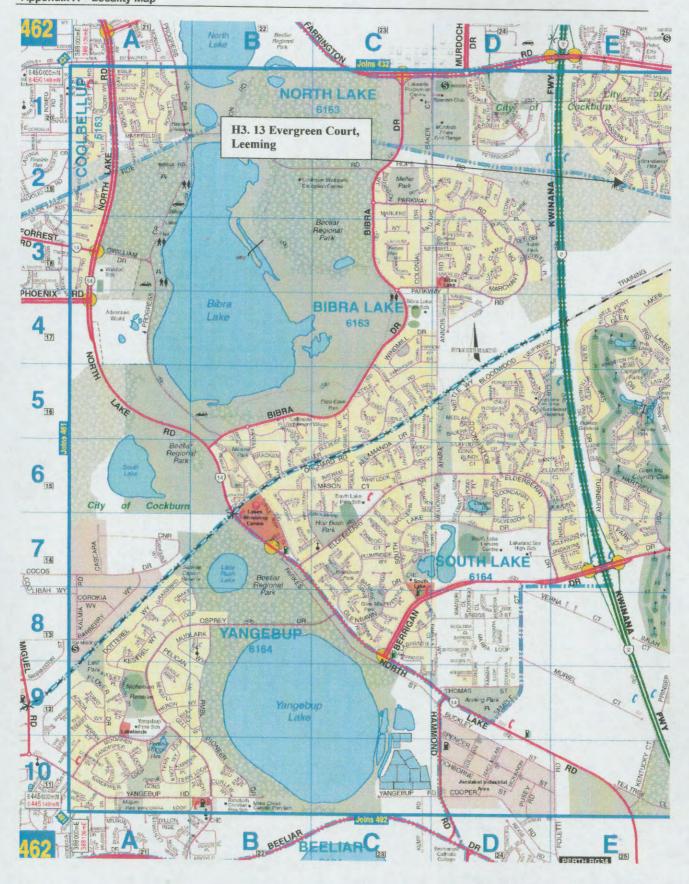
Checked: Lynton Storer

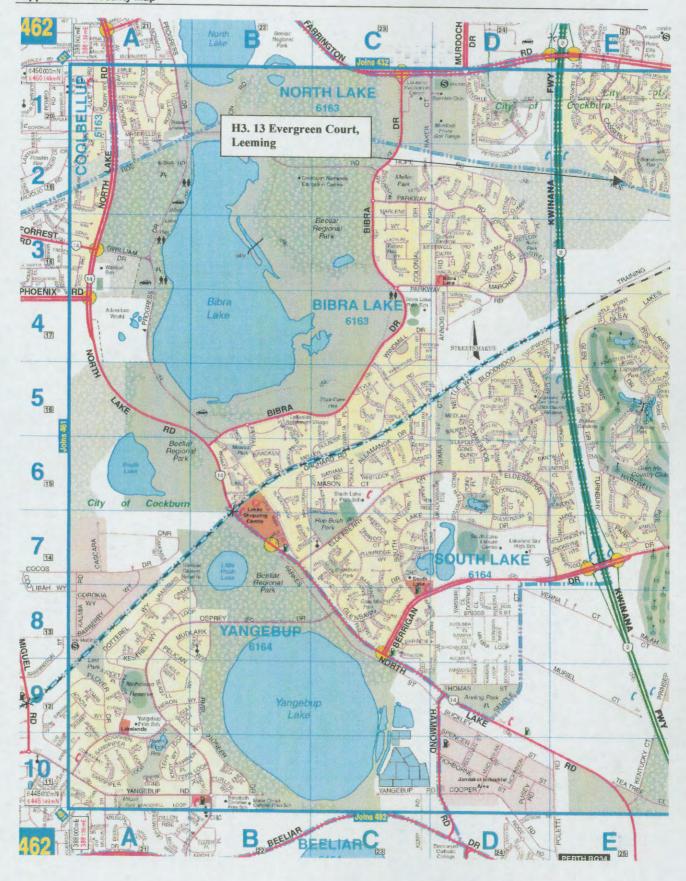
8 August 2003

# **APPENDIX A**

**GENERAL LOCALITY MAP** 







# APPENDIX B

NOISE MONITORING RESULTS

TABLE B1 - NOISE MONITORING RESULTS, dB(A)

Location / Date	L <sub>10(18hour)</sub>	Leq(8hour)	L <sub>eq(24hour)</sub>	
36 Merrifield Circle, Leemin	g			
19/03/03	60.8	58.1	53.8	
20/03/03	61.1	58.1	53.0	
25/03/03	59.0	56.6	53.1	
Average	60	58	53	
17 Heatherlea Parkway, Lee	eming			
18/03/03	52.1	50.2	43.7	
19/03/03	52.5	51.3	45.2	
24/03/03	4/03/03 52.4		47.1	
Average	52	51	45	
13 Evergreen Court, Leemir	ng			
24/03/03	50.9	49.5	44.5	
25/03/03	25/03/03 49.8 47.8		40.1	
26/03/03	51.2	49.3	44.8	
Average	51	49	43	

#### TRAFFIC NOISE MEASUREMENT

#### Results

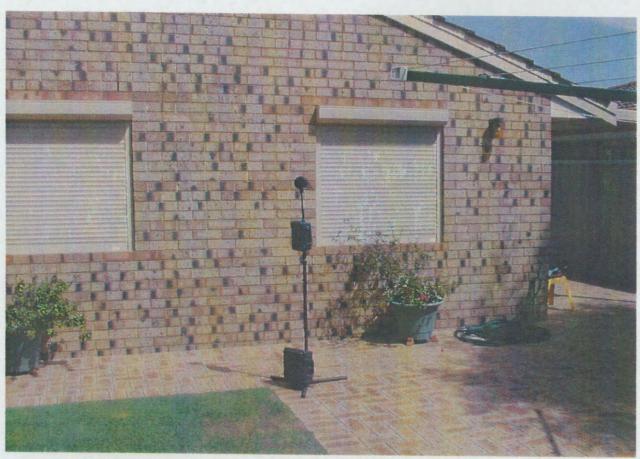
	Site Data
Location	
Project:	Roe Highway Stage 7 - South Street to Kwinana Freeway
Street Address	36 Merrifield Circle
ocality:	Leeming
Occupier	Kirkpatrick
Dates:	17/03/02 to 27/03/02
Category:	Main Roads will provide this information
Site	p. the memorinal of
Distance from the	45m
microphone to the kerb	
Height of the road in	same
relation to the ground	
Road Surface Type:	open-graded-asphalt
Speed Zone:	70kmph
Absorbing Ground	60%
Angle of View:	100 degrees
Road Gradient:	Flat
Traffic Flow	Main Roads will provide this information
leavy Vehicles	Main Roads will provide this information
House-Road Orientation:	South
Carriageways and lanes:	2,6
Comment	=1-
Comment:	Before opening of Roe Highway Stage 7.
	Logger at rear of property, 1 metre from wall and 1.5 metres above ground
	Main source of noise is from South Street
	William source or moise is more source of the source of th
References	And and theight train hoise may inhuence levels.
AMG Z50 E/N	Main Roads will provide this information
Road Name	South Street
EXCEL file	Tr Heatherlea S1.xls
Raw data file	Heather Logger xls
Equipment	reduter Logger.Alb
Analyser Number:	91
Microphone Number	N/A
Calibrator Number	5
Calibrator Values:	94.0, 94.0
Operator:	USANTG
Weather	THOUSE THE PROPERTY OF THE PRO
Wind:	Acceptable used and discourse above and the second
TTING.	Acceptable wind conditions were obtained on the 19, 20 & 25 March 2003

CRTN: Calculation of Road Traffic Noise, by UK Department of Transport, 1988

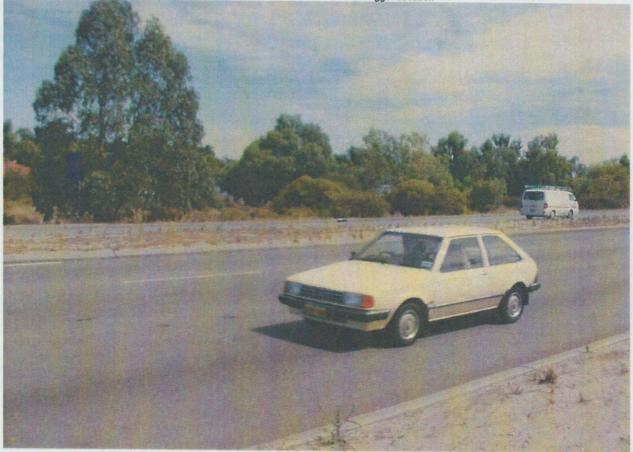
Hourly Noise Level Data

Date	Time	L1	L10	Leq	L90	Wind Dir V	Wind Speed (kn	ots) Rainfall (mm)
19-Mar	100	60.5	52.9	49.5	42.6	100	11	0.0
19-Mar	200	59.0	52.4	48.6	41.3	100	15	0.0
19-Mar	300	61.5	54.6	51.0	43.0	90	13	0.0
19-Mar	400	61.4	55.3	51.6	43.8	90	13	0.0
19-Mar	500	64.1	59.0	55.4	46.8	80	15	
19-Mar	600	65.2	61.9	58.4	51.8	80		0.0
19-Mar	700	66.9	64.0	60.9			15	0.0
19-Mar	800	67.3	65.0		55.5	80	13	0.0
19-Mar	900			62.0	57.2	80	11	0.0
		67.5	63.4	60.8	56.4	80	17	0.0
19-Mar	1000	66.2	62.9	61.3	54.4	90	17	0.0
19-Mar	1100	65.6	62.8	61.7	53.1	70	19	0.0
19-Mar	1200	64.9	61.8	58.5	52.3	100	13	0.0
19-Mar	1300	64.5	61.6	58.3	53.4	80	11	0.0
19-Mar	1400	67.3	61.0	58.9	50.6	70	13	0.0
19-Mar	1500	64.5	60.7	57.4	51.3	80	11	0.0
19-Mar	1600	66.1	60.4	57.9	52.6	200	19	0.0
19-Mar	1700	67.9	60.9	58.4	51.7	200	20	0.0
19-Mar	1800	69.7	61.9	59.9	54.3	220	17	0.0
19-Mar	1900	65.6	61.7	59.0	52.8	340	6	0.0
19-Mar	2000	61.4	57.4	54.3	49.3	0	0	0.0
19-Mar	2100	64.4	57.2	55.1	50.0	0	0	
19-Mar	2200	62.1	57.9	55.0	50.6	160	7	0.0
19-Mar	2300	63.0	57.9	54.8				0.0
19-Mar	0	61.2	55.7	51.9	48.7	110	7	0.0
20-Mar	100	60.7			44.6	80	11	0.0
20-Mar	200		55.0	51.0	43.3	100	11	0.0
20-Mar		62.3	53.0	50.1	41.4	90	15	0.0
	300	62.0	52.9	49.9	41.6	90	13	0.0
20-Mar	400	61.4	54.1	50.3	42.0	90	17	0.0
20-Mar	500	62.7	57.5	53.3	43.5	80	13	0.0
20-Mar	600	65.4	61.1	57.6	50.3	70	13	0.0
20-Mar	700	66.7	64.4	61.4	56.8	80	15	0.0
20-Mar	800	67.1	64.4	61.6	57.1	90	11	0.0
20-Mar	900	71.2	63.8	61.5	56.7	60	17	0.0
20-Mar	1000	69.5	63.4	60.9	55.3	60	19	0.0
20-Mar	1100	67.9	62.9	60.4	54.0	70	15	0.0
20-Mar	1200	64.9	61.4	58.4	52.3	50	15	0.0
20-Mar	1300	67.4	61.6	58.9	52.8	70	11	0.0
20-Mar	1400	69.8	61.8	59.3	51.5	90	13	0.0
20-Mar	1500	65.4	62.1	58.4	51.8	70	11	
20-Mar	1600	65.0	62.4	59.9	52.2			0.0
20-Mar	1700	64.9	60.2	57.4		80	9	0.0
20-Mar	1800	64.0	60.9		52.6	80	9	0.0
20-Mar	1900			58.0	53.4	100	9	0.0
20-Mar		68.0	61.1	58.6	52.5	90	7	0.0
	2000	65.6	59.8	57.3	52.1	90	9	0.0
20-Mar	2100	64.4	59.2	56.7	50.9	90	11	0.0
20-Mar	2200	63.2	58.5	55.4	50.0	90	11	0.0
20-Mar	2300	60.6	56.3	52.5	45.7	90	13	0.0
20-Mar	0	61.9	55.6	52.5	44.1	100	9	0.0
25-Mar	100	61.4	53.8	51.4	43.7	0	0	0.0
25-Mar	200	59.4	51.6	49.8	41.8	0	0	0.0
25-Mar	300	59.8	52.6	50.5	44.9	160	6	0.0
25-Mar	400	60.2	53.6	51.2	44.3	160	6	0.0
25-Mar	500	62.8	57.2	53.9	45.9	160	2	0.0
25-Mar	600	64.7	61.4	57.8	50.3	90	7	0.0
25-Mar	700	67.6	64.0	61.4	57.6	90	7	0.0
25-Mar	800	66.9	63.6	60.8	55.7	80		
25-Mar	900	70.3	63.3	60.7			11	0.0
25-Mar	1000				55.1	70	7	0.0
25-Mar		66.4	61.9	59.4	51.1	70	7	0.0
	1100	63.5	59.9	56.2	49.2	50	6	0.0
25-Mar	1200	68.0	61.0	58.1	50.1	120	4	0.0
25-Mar	1300	64.5	59.8	56.3	49.2	330	7	0.0
25-Mar	1400	64.0	58.8	55.5	49.2	220	17	0.0
25-Mar	1500	64.8	58.3	55.7	48.5	240	15	0.0
25-Mar	1600	63.8	58.6	55.5	49.1	230	17	0.0
25-Mar	1700	70.0	59.0	58.0	49.7	230	17	0.0
25-Mar	1800	63.4	58.2	56.3	50.2	220	17	0.0
25-Mar	1900	69.2	59.0	56.7	49.2	200	17	0.0
25-Mar	2000	66.2	57.2	55.4	48.2	180	13	0.0
25-Mar	2100	60.1	55.6	52.5	46.9	190		
25-Mar	2200	60.2	55.6				13	0.0
25-Mar	2300	60.2		52.5	46.4	180	13	0.0
25-Mar	0		55.5	52.5	46.2	170	9	0.0
ZO-IVIdI	U	60.5	53.6	50.8	44.8	160	4	0.0

Job No. 03107-1-2

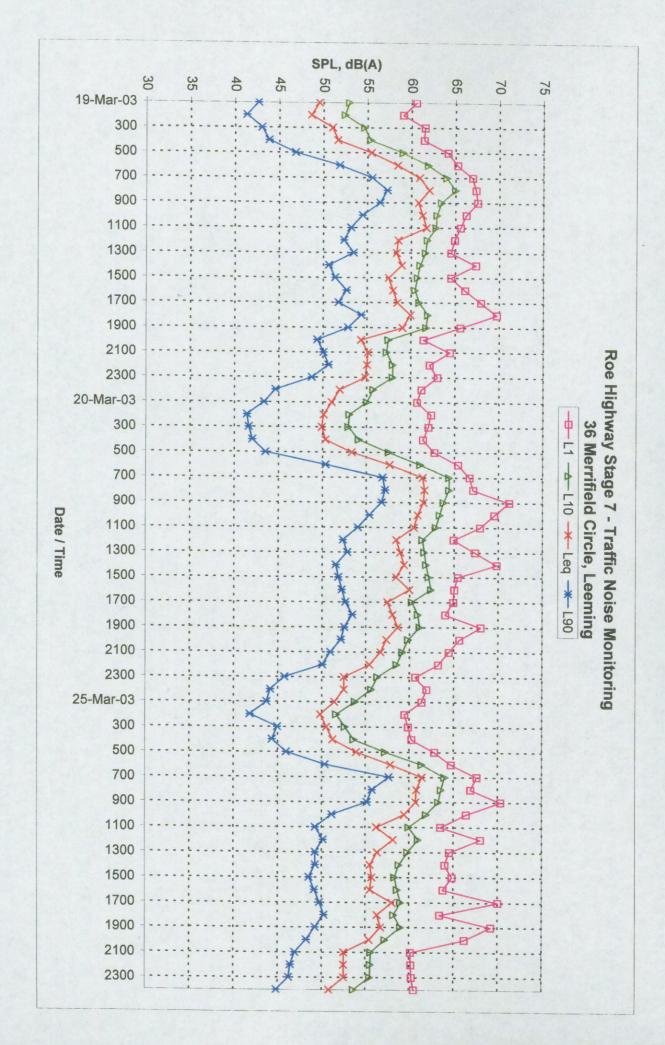


Location H1 - View of Logger Location



Location H1 - View of Road Layout

Job No. 03107-1-2



#### TRAFFIC NOISE MEASUREMENT

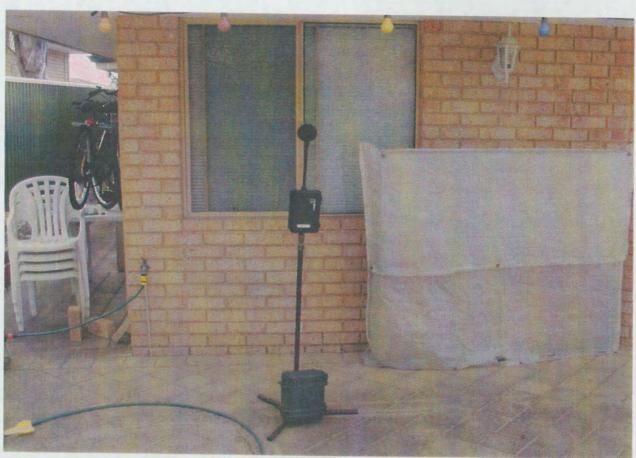
#### Results

Street Address 17 Health Locality: Leeming Occupier Ashworth Dates: 17/03/02 Category: Main Roa Site  Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grad Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degra Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa House-Road Orientation: East Comment Comment: Before op Logger at Main sour Aircraft no	
Street Address 17 Heath Locality: Leeming Occupier Ashworth Dates: 17703/02 Category: Main Roa Site Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grac Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrac Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa Heavy Vehicles Main Roa House-Road Orientation: East Comment Comment: Before op Logger at Main sour Aircraft no References AMG Z50 E/N Main Roa Road Name Karel Aw EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	nerlea Parkway
Street Address 17 Heath Locality: Leeming Occupier Ashworth Dates: 17/03/02 Category: Main Roa Site Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: Open-grat Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrat Road Gradent: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa Heuse Road Orientation: East Carriageways and lanes: 1,2 Comment Comment: Before og Logger at Main soun Aircraft ne References AMG Z50 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Number 5 Collibrator Values: 94.0, 93.8 Operator: HSA/TG	nerlea Parkway
Locality:  Leeming Occupier Ashworth Dates: 17/03/02 Category: Main Roa Site Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: Open-grac Speed Zone: Absorbing Ground Absorbing Ground Angle of View: Road Gradient: Traffic Flow Main Roa Heavy Vehicles House-Road Orientation: Carriageways and lanes: Comment:  Comment:  Before op Logger at Main Roa Arcraft no References AMG Z50 E/N Road Name EXCEL file 17 Heath Raw data file Equipment Analyser Number: Analyser Number: Alicalibrator Values: 94.0, 93.8 Operator: HSA/TG Ashwork Main Roa Raferences AMG Z50 E/N Main Roa Raferences AMG Z50 E/N Amin Roa Raferences Amin Roa Raf	
Dates: 17/03/02 Category: Main Roa Site Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grac Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrac Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa Heavy Vehicles 1,2 Comment Before or Logger at Main soun Aircraft no Road Gradient: References  AMG ZS0 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heather L Equipment Analyser Number: 71 Microphone Number N/A Calibrator Number 5 Collibrator Vulues: 94.0, 93.8 Operator: 150m	
Category:  Site  Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: Speed Zone: Absorbing Ground Absorbing Ground Absorbing Ground Absorbing Ground Traffic Flow Heavy Vehicles House-Road Orientation: Carriageways and lanes: Comment  Comment:  Before op Logger at Main Roa Almar Roa Main Roa Road Name References  AMG Z50 E/N Road Name EXCEL file T7 Heath Raw data file Heather L Equipment Analyser Number: Analyser Number: Alicraftor Vilager Alicraft of Traffic Type Heather L Calibrator Number 5 Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator:  HSA/TG  Smert Som  Main Roa References  AMG Z50 E/N Main Roa References  AMG Z50 E/N Air Roa Road Name EQUIPMENT Analyser Number: Analyser Number: 5 Calibrator Number 5 Calibrator Values: 94.0, 93.8	
Site  Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grat Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrat Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa Heavy Vehicles Main Roa Comment: Before op Logger at Main soun Aircraft no References AMG 250 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: Smart Smart Smart Sommer Son Main Roa Refacences AMG 250 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Number 5 Calibrator Values: 94.0, 93.8	to 27/03/02
Site  Distance from the microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grat Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrat Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa Heavy Vehicles Main Roa Comment: Before op Logger at Main soun Aircraft no References AMG 250 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: Smart Smart Smart Sommer Son Main Roa Refacences AMG 250 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Number 5 Calibrator Values: 94.0, 93.8	ads will provide this information
microphone to the kerb Height of the road in relation to the ground Road Surface Type: open-grac Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degra Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Main Roa House-Road Orientation: East Comment: Before op Logger at Main sour Aircraft no Road Name Karel As EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: 13m Openator  -3m -3m -3m -3m -3m -3m -3m -3m -3m -3	
Height of the road in relation to the ground Road Surface Type: open-grat Speed Zone: 70kmph Absorbing Ground 50% Angle of View: 100 degrat Road Gradient: Flat Traffic Flow Main Road Heavy Vehicles Main Road Heavy Vehicles Main Road Carriageways and lanes: 1,2 Comment Comment: Before op Logger at Main soun Aircraft number Speed Main Road Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
relation to the ground Road Surface Type: Open-grat Speed Zone: 70kmph Absorbing Ground Angle of View: 100 degr. Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Heuse Road Orientation: Comment Comment: Before og Logger at Main soun Aircraft ne References AMG Z50 E/N Road Name Karel Ave EQUIPMENT Road Speed Speed Speed Road Name Road Heather L Equipment Analyser Number: Microphone Number 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: Tokmph To	
relation to the ground Road Surface Type: Open-grat Speed Zone: 70kmph Absorbing Ground Angle of View: 100 degr. Road Gradient: Flat Traffic Flow Main Roa Heavy Vehicles Heuse Road Orientation: Comment Comment: Before og Logger at Main soun Aircraft ne References AMG Z50 E/N Road Name Karel Ave EQUIPMENT Road Speed Speed Speed Road Name Road Heather L Equipment Analyser Number: Microphone Number 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: Tokmph To	
Road Surface Type: open-grate Speed Zone: 70kmph Speed Zone: 70kmph Speed Zone: 70kmph Speed Zone: 70kmph Speed Zone: 100 degrate Absorbing Ground Speed Zone: 100 degrate Analyser Logger at Main Road Road Road Road Road Road Road Road	
Speed Zone	nded-asphalt
Absorbing Ground   50%	
Angle of View: 100 degra Road Gradient: Flat Traffic Flow Main Roa House-Road Orientation: East Carriageways and lanes: 1,2 Comment: Before of Logger at Main soun Aircraft in Road Name References  AMG Z50 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 940, 93.8 Operator: HSA/TG	
Road Gradient:   Flat	ees
Traffic Flow Main Roa Heavy Vehicles Main Roa Main Roa House Road Orientation: East Carriageways and lanes: 1,2 Comment: Before og Logger at Main sour Aircraft nr.  References AMG Z50 E/N Main Roa Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number N/A Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
Heavy Vehicles	ads will provide this information
House-Road Orientation: East Carriageways and lanes: 1,2 Comment: Before op Logger at Main sour Aircraft nr References AMG Z50 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	ads will provide this information
Comment   Before op	p
Comment   Before op	
Logger at Main sour Aircraft not References  AMG Z50 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Equipment Analyser Number: 71 Microphone Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
Logger at Main sour Aircraft no Aircraft n	pening of Roe Highway Stage 7.
Main sour Aircraft nu Aircraft	trear of property, 1 metre from wall and 1.5 metres above ground
References  AMG Z50 E/N  Road Name  EXCEL file  Raw data file  Equipment  Analyser Number:  Alicraft no  Analyser Number:  Analyser Number:  Alicraft no  Analyser Analyser Number:  Analyser Number:  Alicraft no  Alicraf	ince of noise is from Karel Avenue
References           AMG Z50 E/N         Main Roa           Road Name         Karel Ave           EXCEL file         17 Heath           Raw data file         Heather L           Equipment         71           Analyser Number:         74           Microphone Number         N/A           Calibrator Number         5           Calibrator Values:         940, 93.8           Operator:         HSA/TG	noise may influence levels.
AMG Z50 E/N Main Roa Road Name Karel Ave EXCEL file 17 Heath Raw data file Heather L Equipment Analyser Number N/A Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	ose may minuence levels.
Road Name         Karel Ave           EXCEL file         17 Heath           Raw data file         Heather L           Equipment         71           Analyser Number         71           Microphone Number         N/A           Calibrator Number         5           Calibrator Values:         94.0, 93.8           Operator:         HSA/TG	ads will provide this information
EXCEL file 17 Heath Raw data file Heather L  Equipment  Analyser Number: 71  Microphone Number N/A  Calibrator Number 5  Calibrator Values: 940, 93.8  Operator: HSA/TG	
Raw data file Heather L  Equipment  Analyser Number: 71  Microphone Number N/A  Calibrator Number: 5  Calibrator Values: 94.0, 93.8  Operator: HSA/TG	
Equipment Analyser Number: 71 Microphone Number N/A Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
Analyser Number: 71  Microphone Number N/A  Calibrator Number 5  Calibrator Values: 94.0, 93.8  Operator: HSA/TG	Lugger. Acc
Microphone Number N/A Calibrator Number 5 Calibrator Values: 94.0, 93.6 Operator: HSA/TG	
Calibrator Number 5 Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
Calibrator Values: 94.0, 93.8 Operator: HSA/TG	
Operator: HSA/TG	8
The same of the sa	le wind conditions were obtained on the 40,40 to 0.44 May 1,000
Acceptab	ole wind conditions were obtained on the 18, 19 & 24 March 2003
CRTN: Calculation of Road Traffic Nois	

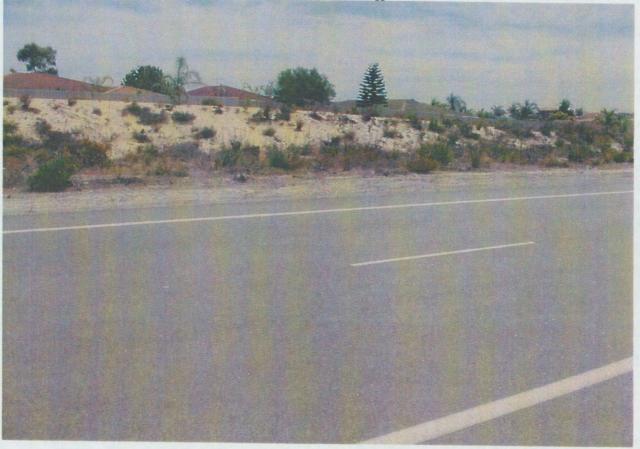
CRTN: Calculation of Road Traffic Noise, by UK Department of Transport, 198

Hourly Noise Level Data

Date 18-Mar	Time	L1	L10	Leq	L90			ots) Rainfall (mm)
	100	49.9	41.2	38.7	28.4	220	9	0.0
18-Mar 18-Mar	200	54.3	43.0	40.5	28.6	140	2	0.0
	300	50.4	40.9	38.4	28.0	140	2	0.0
18-Mar	400	46.4	38.8	35.6	28.8	160	9	0.0
18-Mar	500	54.0	43.2	40.0	29.5	150	7	0.0
18-Mar	600	53.9	47.2	43.8	31.2	160	9	0.0
18-Mar	700	58.1	52.2	48.4	38.5	140	9	0.0
18-Mar	800	62.1	54.6	53.1	39.4	150	15	0.0
18-Mar	900	66.0	56.9	57.7	39.8	150	19	0.0
18-Mar	1000	64.1	56.4	54.7	40.2	190	19	0.0
18-Mar	1100	62.2	51.6	51.6	39.3	170	20	0.0
18-Mar	1200	61.7	51.2	50.7	39.9	180	17	0.0
18-Mar	1300	61.1	50.8	49.8	38.2	210	20	0.0
18-Mar	1400	62.9	52.1	52.0	36.8	200	15	0.0
18-Mar	1500	61.2	51.4	49.4	37.8	210	20	0.0
18-Mar	1600	59.7	50.2	48.3	40.7	200	22	0.0
18-Mar	1700	59.6	50.9	48.7	43.2	210	22	0.0
18-Mar	1800	59.6	51.2	48.8	42.6	210	24	
18-Mar	1900	59.5	51.5	49.0	41.6	190	20	0.0
18-Mar	2000	60.2	50.6	48.1	41.6			0.0
18-Mar	2100	60.9	52.9	50.4		170	15	0.0
18-Mar	2200	61.7	51.9		40.0	170	15	0.0
18-Mar	2300	62.1		49.4	35.7	170	11	0.0
18-Mar	0		50.9	48.4	35.8	140	6	0.0
		62.5	49.9	47.4	39.0	110	7	0.0
19-Mar	100	46.2	41.4	38.8	33.6	100	11	0.0
19-Mar	200	47.4	41.6	38.7	33.7	100	15	0.0
19-Mar	300	55.3	44.6	42.4	33.9	90	13	0.0
19-Mar	400	52.9	45.0	42.0	33.8	90	13	0.0
19-Mar	500	60.2	47.3	46.6	35.4	80	15	0.0
19-Mar	600	63.0	52.0	51.1	40.8	80	15	0.0
19-Mar	700	61.4	55.7	51.8	43.6	80	13	0.0
19-Mar	800	66.6	58.4	57.2	48.8	80	11	0.0
19-Mar	900	68.8	58.4	55.9	49.8	80	17	0.0
19-Mar	1000	65.8	57.0	55.9	44.8	90	17	0.0
19-Mar	1100	63.7	55.0	54.0	43.7	70	19	0.0
19-Mar	1200	62.6	54.0	53.1	43.3	100	13	0.0
19-Mar	1300	61.5	53.0	52.1	40.5	80	11	0.0
19-Mar	1400	65.6	54.0	52.8	38.7	70	13	
19-Mar	1500	64.5	53.8	52.1	40.2	80	11	0.0
19-Mar	1600	60.9	53.2	50.0	40.5	200		0.0
19-Mar	1700	62.7	51.7	50.6			19	0.0
19-Mar	1800	63.0	54.4	51.9	39.6	200	20	0.0
19-Mar	1900	61.4			39.5	220	17	0.0
19-Mar	2000		53.0	50.5	40.2	340	6	0.0
19-Mar		55.0	49.1	46.6	40.0	0	0	0.0
	2100	51.7	47.1	44.6	39.0	0	0	0.0
19-Mar	2200	50.1	46.1	43.6	38.0	160	7	0.0
19-Mar	2300	49.3	45.6	43.1	35.8	110	7	0.0
19-Mar	0	48.5	45.1	43.0	33.9	80	11	0.0
24-Mar	100	48.4	34.4	39.7	30.1	240	17	0.0
24-Mar	200	48.4	33.2	40.4	31.0	220	7	0.0
24-Mar	300	47.3	33.7	40.7	29.3	0	0	0.0
24-Mar	400	55.8	45.9	47.5	31.3	0	0	0.0
24-Mar	500	60.0	52.0	50.8	43.1	0	0	0.0
24-Mar	600	62.1	55.1	52.5	47.4	0	0	0.0
24-Mar	700	64.2	58.1	54.2	46.2	170	7	0.0
24-Mar	800	64.8	57.9	55.1	48.5	160	20	0.0
24-Mar	900	61.2	56.3	54.3	51.2	160	15	0.0
24-Mar	1000	66.0	58.6	55.7	49.2	150	15	
24-Mar	1100	63.6	55.6	52.4	40.0	140		0.0
24-Mar	1200	67.1	55.4	52.0	39.9		13	0.0
24-Mar	1300	71.1	54.5			180	15	0.0
24-Mar	1400	72.8		52.5	38.0	220	17	0.0
24-Mar	1500		57.3	54.9	39.7	210	22	0.0
		68.2	56.8	55.7	39.4	200	17	0.0
24-Mar	1600	65.4	54.0	54.7	41.0	220	20	0.0
24-Mar	1700	62.2	52.5	49.8	39.3	220	19	0.0
24-Mar	1800	59.6	49.9	47.7	37.8	210	13	0.0
24-Mar	1900	56.4	47.8	44.8	38.3	200	13	0.0
24-Mar	2000	54.7	46.7	43.4	38.3	180	9	0.0
24-Mar	2100	53.9	46.1	42.6	37.1	170	11	0.0
24-Mar	2200	53.5	45.9	42.3	34.7	160	9	0.0
	2200 2300	<b>53.5</b> 53.1	<b>45.9</b> <b>45.6</b>	<b>42.3</b> 41.9	34.7	160	9	0.0

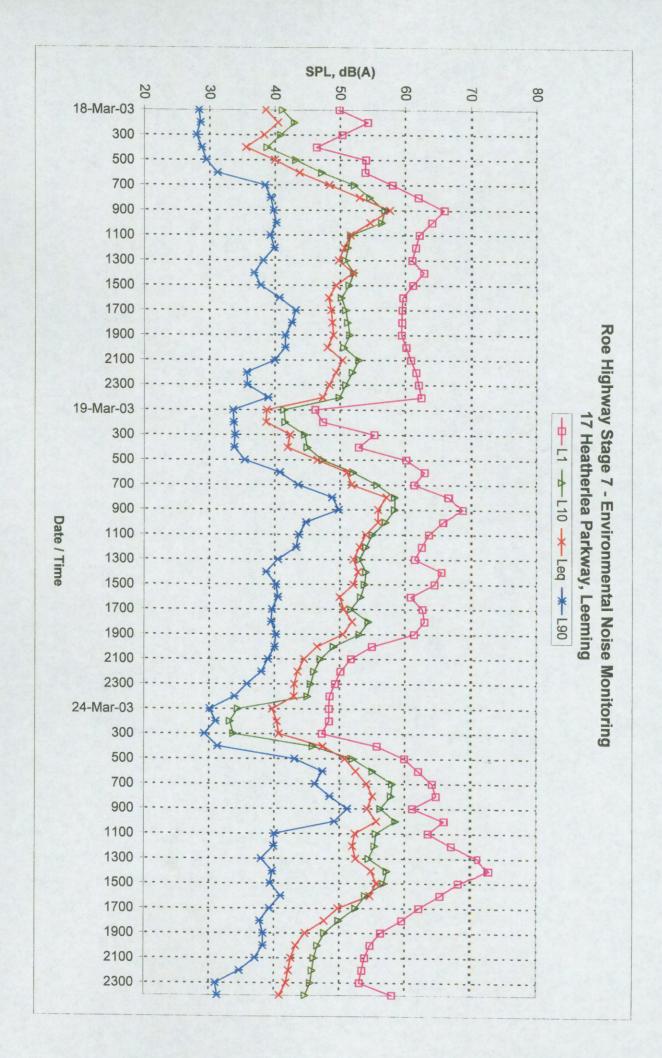


Location H2 - View of Logger Location



Location H2 - View of Road Layout

Job No. 03107-1-2



#### TRAFFIC NOISE MEASUREMENT

#### Results

	Site Data
Location	
Project:	Roe Highway Stage 7 - South Street to Kwinana Freeway
Street Address	13 Evergreen Court
Locality:	Leeming
Occupier	Mitchell
Dates:	17/03/02 to 27/03/02
Category:	Main Roads will provide this information
Site	
Distance from the	
microphone to the kerb	
Height of the road in	
relation to the ground	
Road Surface Type:	
Speed Zone:	
Absorbing Ground	
Angle of View:	
Road Gradient:	
Traffic Flow	Main Roads will provide this information
Heavy Vehicles	Main Roads will provide this information
House-Road Orientation:	South
Carriageways and lanes:	
Comment	
Comment:	Before opening of Roe Highway Stage 7.
	Logger at rear of property, 1 metre from wall and 1.5 metres above ground
	Main source of noise is from Kwinana Freeway
	Aircraft and freight train noise may influence levels.
References	The state of the s
AMG Z50 E/N	Main Roads will provide this information
Road Name	Main Roads will provide this information
EXCEL file	13 Evergreen S1.xls
Raw data file	Evergreen Logger,xls
Equipment	
Analyser Number:	69
Microphone Number	N/A
Calibrator Number	5
Calibrator Values:	94.0, 93.9
Operator:	HSATG
Weather	
Wind:	Acceptable wind conditions were obtained on the 24, 25 & 26 March 2003
	The state of the s
19	
CRTN: Calculation of Road	Traffic Noise, by UK Department of Transport. 1988

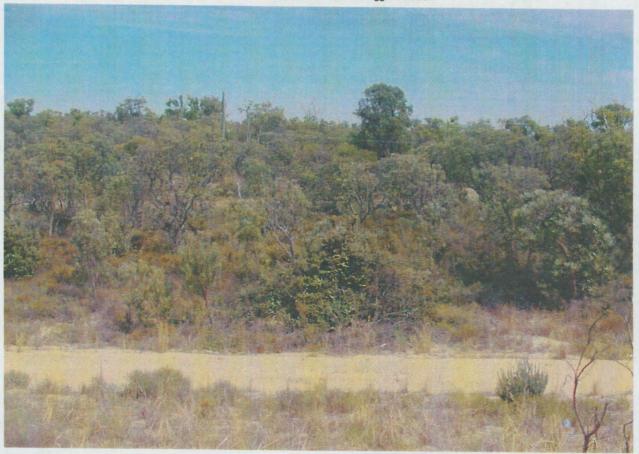
CRTN: Calculation of Road Traffic Noise, by UK Department of Transport, 1988

Hourly Noise Level Data

Date	Time	L1	L10	Leq	L90	Wind Dir	Wind Speed (kn	ots) Rainfall (mm)
24-Mar	100	47.9	44.1	41.1	39.5	240	17	0.0
24-Mar	200	47.8	43.4	40.2	36.1	220	7	0.0
24-Mar	300	47.7	42.8	39.3	32.8	0	0	0.0
24-Mar	400	50.0	44.7	41.1	34.8	0	0	0.0
24-Mar	500	53.5	49.2	46.2	40.5	0	0	0.0
24-Mar	600	55.3	52.4	49.7	46.4	0	0	0.0
24-Mar	700	57.0	54.4	53.3	50.1	170	7	0.0
24-Mar	800	55.7	53.5	52.0	51.2	160	20	0.0
24-Mar	900	54.3	52.5	50.7	49.0	160	15	0.0
24-Mar	1000	57.4	51.0	49.3	45.6	150	15	0.0
24-Mar	1100	56.5	50.3	48.9	44.5	140	13	0.0
24-Mar 24-Mar	1200	63.2	51.3	52.3	44.8	180	15	0.0
24-Mar 24-Mar	1300	62.3	51.6	51.5	45.6	220	17	0.0
24-Mar	1400	62.0	53.9	52.2	47.6	210	22	0.0
24-Mar	1500	62.5	53.6	52.0	48.1	200	17	0.0
24-Mar	1600	59.4	52.8	51.1	48.1	220	20	0.0
24-Mar	1700 1800	60.9	53.1	51.6	48.8	220	19	0.0
24-Mar		60.2	51.1	50.2	46.9	210	13	0.0
24-Mar	1900	55.7	50.5	49.6	45.3	200	13	0.0
24-Mar	2100	57.3	49.6	48.9	44.4	180	9	0.0
24-Mar	2200	51.9 49.8	48.4	46.5	43.3	170	11	0.0
24-Mar	2300	54.8	47.1	44.7	42.3	160	9	0.0
24-Mar	0	46.5	48.1	45.7	41.5	0	0	0.0
25-Mar	100	55.7	43.0 41.6	40.4	36.9	0	0	0.0
25-Mar	200	47.5	41.4	41.0	32.2	0	0	0.0
25-Mar	300	47.5	40.7	37.9 37.4	31.5	0	0	0.0
25-Mar	400	47.5	39.9	36.8	31.5	160	6	0.0
25-Mar	500	48.2	37.9	36.8	31.6 32.8	160 160	6	0.0
25-Mar	600	42.0	40.5	38.7	36.6	90	2 7	0.0
25-Mar	700	53.9	46.4	44.8	39.6	90	7	0.0
25-Mar	800	60.7	52.0	50.0	39.6	80	11	0.0
25-Mar	900	58.5	49.3	46.6	37.3	70	7	0.0
25-Mar	1000	60.4	49.7	48.5	39.9	70	7	0.0
25-Mar	1100	59.7	48.7	47.9	39.9	50	6	0.0
25-Mar	1200	64.3	49.0	47.0	41.4	120	4	0.0
25-Mar	1300	61.8	49.4	49.3	43.2	330	7	0.0
25-Mar	1400	59.5	50.1	49.0	44.7	220	17	0.0
25-Mar	1500	57.9	50.5	49.1	46.5	240	15	0.0
25-Mar	1600	60.9	51.7	51.5	47.3	230	17	0.0
25-Mar	1700	64.0	54.4	52.4	49.4	230	17	0.0
25-Mar	1800	59.2	54.0	51.8	49.2	220	17	0.0
25-Mar	1900	61.3	51.5	49.5	46.9	200	17	0.0
25-Mar	2000	64.9	52.3	50.3	46.4	180	13	0.0
25-Mar	2100	62.0	49.5	47.5	44.7	190	13	0.0
25-Mar	2200	59.7	48.1	46.1	43.4	180	13	0.0
25-Mar	2300	54.2	46.7	44.7	40.2	170	9	0.0
25-Mar	0	47.8	43.9	40.8	35.9	160	4	0.0
26-Mar	100	48.1	43.3	39.8	33.6	170	7	0.0
26-Mar	200	50.7	44.4	41.0	32.7	190	2	0.0
26-Mar	300	48.9	43.4	39.6	31.4	180	9	0.0
26-Mar	400	50.4	44.3	40.5	32.5	180	6	0.0
26-Mar	500	50.5	47.2	43.9	37.4	170	7	0.0
26-Mar	600	59.8	50.4	48.9	43.8	160	4	0.0
26-Mar	700	59.3	53.3	52.4	48.9	170	7	0.0
26-Mar	800	59.8	55.1	51.9	47.9	160	13	0.0
26-Mar	900	60.0	48.4	48.9	40.1	140	9	0.0
26-Mar	1000	60.5	47.6	47.3	38.9	130	7	0.0
26-Mar	1100	59.9	50.0	48.2	40.2	230	13	0.0
26-Mar	1200	59.5	50.6	49.0	43.6	210	15	0.0
26-Mar	1300	57.5	51.4	49.6	47.0	200	15	0.0
26-Mar	1400	60.6	50.4	49.5	44.5	200	13	0.0
26-Mar	1500	60.1	52.4	51.1	47.3	240	15	0.0
26-Mar	1600	57.8	52.0	52.1	47.9	220	19	0.0
26-Mar	1700	63.5	54.7	53.1	49.2	210	20	0.0
26-Mar	1800	64.7	53.7	51.7	48.1	210	17	0.0
26-Mar	1900	66.2	52.8	50.8	47.7	210	17	0.0
26-Mar	2000	60.3	51.8	50.4	46.2	200	11	0.0
26-Mar	2100	57.9	51.0	49.0	44.9	180	9	0.0
26-Mar	2200	54.3	50.1	48.1	45.3	180	7	0.0
26-Mar	2300	57.6	49.1	48.0	45.2	0	0	0.0
26-Mar	0	59.5	47.1	45.4	37.5	0	0	0.0

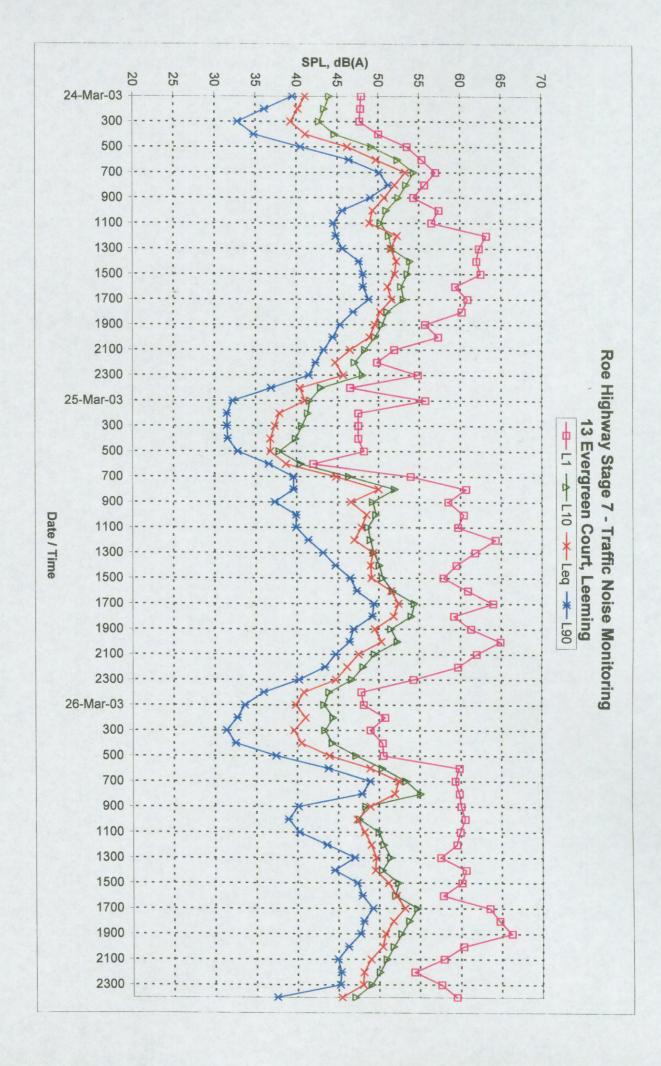


Location H3 - View of Logger Location



Location H3 - View Towards Future Road

Job No. 03107-1-2



## **APPENDIX C**

PREDICTED NOISE LEVELS TO RESIDENCES
SINGLE POINT CALCULATIONS

Roe7 Results.xls / Roe7\_L10(18hour) / Page 1

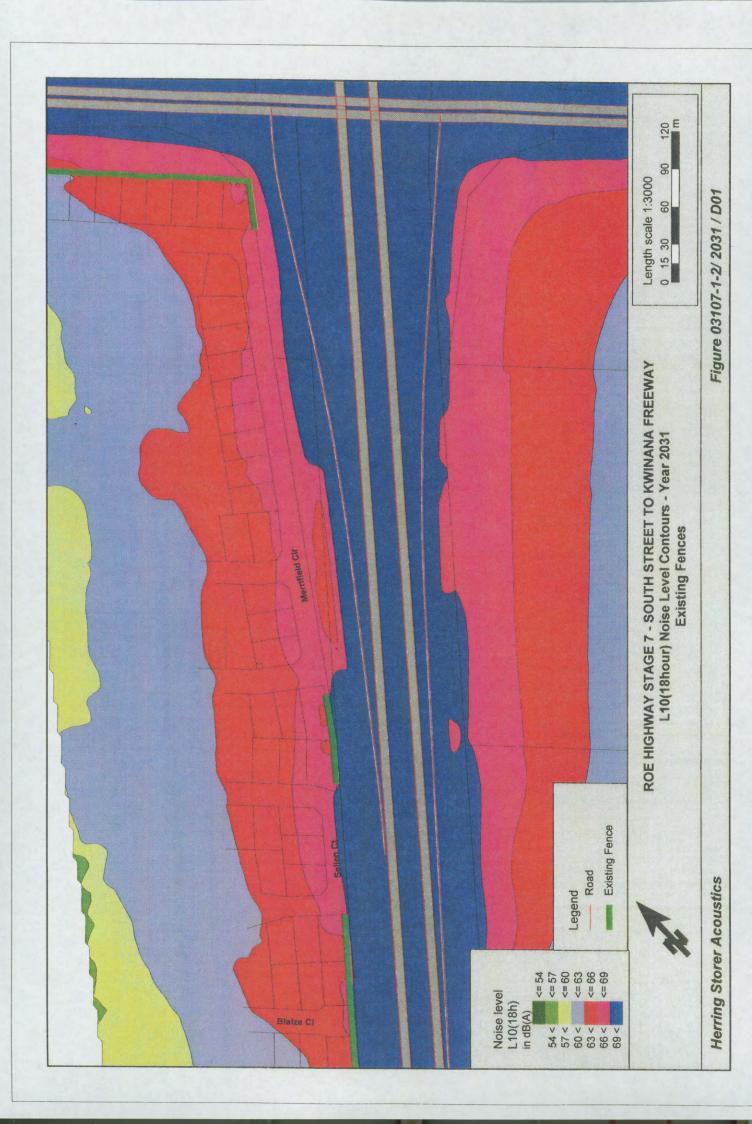
H	H
2	63.2
0	2.0
9	3.6
00 00	63.9
0 80	833
6	8.9
1	69.1
4	68.4
9	9.7
8	7.8
3	7.3
9	7.6
2	67.2
2	7.2
2	66.2
9	7.6
6	3.9
7	3.7
9	61.6
0	2.0
9	3.6
6	1.9
0	62.0
2	4.2
6	5.9
2	6.2
7	6.7
5	6.5
80	4.8
7	2.69
+   0	7.0
7	66.7
. 00	4.8
6	4.9
2	65.2
0	4.0
0	7.0
4	7.4
6	67.9
9	8.6
9	68.6
5	68.5
9	62.6
9	61.6
0	61.0
9	88
0 0	00.00 GE 2
5	5.0
7	7.7
2	67.2
3	67.3
9	9.99
9	9.99
20 0	8.9
2	662
	1.0

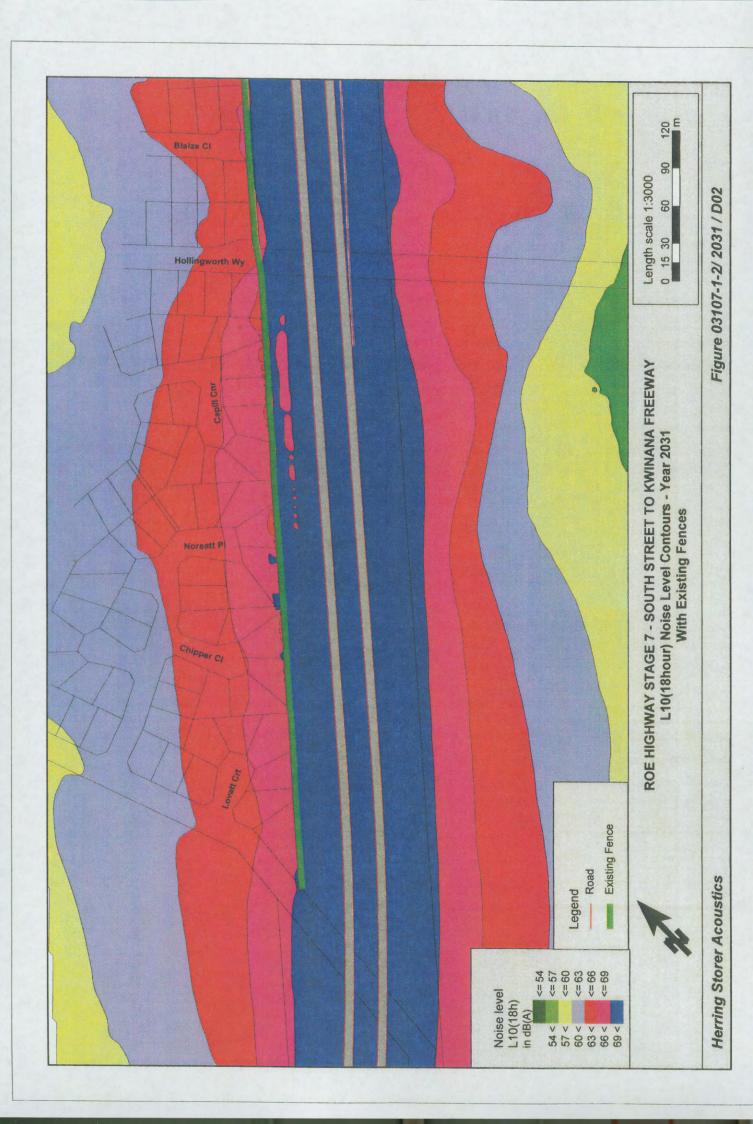
CD	
7.5	
S	
-	
CO	
0,	
-	
_	
0	
()	
0	
ACOL	
4	
Store	
(1)	
-	
_	
-	
CO	
0,	
-	
0,	
pros	
han	
-	
home	
41	
Herri	
_	
7	
-	

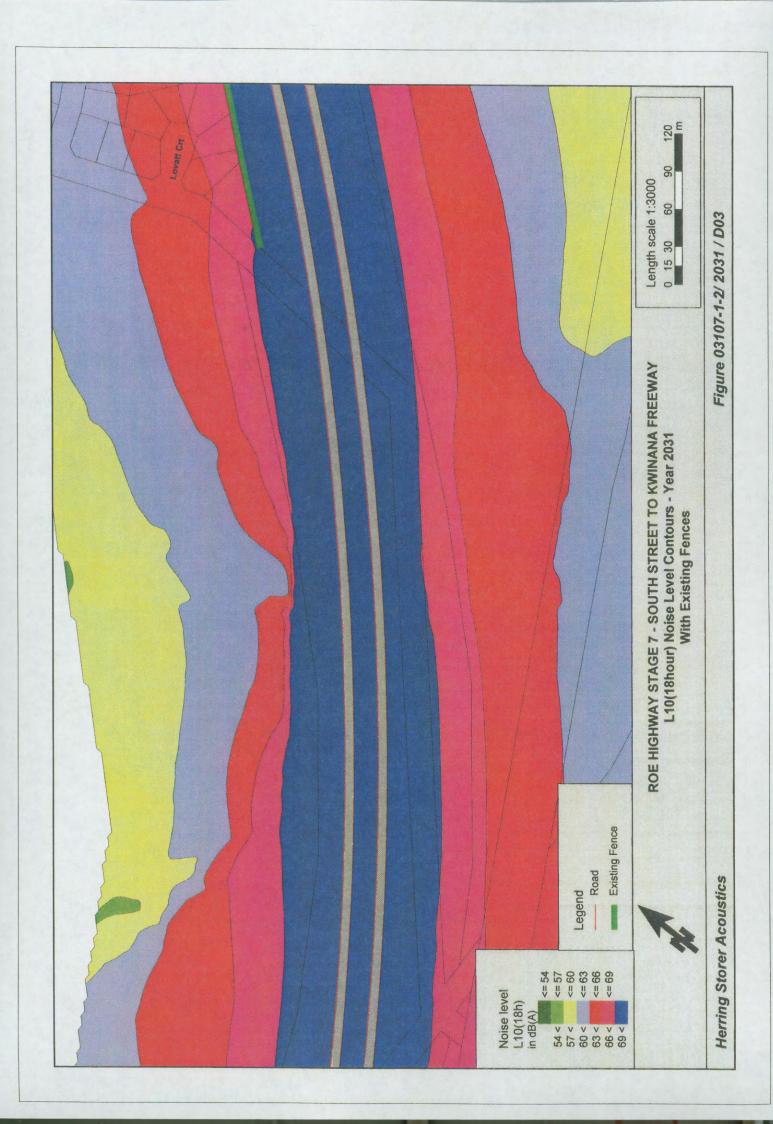
Method Circle         Light Rauny         Light Rauny	ONO	2011	2031	70.11	203	1107	2024	2044	PC-UC-
Memmed Circle         616A)         616A		L10(18hour)	L10(18hour)	L10(18hour)	L10(18hour)	L10(18hour)	L10(18hour)	1 40/48hour)	110/18hour
Meminded Cricle         61.5         66.9         1.2         60.9         62.2         69.9           Meminded Cricle         61.5         66.2         1.5         6.0         6.0         6.0         6.0           Meminded Cricle         65.4         66.2         1.5         2.6         6.0         6.0         6.0         6.0           Meminded Cricle         61.0         66.2         1.5         2.6         6.0			dB(A)	dB(A)	dB(A)	dB(A)	dB(A)	dR/A)	dR(A)
Memminded Circle         60.4         66.8         2.0         3.5         60.5         61.8         60.6           Memminded Circle         66.4         66.5         1.5         2.5         60.9         61.9         61.9         60.6           Memminded Circle         66.5         1.5         2.3         61.9         61.9         61.9         60.9           Memminded Circle         66.3         1.5         2.3         61.9         61.9         61.9         61.9           Memminded Circle         60.3         66.0         1.8         1.6         61.9         61.9         61.9           Memminded Circle         60.3         66.0         1.8         1.6         61.9         61.9         61.9           Memminded Circle         61.3         66.2         1.8         3.2         61.9         61.9         61.9           Memminded Circle         61.3         66.2         1.8         3.2         61.9         61.9         61.9         61.9           Memminded Circle         61.3         66.2         1.2         3.2         61.9         61.9         61.9         61.9         61.9         61.9           Memminded Circle         61.3         66.2			65.0		2.0	60.8	62.2	60.7	62 4
Memminde Circle         65.0         65.0         75.0         75.0         65.0			64.8		1.8	60.5	618	808	61.0
Memiliad Circle         64.5         6.6         1.5         2.6         6.19         6.3         6.2           Memiliad Circle         65.9         6.5         1.5         2.0         61.9         62.9         62.9           Memiliad Circle         65.9         6.6         0.9         2.0         61.9         61.9         62.9           Memiliad Circle         65.9         6.6         0.9         1.6         61.9         61.9         61.9           Memiliad Circle         62.2         6.0         1.8         1.6         61.9         61.9         61.9           Memiliad Circle         64.2         60.2         1.6         6.0         61.9         61.9         61.9         61.9           Memiliad Circle         64.3         60.2         1.5         2.0         61.9<			66.2	2.0	3.2	59.9	610	80.8	6.10
Mermind Circle         643         653         12         23         620         623         621         622         621 <t< td=""><td></td><td></td><td>929</td><td>1.5</td><td>2.6</td><td>61.9</td><td>63.1</td><td>62.3</td><td>63.5</td></t<>			929	1.5	2.6	61.9	63.1	62.3	63.5
Mermind Crole         63.0         0.9         2.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0         61.9         62.0			65.3	1.2	2.3	62.0	63.2	62.7	63.3
Mernified Circle         646         0.6         1.6         61.8         67.9         67.0           Mernified Circle         68.1         64.1         1.8         5.5         5.9         5.0         67.1           Mernified Circle         68.1         64.1         1.8         3.5         5.9         5.9         67.1         67.1           Mernified Circle         67.2         68.2         1.8         3.5         5.9         67.1         60.3         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1			65.0	6.0	2.0	61.9	63.0	610	63.0
Meminded Circles         64.8         66.5         1.8         3.5         5.9         5.9         5.7           Meminded Circles         63.2         66.2         66.2         67.2         67.2         67.1         67.1           Meminded Circles         62.0         62.2         62.2         62.2         67.2			64.6	0.6	1.6	618	62.0	61.0	03.0
Merminded Circles         62.1         64.1         1.1         61.4         62.2         67.1           Merminded Circles         62.2         62.2         64.1         67.2         65.2         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.1         67.2 <th< td=""><td></td><td></td><td>66.5</td><td>1.8</td><td>3.5</td><td>57.9</td><td>50.5</td><td>67.0</td><td>60.2</td></th<>			66.5	1.8	3.5	57.9	50.5	67.0	60.2
Merrified Circle         62.2         62.2         62.2         62.2         62.3         Merrified Circle         61.4         60.3         61.4         60.3           Merrified Circle         64.4         66.2         1.5         3.5         57.6         59.3         61.4         60.0           Merrified Circle         64.8         66.5         1.5         3.2         57.6         59.3         57.6         59.0         57.7         60.0         57.7         60.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0         57.7         59.0<			64.1		11	614	62.5	07.0	20.7
Merrified Circle         62.0         62.0         62.0         62.0         62.0         62.0         Merrified Circle         64.8         66.2         1.8         3.5         69.3         61.1         60.0         61.1         60.0         61.1         60.0         61.2         60.0         61.2         60.0         61.2         60.0         61.2         61.2         62.0         61.2         62.0         61.0         62.0 <th< td=""><td></td><td></td><td>63.2</td><td></td><td></td><td>60.3</td><td>614</td><td>603</td><td>64.4</td></th<>			63.2			60.3	614	603	64.4
Merrified Circle         61.4         66.2         1.6         63.5         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.7         69.2         67.7         69.2         67.7         69.2         67.7         69.2         67.7         69.2         67.7         69.2         67.7         69.2         67.7         67.7         69.2         67.7         67.2         67.2         67.2         67.2         67.2         67.2         67.2			62.9			0 09	611	6000	61.4
Mertified Circle         64.8         66.5         1.8         3.5         57.8         50.5           Mertified Circle         64.3         66.5         1.5         3.2         57.6         50.5           Mertified Circle         64.3         66.0         1.5         3.2         57.6         57.6         57.7           Mertified Circle         65.0         66.7         2.0         3.7         61.3         60.2         57.7           Mertified Circle         65.0         66.7         2.0         3.7         61.3         67.2         67.2           Mertified Circle         65.0         67.3         2.2         3.8         6.0         67.2         67.2           Noveate Part         66.2         67.3         6.0         67.2         6.0         67.2         67.2           Noveate Part         66.2         67.0         4.3         6.0         67.2			62.3			593	60.4	60.0	604
Mertified Circle         64.5         66.0         1.5         3.2         57.6         56.2           Mertified Circle         64.5         66.0         1.5         3.0         57.9         56.2         57.5           Mertified Circle         64.6         66.2         2.0         3.7         6.0         5.0         57.5           Mertified Circle         65.0         66.7         2.0         3.7         6.0         6.0         56.7           Mertified Circle         65.0         66.7         2.0         3.7         6.0         6.0         56.7         56.7           Moreatif Pl.2         67.0         66.0         4.3         6.0 </td <td>1</td> <td></td> <td>66.5</td> <td>1.8</td> <td>3.5</td> <td>57.8</td> <td>50.5</td> <td>57.4</td> <td>600.4</td>	1		66.5	1.8	3.5	57.8	50.5	57.4	600.4
Merinded Circle         64.3         66.0         13         3.0         57.7         9.6         0.0           Merinded Circle         64.0         66.0         1.3         3.0         67.7         60.9         50.9           Merinded Circle         65.0         66.7         2.0         3.7         60.9         60.9         58.2           Merinded Circle         65.0         66.7         2.0         3.7         60.9         62.9         58.7           Merinded Circle         65.0         66.7         2.2         3.8         62.0         62.9         68.7           Norealt PLA         65.2         66.9         1.2         2.9         68.8         60.0         67.5           Norealt PLA         66.2         67.3         2.2         2.9         68.8         60.0         67.5           Norealt PLA         66.7         67.2         68.9         67.6         67.6         67.6         67.6           Norealt PLA         66.8         66.8         66.8         66.8         66.9         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         67.6         6			66.2	1.5	32	57.6	50.3	57.0	20.00
Mertinded Circle         64.6         66.3         1.6         3.3         69.2         60.0         65.2           Mertinded Circle         65.0         66.7         2.0         3.7         61.3         67.2         55.2           Mertinded Circle         65.0         66.7         2.0         3.7         61.3         62.2         63.2           Noreate Pri 2         65.2         66.2         62.2         65.0         61.2         65.2         61.1           Noreate Pri 2         65.2         65.0         12.2         6.0         61.2         65.2         61.1           Noreate Pri 2         65.2         65.0         61.2         65.0         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.2         62.2         61.1         61.1         61.1         61.2         62.2         61.1         61.1         61.2         62.2         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61.1         61			0.99	1.3	3.0	57.9	59.6	57.5	50.7
Merinded Circle         650         667         20         37         605         605         602         602         602         602         602         602         602         602         602         602         602         602         602         602         602         602         602         602         602         603         <			66.3	16	33	50.0	0.00	0.70	2.60
Metrified Cricle         65.0         66.7         2.0         37         67.3         62.2         53.4           Metrified Cricle         65.0         66.2         66.2         66.2         66.2         65.0         63.5         61.1           Noreath PL         67.3         62.2         4.3         6.0         62.0         62.0         61.1           Noreath PL         67.3         65.0         4.3         6.0         61.2         62.0         61.1           Noreath PL         67.3         65.0         65.0         65.0         67.0 <t< td=""><td></td><td></td><td>66.7</td><td>20</td><td>3.7</td><td>60.8</td><td>60.9</td><td>2.00</td><td>58.8</td></t<>			66.7	20	3.7	60.8	60.9	2.00	58.8
Morental Cricle         66.2         66.8         2.2         3.8         62.0         63.5         63.1           Norealt P1         65.6         67.3         4.3         67.2         62.9         63.9         61.2           Norealt P1         65.6         67.3         6.5         4.3         61.2         62.9         60.6           Norealt P1         67.2         65.9         1.2         5.9         66.3         60.0         87.5           Norealt P1         66.9         68.9         1.2         2.9         68.3         60.0         87.5           Rankwood         61.2         68.9         1.8         5.9         68.9         62.0         88.7           Sellen C1.2         66.9         2.1         8.9         60.0         67.1         67.0           Sellen C1.2         66.3         2.2         3.9         60.0         67.0         88.7           Sellen C1.2         66.3         2.2         3.9         60.0         67.0         88.7           Sellen C1.2         66.3         2.2         3.9         60.0         61.7         68.7           Sellen C1.2         66.3         2.2         3.9         60.0 <t< td=""><td></td><td></td><td>7 99</td><td>20</td><td>3.7</td><td>613</td><td>62.0</td><td>29.7</td><td>60.3</td></t<>			7 99	20	3.7	613	62.0	29.7	60.3
Moreatt P1         656         673         2.6         43         612         623         611           Noreatt P1         673         683         4.3         6.0         60.2         61.9         61.9         61.9           Noreatt P1         673         663         4.3         6.0         60.2         61.9         69.7           Noreatt P1         66.9         4.3         6.0         60.4         62.1         69.7           Randwood         58.7         68.9         66.5         6.6         6.0         60.1         67.1           Randwood         58.7         68.3         67.0         2.3         60.9         60.1         67.8           Sellen C1         66.3         67.0         2.3         4.0         60.9         67.8         66.6           Sellen C1         66.3         67.0         2.3         4.0         60.9         67.0         68.4           Sellen C1         66.3         67.0         2.3         4.0         60.0         67.1         68.7           Sellen C1         66.3         67.0         2.3         4.0         60.0         67.1         68.7           Sellen C1         66.3         6			899	22	3.00	62.0	62.5	29.7	4.10
Noreatt P12         673         689         4.3         60         60.2         67.2         60.9         60.1         60.2         60.9         60.1         <			67.3	2.5	43	64.2	03.5	61.1	62.7
Noreatt P13         64.2         65.9         17.2         2.0         68.7         69.4         69.1         59.1           Noreatt P14         66.9         68.6         3.9         5.6         60.4         60.1         67.1         69.1           Randwood         68.7         61.8         3.9         5.6         60.4         60.1         67.1         69.3           Selfen Ct1         64.8         66.5         1.8         3.6         60.3         60.0         60.1         61.2         61.2           Sollen Ct1         66.3         66.6         2.1         3.8         60.1         67.0         68.8           Sollen Ct2         66.3         67.0         2.3         4.0         60.1         61.7         68.8           Sollen Ct4         66.3         67.0         2.3         4.0         60.1         67.3         68.0           Sollen Ct4         66.3         67.0         2.3         4.0         60.1         67.2         68.2           Sollen Ct4         66.3         67.0         2.3         4.0         60.1         67.2         66.0           Sollen Ct4         66.1         67.1         67.1         67.2         67.2<		673	69.0	43	6.4	2.10	6.79	9.09	62.3
Noreatt P14         666 3         666 3         656 4         657 5         657 5           Randwood         587 618         618         3         56 601         541         591           Randwood         587 618         618         3         661         541         591           Randwood         612         663         18         35         601         541         593           Randwood         612         668         18         66         23         569         543           Sellen C1         648         668         21         3         601         618         584           Sellen C1         663         670         23         40         600         617         587           Sellen C1         663         670         22         39         600         617         587           Sellen C1         662         22         39         600         613         587           Sellen C1         663         61         621         623         601         623         578           Stone Court 2         610         621         623         601         623         614         578           S	1	642	65.0	1.3	0.0	200.2	61.9	59.7	61.4
Randwood         597         618         59         59         59         59         59         59         58         48         601         621         543         693         621         683         684         685         683         684         685         683         684         685         683         684         683         683         684         683         683         683         683		2.50	68.6	3.0	6.7	58.3	0.09	57.5	59.2
Randwood         357         618         661         541           Randwood         612         618         661         541           Randwood         612         613         618         661         661           Randwood         612         663         633         603         644           Sellen Ct2         664         665         668         21         38         603         618         664           Sellen Ct3         665         669         23         40         600         613         587           Sellen Ct4         665         669         22         39         60         613         68           Sellen Ct4         665         669         22         39         60         613         68           Sellen Ct4         665         669         22         39         60         61         62           Sellen Ct4         665         669         22         39         60         61         62           Sellen Ct4         661         623         623         67         60         61         61         62           Slywan Ct4         610         623         623         6		600.3	64.0	3.8	9.6	60.4	62.1	59.3	61.0
Randwood         612         613         61         62         61         62         61         62         61         62         62         62         62         62         62         62		50.7	610			58.0	60.1	54.1	56.2
Sellen Ct 2         64.8         66.8         1.8         3.5         60.8         54.6           Sellen Ct 2         66.1         66.8         2.1         3.8         60.1         60.8         54.6           Sellen Ct 3         66.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen Ct 3         66.3         67.0         2.3         4.0         60.0         61.7         58.6           Sellen Ct 4         66.3         67.0         2.3         4.0         60.0         61.7         58.0           Sellen Ct 4         66.3         67.0         2.3         4.0         60.0         61.3         58.0           Sellen Ct 4         66.3         66.3         67.0         2.3         4.0         60.0         61.3         58.0           Stone Court 5         61.1         63.1         67.1         63.1         67.2         67.5         59.5         61.1         58.7           Stone Court 5         61.1         63.1         66.3         66.3         66.3         66.3         66.1         67.2         67.2         67.2         67.2         67.2         67.2         67.2         67.2         67.2		64.2	01.0			57.8	59.9	53.9	56.0
Sollar CL21         65.4         66.0         61.0         62.0         65.4           Sellen CL3         66.1         66.3         66.0         61.7         56.4           Sellen CL3         65.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen CL4         65.3         67.0         2.3         4.0         60.0         61.7         58.2           Sellen CL4         65.3         67.0         2.3         4.0         60.0         61.7         58.2           Solvan CL1         61.1         63.1         63.1         66.0         61.5         56.0           Sylvan CL1         61.0         67.0         1.9         4.0         60.0         67.2         57.6           Sylvan CL1         61.0         65.7         0.6         2.7         60.0         62.2         67.0           Sylvan CL1         63.6         64.7         0.6         2.7         60.1         62.2         67.5           Sylvan CL3         61.2         63.3         64.7         0.6         2.7         60.1         62.2         67.5           Sylvan CL3         61.3         63.5         0.6         63.2 <td< td=""><td></td><td>2.10</td><td>03.3</td><td></td><td></td><td>58.7</td><td>8.09</td><td>54.6</td><td>26.7</td></td<>		2.10	03.3			58.7	8.09	54.6	26.7
Sellen Ct, 4         65.3         67.0         2.1         3.8         60.1         61.8         58.8           Sellen Ct, 4         65.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen Ct, 4         65.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen Ct, 4         65.2         66.9         2.2         3.9         60.0         61.7         58.7           Solvan Ct, 1         61.0         61.5         61.5         65.0         61.5         65.0           Shyan Ct, 1         63.8         65.9         0.8         2.9         60.1         62.2         67.6           Sylvan Ct, 1         63.8         65.9         0.8         2.9         60.1         62.2         67.6           Sylvan Ct, 1         63.8         65.7         0.6         2.7         60.1         62.2         67.8           Sylvan Ct, 2         61.2         63.5         0.6         2.7         60.1         62.2         62.6           Sylvan Ct, 3         61.3         63.5         0.7         60.1         62.2         62.2           Sylvan Ct         61.3         63.5 </td <td></td> <td>04.0</td> <td>6.00</td> <td>1.8</td> <td>3.5</td> <td>60.3</td> <td>62.0</td> <td>56.4</td> <td>58.1</td>		04.0	6.00	1.8	3.5	60.3	62.0	56.4	58.1
Sellen Ct 4         66.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen Ct 4         66.3         67.0         2.3         4.0         60.0         61.7         58.7           Sellen Ct 6         66.3         66.9         2.2         3.9         60.6         62.3         59.2           Sellen Ct 6         66.3         66.9         2.2         3.9         60.6         62.3         59.0           Stone Court 1         61.0         61.1         63.1         1.9         4.0         60.6         62.3         59.0           Stone Court 2         61.0         63.1         1.9         4.0         60.6         62.3         59.0           Stylvan Cr 10         64.9         67.0         1.9         4.0         60.9         62.9         67.1           Sylvan Cr 12         65.6         65.7         0.6         2.7         60.5         62.2         67.5           Sylvan Cr 13         62.7         64.3         1.7         60.4         62.4         56.2           Sylvan Cr 2         61.3         62.3         63.3         63.3         62.3         66.2           Sylvan Cr 3         61.3<		65.1	8.99	2.1	3.8	60.1	61.8	58.8	60.5
Sellent Ct 4         66.3         67.0         2.3         4.0         59.6         61.3         58.2           Sellent Ct 4         66.3         66.9         2.2         3.9         60.6         61.3         58.0           Slone Court 1         66.1         61.1         63.1         63.5         61.5         56.2           Slone Court 2         61.1         63.1         63.6         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.0         61.1         56.0         61.1         56.0         61.1         56.0         61.1         56.0         61.0         62.0		65.3	0.79	2.3	4.0	0.09	61.7	58.7	60.4
Solue Cut         652         669         2.2         3.9         606         62.3         59.0           Solue Court         61.5         61.5         6.1         6.1         6.1         6.1         6.0         6.2         6.0		65.3	0.79	2.3	4.0	59.6	61.3	58.2	59.9
Stone Court 1         59.5         61.5         56.6           Stone Court 2         61.1         63.1         61.5         56.6           Stone Court 2         61.1         63.1         63.1         57.6         59.5         61.1           Stone Court 2         61.0         63.1         1.9         4.0         60.9         62.9         61.4         55.7           Sylvan Cr 1         63.8         65.9         0.6         62.9         60.1         62.9         67.5           Sylvan Cr 1         63.6         64.3         0.6         62.7         60.4         62.4         56.2           Sylvan Cr 2         61.2         63.3         64.3         60.5         62.4         56.2           Sylvan Cr 3         61.3         63.5         64.3         60.5         62.4         56.2           Sylvan Cr 4         61.3         63.5         64.5         60.1         62.2         56.2           Sylvan Cr 5         61.3         63.5         64.5         60.7         60.1         62.2         56.2           Sylvan Cr 6         62.3         64.5         63.6         62.1         60.1         62.1         56.2           Sylvan Cr 8		65.2	6.99	2.2	3.9	9.09	62.3	59.0	2 09
Sylvan Crif         61.1         63.1         63.1         61.1         63.1         61.2         61.1         61.2         61.1         61.2		59.5	61.5			59.5	61.5	56.6	58.5
Sylvan Cr1         61.0         63.1         1.9         4.0         69.2         61.4         55.7           Sylvan Cr1         64.9         67.0         1.9         4.0         60.9         62.9         57.8           Sylvan Cr1         63.8         65.7         0.6         2.7         60.5         62.2         57.2           Sylvan Cr1         63.8         66.7         0.6         2.7         60.5         62.2         57.2           Sylvan Cr1         62.3         64.3         0.6         2.7         60.4         62.4         56.2           Sylvan Cr3         61.5         63.7         0.7         60.1         62.2         56.2           Sylvan Cr3         61.3         63.5         0.7         60.1         62.2         56.2           Sylvan Cr4         61.3         63.5         0.7         60.1         62.2         56.2           Sylvan Cr5         60.0         62.1         1.5         60.0         62.1         56.6           Sylvan Cr5         60.0         62.1         62.5         66.6         60.0         62.1         56.6           Sylvan Cr5         60.0         62.5         63.6         66.6 <td< td=""><td></td><td>61.1</td><td>63.1</td><td></td><td></td><td>57.6</td><td>59.5</td><td>61.1</td><td>63.0</td></td<>		61.1	63.1			57.6	59.5	61.1	63.0
Sylvan Cr 10         64.9         67.0         1.9         4.0         60.9         62.9         57.8           Sylvan Cr 11         63.8         65.9         0.8         2.9         60.1         62.2         57.8           Sylvan Cr 12         63.6         65.7         0.6         2.7         60.5         62.6         57.2           Sylvan Cr 13         62.7         64.7         0.6         6.0         62.4         56.2           Sylvan Cr 14         62.3         64.3         7         60.5         62.4         56.2           Sylvan Cr 2         61.5         63.3         63.5         61.6         62.4         56.2           Sylvan Cr 3         61.5         63.5         64.5         60.0         62.1         56.2           Sylvan Cr 4         61.3         63.5         64.5         60.0         62.1         56.2           Sylvan Cr 5         61.3         64.5         62.1         60.0         62.1         56.6           Sylvan Cr 6         62.3         64.5         62.6         62.5         60.0         62.3         66.6           Sylvan Cr 7         66.3         66.6         62.7         60.9         62.3         62		61.0	63.1			59.2	61.4	55.7	57.9
Sylvan Cr 12         63.8         66.9         0.8         2.9         60.1         62.2         67.5           Sylvan Cr 12         63.6         66.7         0.6         2.7         60.5         62.2         67.5           Sylvan Cr 13         62.3         64.3         0.6         2.7         60.5         62.4         56.6           Sylvan Cr 14         62.3         64.3         1.3         60.5         62.4         56.2           Sylvan Cr 2         61.2         63.3         0.7         60.1         62.2         56.2           Sylvan Cr 3         61.5         63.5         0.7         60.1         62.2         56.2           Sylvan Cr 6         62.3         64.5         0.7         60.1         62.2         56.1           Sylvan Cr 6         62.3         64.5         0.7         60.4         62.2         56.1           Sylvan Cr 6         62.3         64.5         0.6         62.5         56.6         56.1           Sylvan Cr 7         60.0         62.1         62.5         60.4         62.5         56.6           Sylvan Cr 8         62.5         64.5         3.3         5.5         60.8         57.1		64.9	0.79	1.9	4.0	6.09	62.9	57.8	59.9
Sylvan Cr 12         63.6         65.7         0.6         2.7         60.5         62.6         57.2           Sylvan Cr 13         62.7         64.7         1.7         60.4         62.4         56.6           Sylvan Cr 14         62.3         64.3         1.3         60.5         62.4         56.2           Sylvan Cr 1         61.2         63.3         0.7         60.1         62.2         56.2           Sylvan Cr 2         61.3         63.5         0.7         60.1         62.2         56.2           Sylvan Cr 4         61.3         63.5         64.5         64.5         60.0         62.1         56.1           Sylvan Cr 5         60.0         62.1         60.0         62.1         56.1         56.6           Sylvan Cr 6         62.5         64.5         64.5         64.5         60.9         62.5         56.6           Sylvan Cr 8         61.5         63.6         1.7         59.7         61.7         56.6           Sylvan Cr 9         62.6         64.7         3.3         5.5         60.8         62.9         57.9           Tana Crt 1         66.3         66.6         1.5         66.9         60.8         62.9		63.8	62.9	0.8	2.9	60.1	62.2	57.5	59 6
Sylvan Cr 13         62.7         64.7         1.7         60.4         62.4         56.6           Sylvan Cr 14         62.3         64.3         1.3         60.5         62.4         56.2           Sylvan Cr 2         61.2         63.3         67.2         60.1         62.2         56.2           Sylvan Cr 3         61.3         63.5         63.5         62.2         56.2         56.2           Sylvan Cr 4         61.3         63.5         63.5         62.2         56.2         56.2           Sylvan Cr 5         61.3         64.5         62.1         60.0         62.1         56.1           Sylvan Cr 9         62.3         64.5         64.7         60.0         62.5         56.6           Sylvan Cr 9         62.6         64.7         1.7         59.7         61.7         56.7           Sylvan Cr 9         62.5         64.7         66.8         62.3         66.7         62.2         56.6           Sylvan Cr 9         66.3         66.5         1.7         59.7         61.7         56.7           Ima Crt 1         66.3         66.5         1.5         60.8         62.5         57.9           Ima Crt 2 <td< td=""><td></td><td>63.6</td><td>65.7</td><td>0.6</td><td>2.7</td><td>60.5</td><td>626</td><td>57.2</td><td>59.2</td></td<>		63.6	65.7	0.6	2.7	60.5	626	57.2	59.2
Sylvan Cr 14         62.3         64.3         1.3         60.5         62.4         56.2           Sylvan Cr 2         61.2         63.3         63.7         60.1         62.2         56.8           Sylvan Cr 3         61.5         63.5         63.5         66.2         56.2         56.2           Sylvan Cr 4         61.3         63.5         63.5         64.5         60.1         62.1         56.2           Sylvan Cr 5         61.3         64.5         64.5         60.0         62.1         56.7           Sylvan Cr 6         62.3         64.5         62.1         56.7         56.6           Sylvan Cr 6         62.0         62.1         60.9         62.1         56.6           Sylvan Cr 7         60.0         62.1         60.9         56.6         56.6           Sylvan Cr 8         61.5         64.7         63.6         60.1         62.3         56.6           Sylvan Cr 8         61.5         64.7         3.3         5.5         60.1         62.3         56.6           Sylvan Cr 9         66.3         64.5         3.3         5.5         60.8         62.6         57.9           Tana Crt 1         66.3         <		62.7	64.7		1.7	604	62.4	56.6	58.6
Sylvan Cr2         61.2         63.3         61.2         63.3         61.5         61.6         55.8           Sylvan Cr3         61.5         63.7         63.7         60.1         62.2         66.2           Sylvan Cr4         61.3         63.5         63.5         60.0         62.1         66.2           Sylvan Cr5         61.3         64.5         60.0         62.1         56.1           Sylvan Cr6         62.3         64.5         60.0         62.5         56.6           Sylvan Cr7         60.0         62.1         60.9         55.6         56.7           Sylvan Cr8         61.5         63.6         64.7         60.9         56.7         56.7           Sylvan Cr8         62.6         64.7         1.7         60.9         56.7         56.6           Sylvan Cr8         62.6         64.7         1.7         59.7         61.7         56.6           Sylvan Cr9         66.3         68.5         33.3         5.5         60.8         62.2         57.9           Tana Crt 2         64.5         66.6         1.5         66.8         62.6         57.1           Tana Crt 3         62.7         64.9         62.2 <td></td> <td>62.3</td> <td>64.3</td> <td></td> <td>6.1</td> <td>60.5</td> <td>62.4</td> <td>56.2</td> <td>58.3</td>		62.3	64.3		6.1	60.5	62.4	56.2	58.3
Sylvan Cr 3         61.5         63.7         63.7         60.1         62.2         56.2           Sylvan Cr 4         61.3         63.5         63.5         63.5         60.1         62.2         56.2           Sylvan Cr 5         61.3         63.5         64.5         64.5         60.0         62.1         56.7           Sylvan Cr 6         62.3         64.5         62.1         60.0         62.5         56.6           Sylvan Cr 7         60.0         62.1         60.9         55.6         56.7           Sylvan Cr 9         62.6         64.7         63.6         60.1         62.3         56.7           Sylvan Cr 9         62.6         64.7         64.7         64.7         60.9         55.6           Sylvan Cr 9         62.6         64.7         66.6         1.7         59.7         61.7         56.6           Tana Crt 2         64.5         66.6         1.5         66.8         60.5         62.6         57.1           Tana Crt 3         62.7         64.9         1.5         60.5         62.5         56.9           Tetlow Place 2         60.4         62.2         60.4         62.1         62.9         62.9 <t< td=""><td></td><td>61.2</td><td>63.3</td><td></td><td></td><td>59 5</td><td>616</td><td>55.8</td><td>57.0</td></t<>		61.2	63.3			59 5	616	55.8	57.0
Sylvan Cr 4         61.3         63.5         63.5         60.1         62.2         56.2           Sylvan Cr 5         61.3         63.5         63.5         64.5         60.4         62.1         56.7           Sylvan Cr 6         62.3         64.5         62.1         60.4         62.5         56.6           Sylvan Cr 7         60.0         62.1         60.4         62.5         56.6           Sylvan Cr 8         61.5         64.7         0.6         60.1         62.3         56.7           Sylvan Cr 9         62.6         64.7         1.7         59.7         61.7         56.6           Sylvan Cr 9         66.3         68.5         3.3         5.5         60.8         62.3         57.9           Tana Crt 1         66.3         66.6         1.5         3.6         60.8         62.6         57.1           Tana Crt 2         64.9         1.5         3.6         60.5         62.6         57.1           Tetlow Place 1         61.7         63.0         61.1         63.0         62.5         56.9           Tetlow Place 2         60.4         62.2         60.8         62.1         62.9         62.9           Tet		61.5	63.7		07	60.1	62.2	56.7	50.2
Sylvan Cr 5         61.3         63.5         90.2         50.1         50.1         50.2		61.3	63.5			60.1	22.20	50.7	20.3
Sylvan Cr 6         62.3         64.5         1.5         60.4         62.5         56.6           Sylvan Cr 7         60.0         62.1         62.5         56.6           Sylvan Cr 8         61.5         63.6         60.9         55.6           Sylvan Cr 9         62.6         64.7         68.5         3.3         5.5         60.8         62.3         56.7           Tana Crt 1         66.3         66.6         1.5         3.6         60.8         62.9         57.9           Tana Crt 2         64.5         64.9         1.5         3.6         60.5         62.6         57.1           Tana Crt 3         62.7         64.9         60.5         62.6         57.1           Tana Crt 3         62.7         63.6         62.5         56.6           Tetlow Place 1         61.7         63.6         62.5         56.9           Tetlow Place 2         60.4         62.2         62.1         58.2           Tetlow Place 3         60.5         62.2         58.1           Tetlow Place 3         60.5         60.5         62.2         58.1		61.3	63.5			60.0	62.4	56.1	20.3
Sylvan Cr 7         60.0         62.1         70.0           Sylvan Cr 8         61.5         60.0         62.3         55.6           Sylvan Cr 8         61.5         63.6         64.7         60.9         55.6           Sylvan Cr 9         62.6         64.7         64.7         66.3         66.6         67.7         56.6           Tana Crt 1         66.3         66.6         1.5         3.3         5.5         60.5         62.9         57.1           Tana Crt 2         64.5         64.9         6.0         60.5         62.6         57.1         56.6           Tetlow Place 1         61.7         63.6         62.5         56.9         56.9           Tetlow Place 2         60.4         62.2         60.5         60.5         62.1         58.2           Tetlow Place 3         60.5         60.5         60.5         60.5         62.2         58.1		62.3	64.5		15	60.4	C2 E	20.1	200.2
Sylvan Cr 8         61.5         63.6         0.6         0.6         60.1         60.3         55.0           Sylvan Cr 8         61.5         63.6         64.7         63.6         62.3         56.7         56.6           Sylvan Cr 9         62.6         64.7         63.6         67.9         67.9         57.9         56.6           Tana Crt 2         64.5         66.6         1.5         3.6         60.5         62.6         57.9         57.1           Tana Crt 3         62.7         64.9         1.9         60.3         62.6         56.9         56.9<		60.0	62.1		0.1	00.4	0.20	20.00	28.7
Sylvan Cr 9         62.6         64.7         3.3         5.5         60.8         62.9         57.9           Tana Crt 2         66.3         68.5         3.3         5.5         60.8         62.9         57.9           Tana Crt 2         64.5         66.6         1.5         3.6         60.5         62.9         57.9           Tana Crt 3         62.7         64.9         1.9         60.5         62.5         56.6           Tetlow Place 1         61.7         63.6         62.5         56.9           Tetlow Place 2         60.4         62.2         60.4         62.1         58.2           Tetlow Place 3         60.5         60.5         60.5         62.2         58.1		61.5	63.6		30	20.7	6.09	55.6	57.7
Tana Crt 1         66.3         68.5         3.3         5.5         60.8         62.9         57.9           Tana Crt 2         64.5         66.6         1.5         3.6         60.5         62.6         57.1           Tana Crt 3         62.7         64.9         1.9         60.3         62.5         56.6           Tetlow Place 1         61.7         63.6         62.5         56.9         56.9           Tetlow Place 2         60.4         62.2         60.4         62.1         58.2           Tetlow Place 3         60.5         60.5         60.5         62.2         58.1		62.6	64.7		0.0	50.1	62.3	2007	58.8
Tana Crt 2         64.5         66.6         1.5         3.6         60.5         62.6         57.1           Tana Crt 3         62.7         64.9         1.9         60.5         62.6         57.1           Tetlow Place 1         61.7         63.6         62.5         56.9           Tetlow Place 2         60.4         62.2         60.4         62.1         58.2           Tetlow Place 3         60.5         62.2         60.5         62.2         58.1		663	68.5	22	1.1	29.7	00.0	20.6	58.6
Tana Crt 3         66.5         62.6         57.1           Tana Crt 3         62.7         64.9         1.5         3.6         60.5         62.6         57.1           Tetlow Place 1         61.7         63.6         62.5         56.9           Tetlow Place 2         60.4         62.2         60.4         62.1         58.2           Tetlow Place 3         60.5         62.2         60.5         62.2         58.1	1	645	000.0	0.0	5.0	8.09	67.9	57.9	60.1
Tetlow Place 2         60.5         62.5         56.6           Tetlow Place 3         61.7         63.6         62.5         56.9           Tetlow Place 3         60.4         62.1         58.2           Tetlow Place 3         60.5         62.2         58.1	1	04.3	0.00	1.5	3.6	60.5	62.6	57.1	59.3
Tellow Place 2         60.4         62.2         60.4         62.2         60.5         60.5         60.5         60.5         60.5         60.5         58.2	T		64.9		1.9	60.3	62.5	9.99	58.8
Tetlow Place 3 60.5 62.2 60.5 60.5 62.2 58.1	Totlow Place		63.6		9.0	61.1	63.0	6.99	58.6
Testinov Place 3 60.5 62.2 58.1			7.70			60.4	62.1	58.2	59.9
			1.1.3						

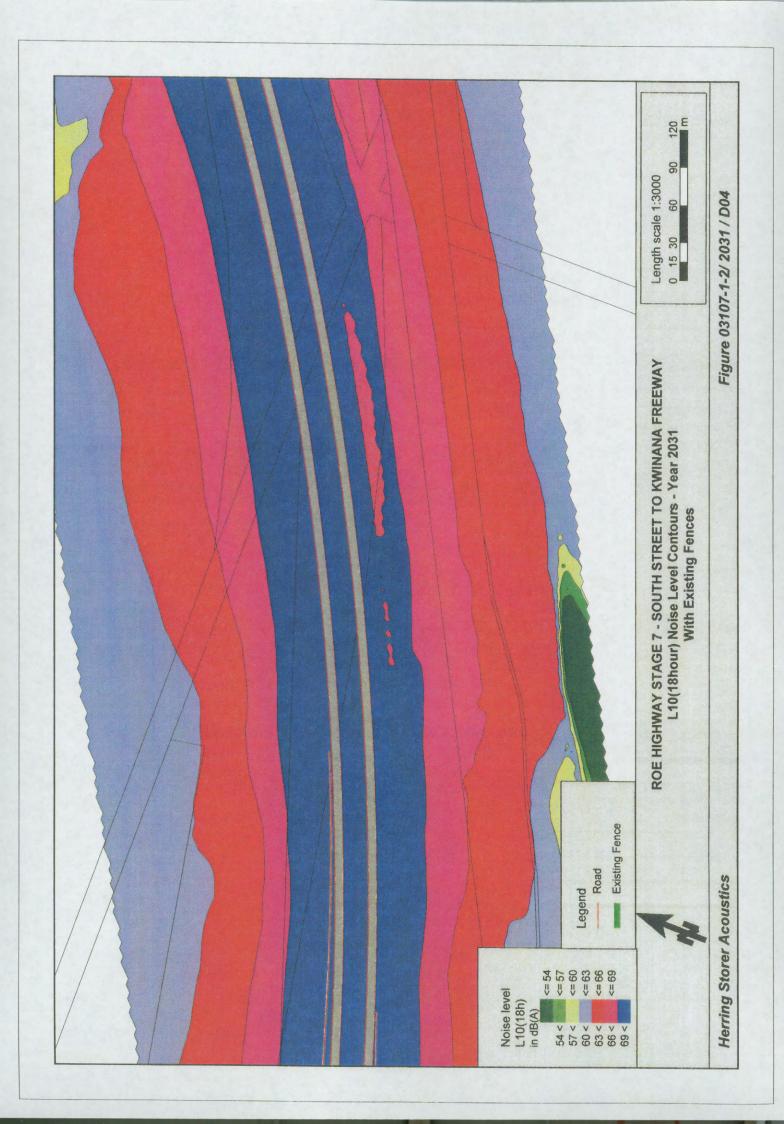
## **APPENDIX D**

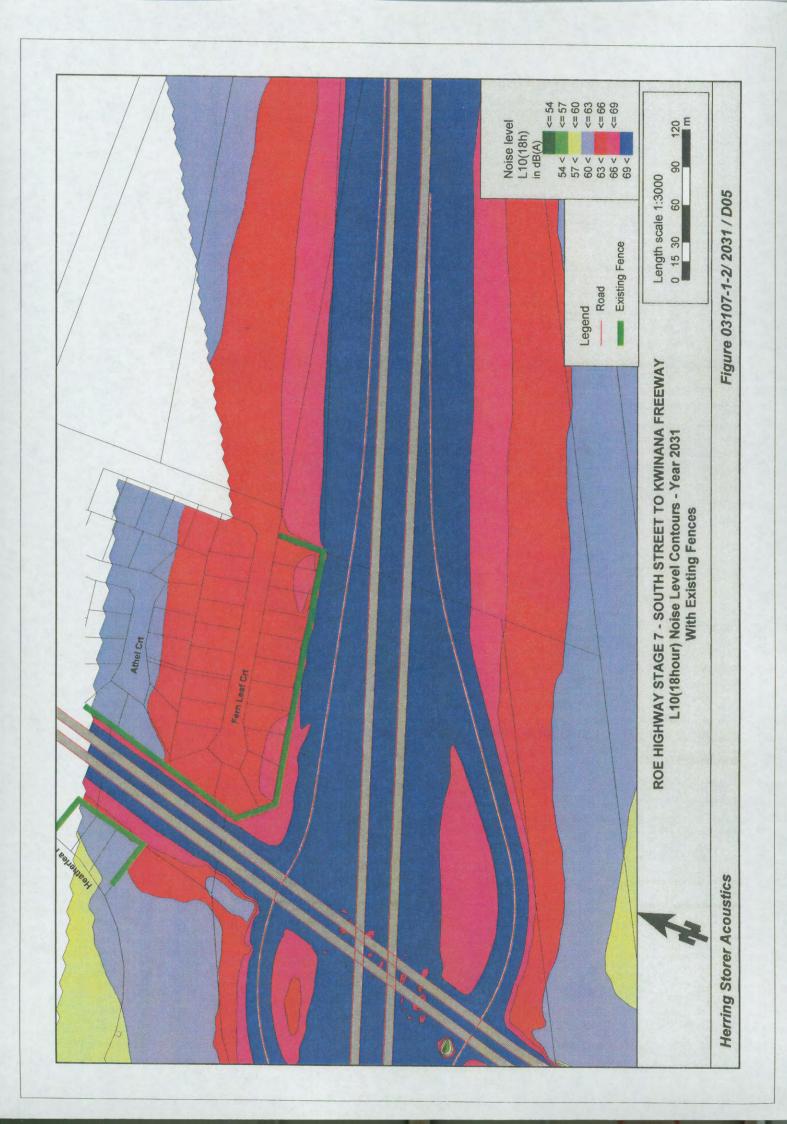
PREDICTED 2031 NOISE LEVELS TO SURROUNDING AREAS
- NOISE LEVEL CONTOUR PLOTS: EXISTING FENCES

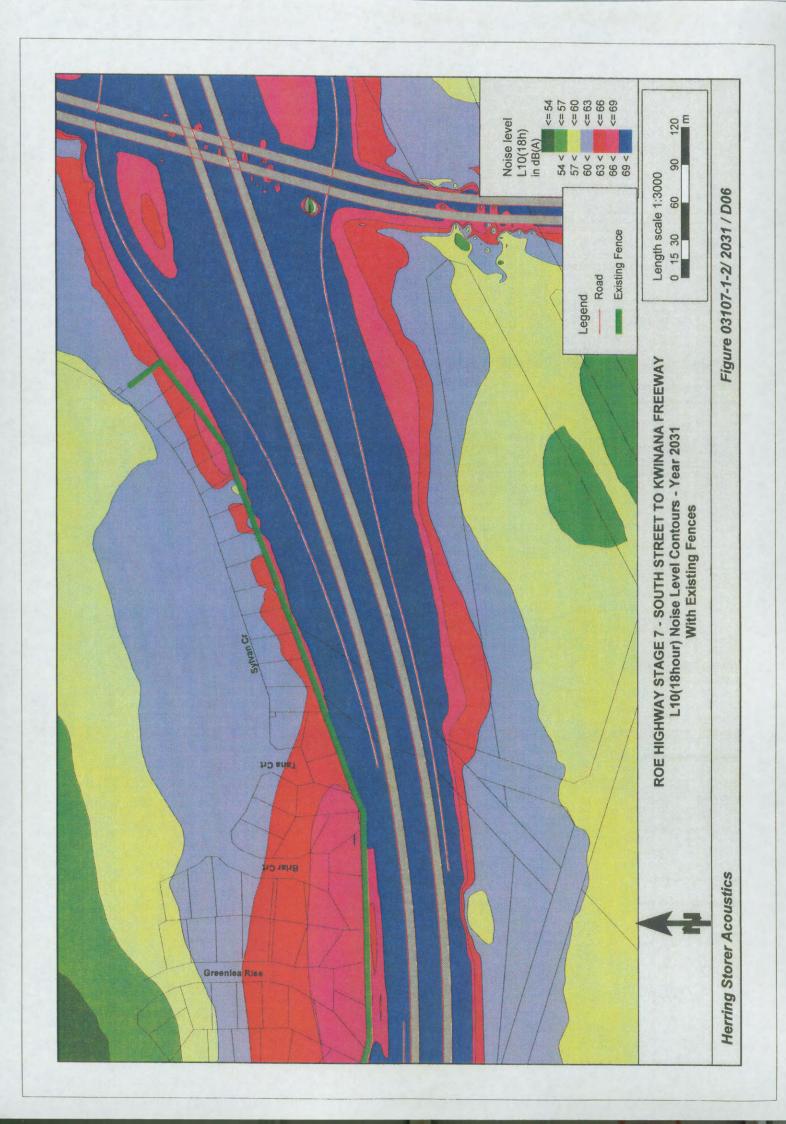


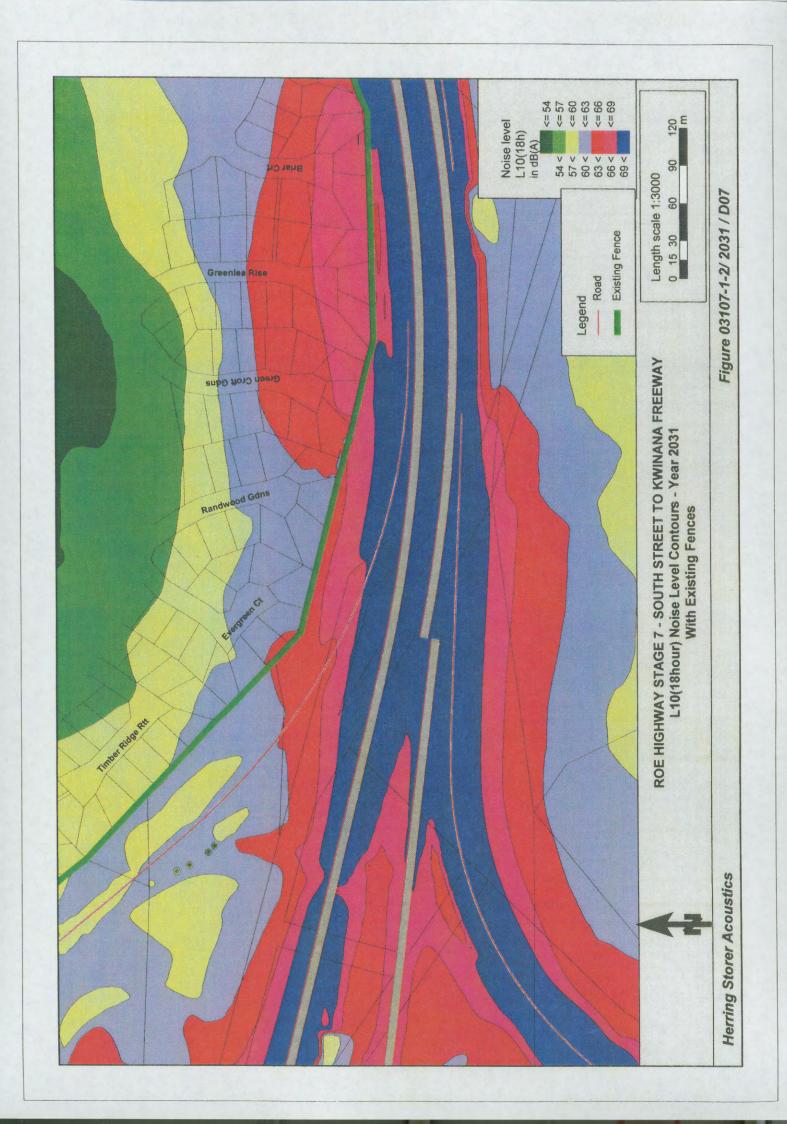




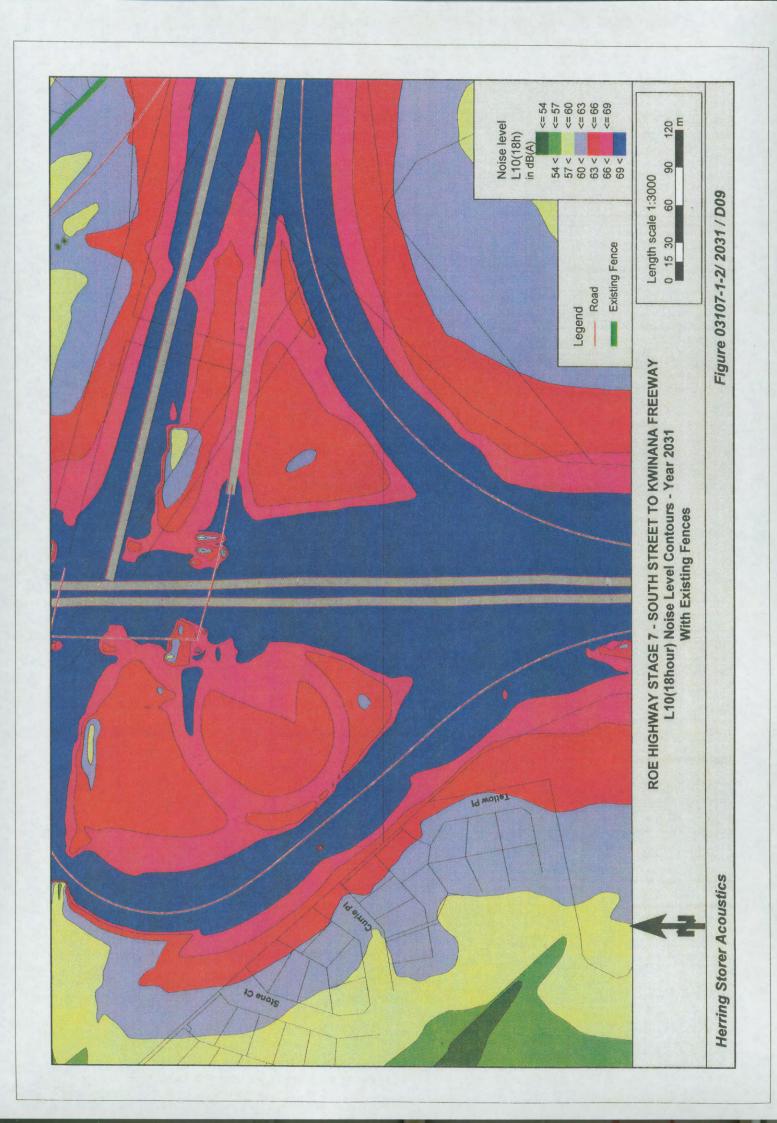








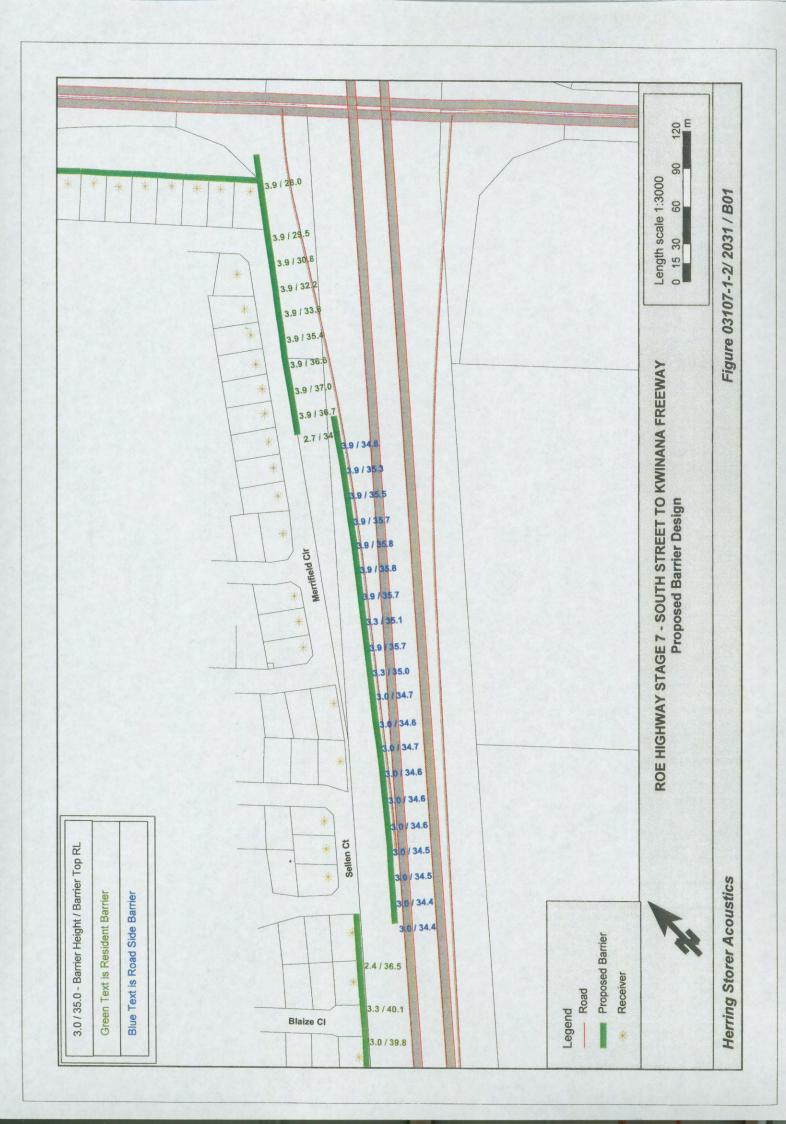




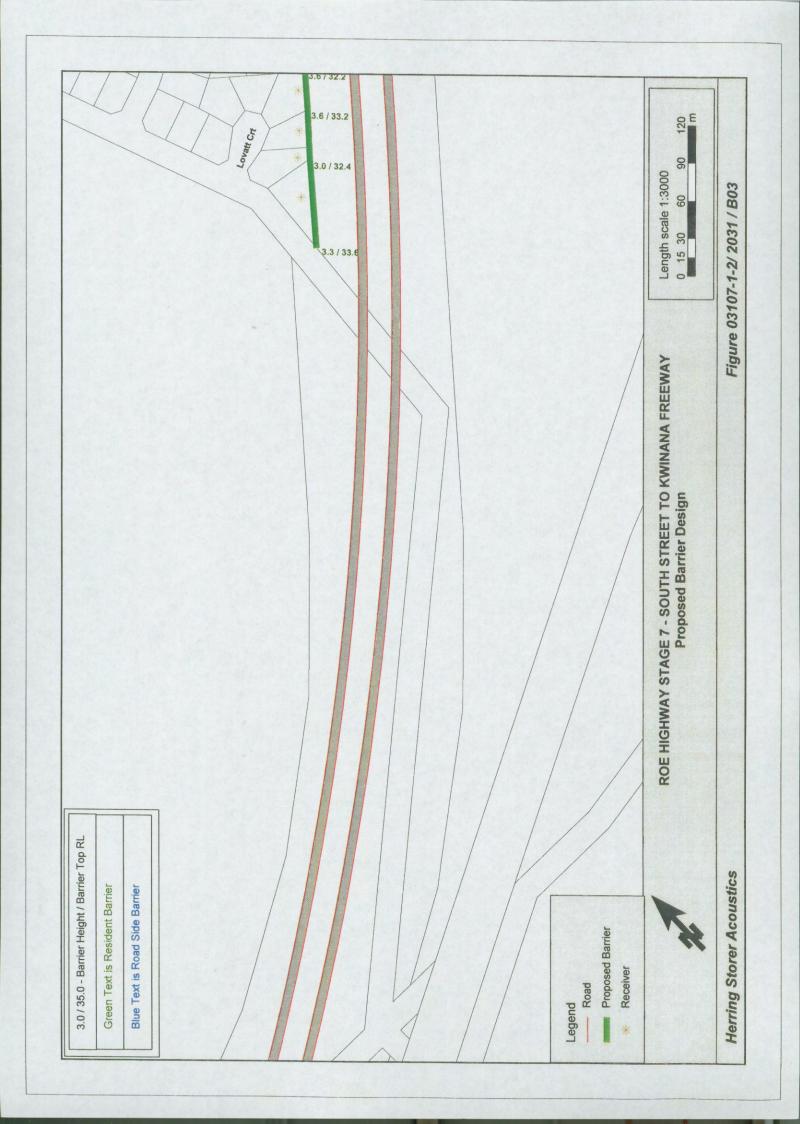


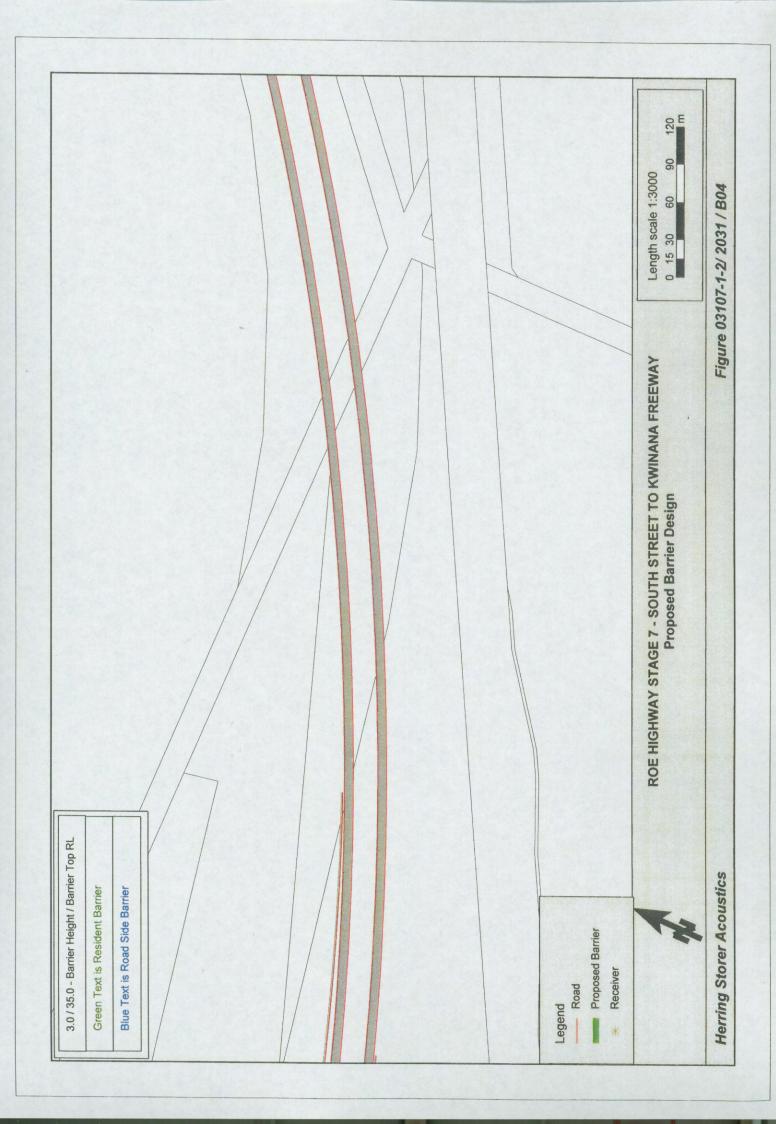
## **APPENDIX E**

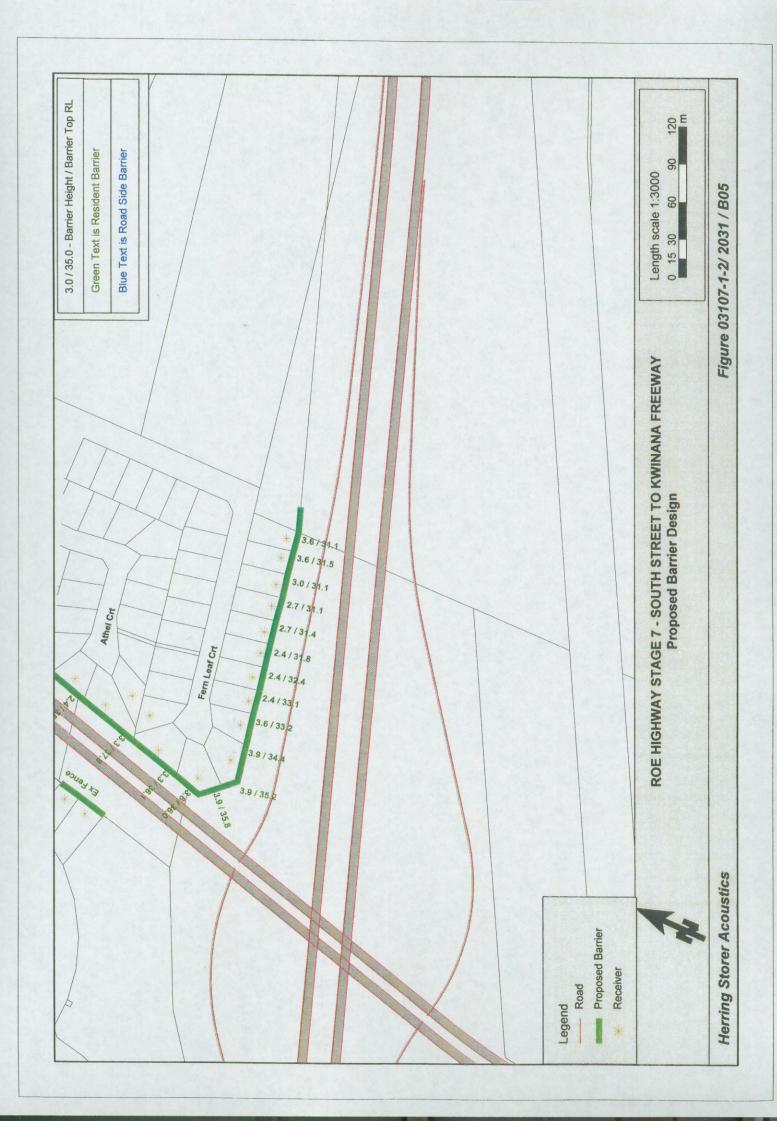
MINIMUM RECOMMENDED NOISE WALLS

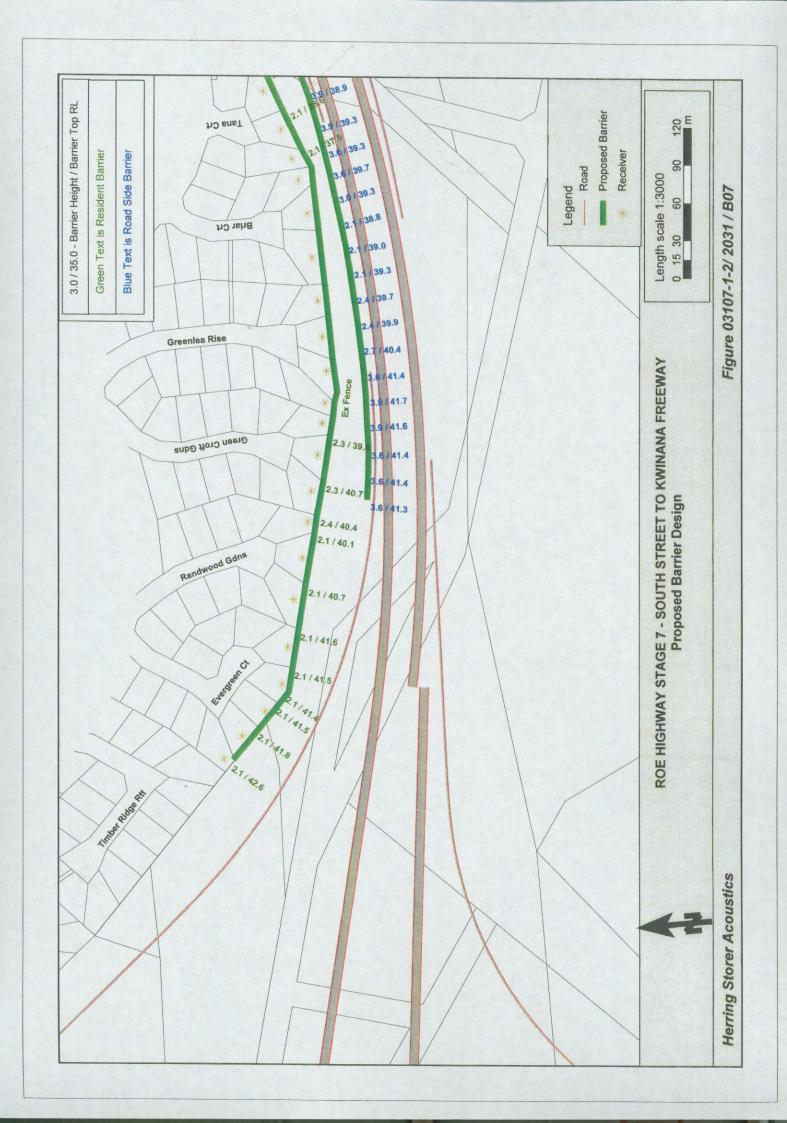




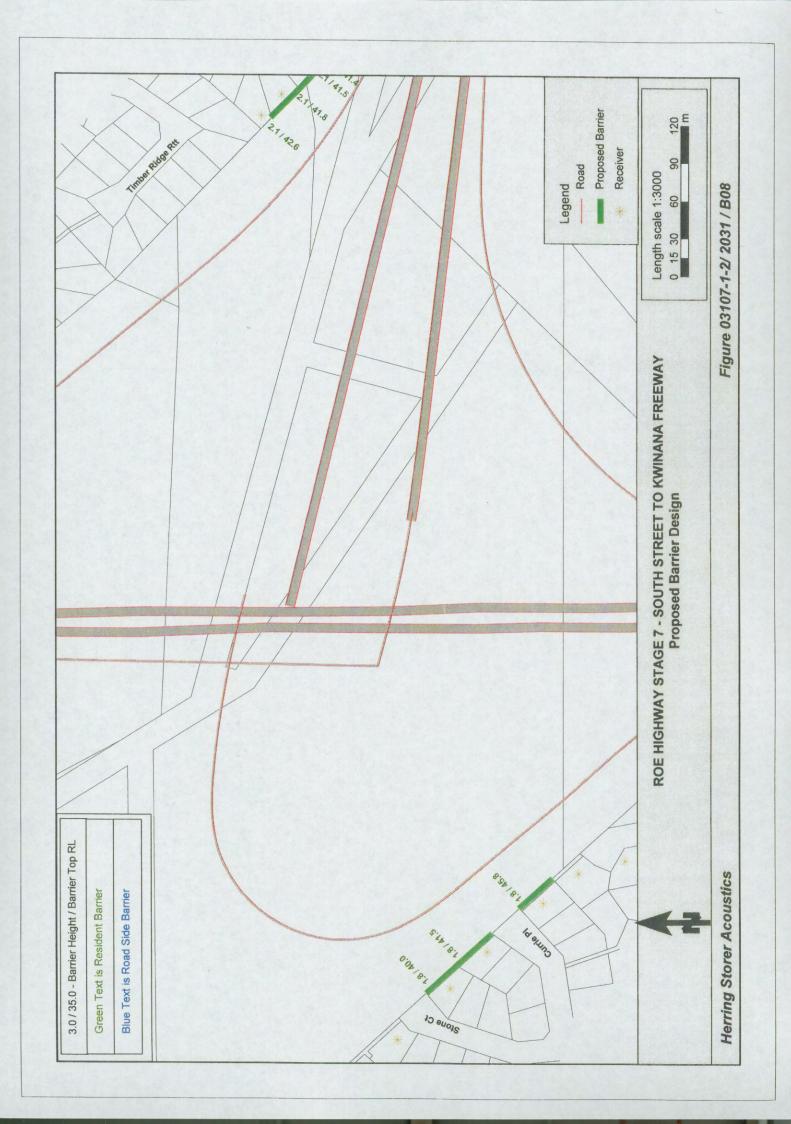


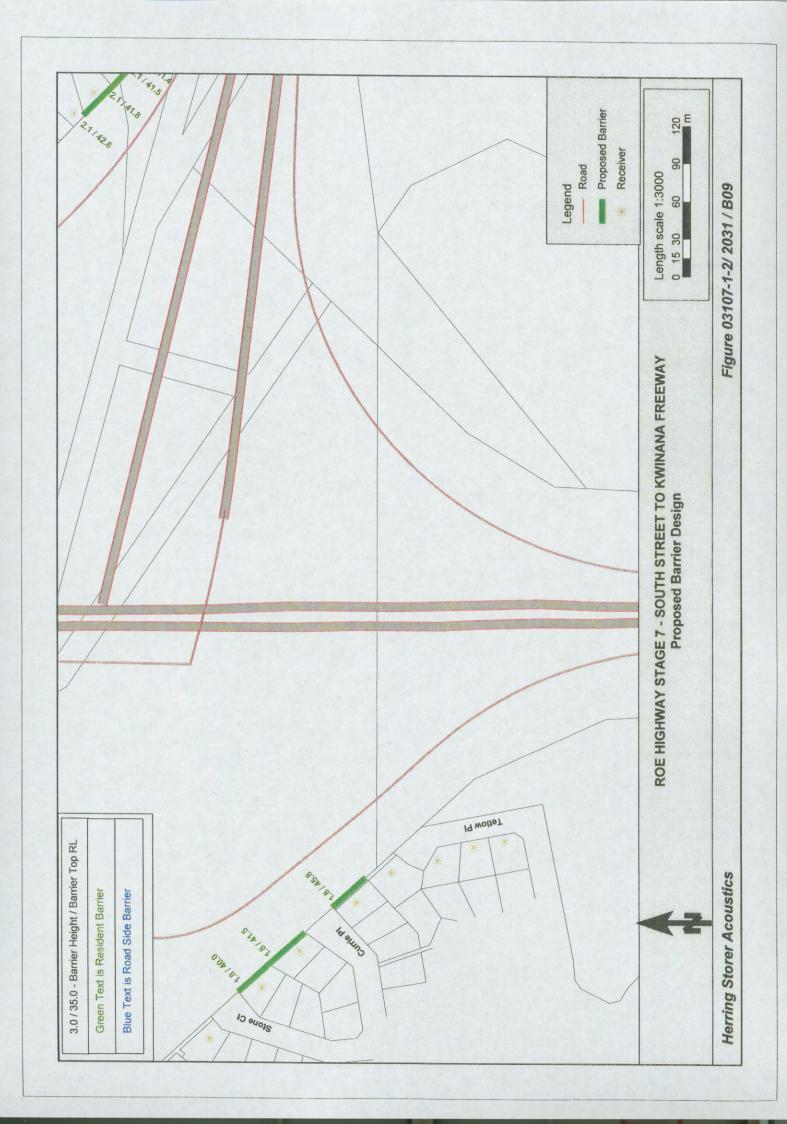


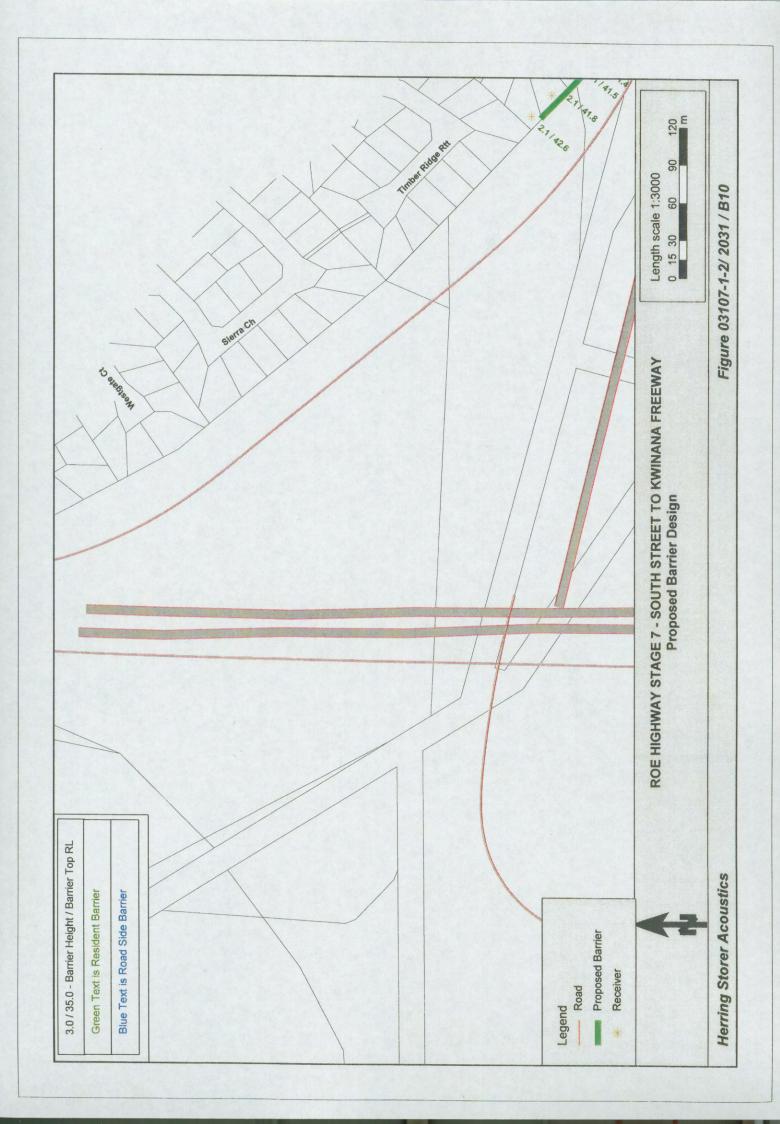












## **APPENDIX F**

PREDICTED 2031 NOISE LEVELS TO SURROUNDING AREAS-NOISE LEVEL CONTOUR PLOTS: RECOMMENDED NOISE WALLS

